

X. *Contributions to Terrestrial Magnetism.—No. V.*  
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Received June 14,—Read June 15, 1843.

§ 8. *Observations within the Antarctic Circle, made on Board Her Majesty's Ships Erebus and Terror, in the Summer of 1840, 1841, in the Expedition under the command of Captain JAMES CLARK ROSS, R.N.*

§ 9. *Observations between Kerguelen Island and Van Diemen Island, made on Board Her Majesty's Ship Erebus, July and August 1840.*

§ 8. *Observations within the Antarctic Circle in the Summer of 1840, 1841.*

IN the present number of these Contributions, I have the pleasure of laying before the Royal Society the magnetic observations made by Captain JAMES CLARK ROSS, and the Expedition under his command, in the first of the three voyages in which these researches have been prosecuted within the Antarctic Circle; and I gladly avail myself of the opportunity which the occasion affords, of congratulating the Society on the successful completion of the labours and on the approaching return, of an Expedition, in which the Fellows individually, and as a body, have taken so strong an interest. A large portion of the observations contained in this number were made in southern latitudes never before reached by man; and nearly the whole in a part of the globe extremely difficult of access, but containing within itself a field for researches peculiarly needed for completing and perfecting, in the words of HALLEY, “the abstruse theory of terrestrial magnetism.”

In presenting to the Royal Society this portion of the results of an arduous enterprise, undertaken at their recommendation, it appears no improper departure from the usual tone of these communications, to allude very briefly to the causes which, under Providence, have conduced to its safe and successful issue;—to the admirable preparation and equipment of the vessels on the part of the Government,—to the high qualities of its Commander, manifested in conducting to its close, almost without an accident, and to the fullest accomplishment of its objects, a service of such duration and peculiar hazard,—and to the excellent spirit in which the Commander has been seconded by Captain CROZIER, and supported by the officers and seamen who have been their worthy associates.

Viewed merely as an expedition of discovery, its voyages must ever rank high in the annals of those maritime achievements of which our country is proud; but as a scientific expedition, which is its more proper character, as well as that in which the

Royal Society must regard it with the greatest satisfaction, its best praise will undoubtedly be found in the record of its performances ; and I hasten therefore to enter on that portion of them which I am now enabled to present to the Society.

The peculiar feature in the magnetic survey of the portion of the southern hemisphere now under notice is, that it was conducted almost exclusively on board ship, the observations being subject to the disturbance occasioned by the ship's iron, in a part of the globe where the effect of this influence becomes excessive. The first consideration, therefore, must be to investigate the corrections which it is necessary to employ in compensation. The analysis of the effects produced by the iron of a vessel, and the theory of their corrections, have been given by the late M. Poisson, in a memoir read in 1838, and published in the Transactions of the Académie des Sciences, entitled "Mémoire sur les déviations de la Boussole produites par le fer des Vaisseaux." In cases in which the disturbance is due, partly to the magnetism induced by the earth's influence in the soft iron of the vessel, and partly to permanent magnetism acquired and retained by harder portions of her iron, the complexity of the source from whence the disturbance originates renders its correction very difficult. But in wood-built ships, when proper precautions are taken in regard to the place in the ship in which the instrument is used in observation, the disturbing influence is generally found to be that of induced magnetism alone : and in this case the correction may be obtained with tolerable facility\*. The disturbance produced by the iron of the Erebus and Terror appearing to be of the latter class, I requested my friend Mr. ARCHIBALD SMITH, Fellow of Trinity College, Cambridge, who in his academic course obtained the highest distinction conferred by the University, to draw out from M. Poisson's fundamental equations, applicable to induced magnetism, the most convenient and practical formulæ for computing the corrections of the three magnetic

\* Since this communication was read to the Royal Society, Mr. AIRY has favoured me with the following note :—"M. Poisson's deductions are founded on the assumption, that the phenomena of magnetism depend on the action of two fluids which attract each other, but which each repel other portions of fluid of the same kind : and that induction is caused by an alteration in the arrangement of these fluids among the particles of iron, produced by the attraction and repulsion of the earth's magnetic fluids. His fundamental equations in common language may be stated as follows :—

$$\left. \begin{array}{l} \text{Horizontal force towards the} \\ \text{ship's head, as disturbed,} \end{array} \right\} = A' \times \left\{ \begin{array}{l} \text{Undisturbed horizontal} \\ \text{force to ship's head} \end{array} \right\} + C \times \text{undisturbed vertical force.}$$

$$\left. \begin{array}{l} \text{Horizontal force towards the} \\ \text{ship's head, as disturbed,} \end{array} \right\} = E' \times \left\{ \begin{array}{l} \text{Undisturbed horizontal} \\ \text{force to ship's side} \end{array} \right\}$$

$$\text{Vertical force, as disturbed . . .} = G \times \left\{ \begin{array}{l} \text{Undisturbed horizontal} \\ \text{force to ship's head} \end{array} \right\} + K' \times \text{undisturbed vertical force.}$$

"These equations are the same as those obtained by Mr. AIRY in the Philosophical Transactions, 1839, the first and second being the same as the two equations in page 184, and the third being the same as the last of the group of three equations in page 181. Mr. AIRY's expressions however imply that G is equal to C. The calculations in the sequel of this paper seem to show that in the Erebus G is greater than C. Mr. AIRY's deductions are founded on the assumption that each particle of iron is converted, by the earth's magnetic action, into a magnet with its length parallel to the direction of terrestrial magnetism."

elements, for the use of nautical men, and of others who might be engaged in reducing magnetic observations made at sea. He has obligingly furnished me with the following memorandum :—

“At a given geographical position let  $\phi$  represent the total magnetic intensity of the earth ;  $\theta$  the dip, which is considered positive when the north end of the needle dips below the horizontal plane, negative when it inclines above it ;  $\zeta$  the azimuth of the ship’s head, or the angle between the principal section of the ship and the magnetic meridian, which is considered positive when the ship’s head is to the west of the magnetic north, negative when to the east. Let  $\phi', \theta', \zeta'$ , be the values of the same elements shown by a needle whose centre is at a given place in the ship, when affected by the magnetism induced in the soft iron of the ship by the magnetism of the earth. M. POISSON has shown that if the dimensions of the needle are very small compared to its distance from the iron by which it is affected, the following equations are true ;

$$\begin{aligned} \phi' \cos \theta' \cos \zeta' &= \phi [A' \cos \theta \cos \zeta + B \cos \theta \sin \zeta + C \sin \theta], \\ \phi' \cos \theta' \sin \zeta' &= \phi [D \cos \theta \cos \zeta + E' \cos \theta \sin \zeta + F \sin \theta], \\ \phi' \sin \theta' &= \phi [G \cos \theta \cos \zeta + H \cos \theta \sin \zeta + K' \sin \theta]. \end{aligned}$$

“In these equations,  $A', B, C, D, E', F, G, H, K'$  are constants which depend only on the distribution of the iron in the ship relatively to the position of the needle and the plane of the horizon, and which continue the same for every geographical position of the ship, while the distribution of the iron within the ship, and the inclination of the ship to the horizon, remain the same.

“If the centre of the needle is placed in the principal section of the ship, and the iron is symmetrically distributed on each side of that section, it will easily be seen that for values of  $\zeta$  equal in magnitude and opposite in sign, the corresponding values of  $\zeta'$  are equal in magnitude and opposite in sign, and the corresponding values of  $\phi'$  and  $\theta'$  are respectively equal in magnitude and the same in sign. These results necessarily imply that  $B, D, F$  and  $H$  are equal to zero. The equations in this case become

$$\begin{aligned} \phi' \cos \theta' \cos \zeta' &= \phi [A' \cos \theta \cos \zeta + C \sin \theta], \\ \phi' \cos \theta' \sin \zeta' &= \phi \cdot E' \cos \theta \sin \zeta, \\ \phi' \sin \theta' &= \phi [G \cos \theta \cos \zeta + K' \sin \theta]. \end{aligned}$$

“If we divide each term by  $\phi A'$  and put  $\frac{C}{A'} = a, \frac{E'}{A'} = b, \frac{G}{A'} = c, \frac{K'}{A'} = d,$

$$\frac{\phi'}{A' \phi} \cos \theta' \cos \zeta' = \cos \theta \cos \zeta + a \sin \theta \quad . . . . . (1.)$$

$$\frac{\phi'}{A' \phi} \cos \theta' \sin \zeta' = b \cos \theta \sin \zeta. \quad . . . . . (2.)$$

$$\frac{\phi'}{A' \phi} \sin \theta' = c \cos \theta \cos \zeta + d \sin \theta. \quad . . . . . (3.)$$

“ From these equations are derived the following :—

$$\frac{\theta'}{A'\phi'} \cos \theta' = (\cos \zeta \cos \zeta' + b \sin \zeta \sin \zeta') \cos \theta + a \cos \zeta' \sin \theta, \dots (4.)$$

$$\cos \zeta \sin \zeta' + a \tan \theta \sin \zeta' = b \sin \zeta \cos \zeta'; \dots (5.)$$

and representing  $\zeta - \zeta'$ , or the deviation by  $\delta$ ,

$$\sin \delta = a \tan \theta \sin \zeta' + (1 - b) \cos \zeta' \sin \zeta \dots (6.)$$

$$= \frac{2a}{1+b} \tan \theta \sin \zeta' + \frac{1-b}{1+b} \sin (\zeta + \zeta') \dots (7.)$$

$$\tan \zeta' = \frac{b \sin \zeta}{\cos \zeta + a \tan \theta} \dots (8.)$$

$$c \cos \zeta + d \tan \theta = b \sin \zeta \operatorname{cosec} \zeta' \tan \theta' \dots (9.)$$

$$= (\cos \zeta + a \tan \theta) \sec \zeta' \tan \theta' \dots (10.)$$

$$= \sqrt{(\cos \zeta + a \tan \theta)^2 + b^2 \sin^2 \zeta} \tan \theta' \dots (11.)$$

$$\tan \theta' = \frac{c}{b} \cdot \left( \cos \zeta + \frac{d}{c} \tan \theta \right) \sin \zeta' \operatorname{cosec} \zeta \dots (12.)$$

$$= c \frac{\cos \zeta + \frac{d}{c} \tan \theta}{\cos \zeta + a \tan \theta} \cdot \cos \zeta' \dots (13.)$$

$$= c \cdot \frac{\cos \zeta + \frac{d}{c} \tan \theta}{\sqrt{(\cos \zeta + a \tan \theta)^2 + b^2 \sin^2 \zeta}} \dots (14.)$$

“ From these equations, and observations made at one geographical position with the ship’s head on different azimuths, the constants  $a, b, c, d, A'$  may be determined, and the corrections of the affected elements at any other geographical position may be calculated.

“  $a$  and  $b$  may be determined from observed deviations of the compass needle by means of equation (5.). A table of the deviations on each affected or compass course, and of the true magnetic course for each affected or compass course, may then be calculated by equations (6.) or (7.). In these equations  $\zeta$ , which is an unknown quantity, occurs in the second term on the right-hand side; but the term is so small that an approximate value of  $\zeta$  may be used, and the error caused thereby neglected. This error is least in equation (7.), which is also the most convenient for calculation except on east and west courses.

“ To find the compass course for each true magnetic course, it will generally be sufficient to apply the deviations corresponding to the nearest true magnetic courses contained in the Table last described; but if the deviations are large, it will be better to construct a separate table by means of equation (8.).

“  $c$  and  $d$  may be determined from the true dip and the affected dips observed on different courses by means of equation (11.), or more easily by means of (9.) and (10.); observing that the values of  $\zeta$  employed should be not observed values, but tabular

values calculated in the manner described above. A table of the affected dip, and of the dip corrections on each course, may then be calculated from (14.), or more easily from (12.) and (13.); observing that (12.) must not be used when the ship's course is nearly north or south, and that (13.) must not be used when the ship's course is nearly east or west, and that the values of  $\zeta$  should be tabular, not observed.

“The constants may also be determined from observations of the total intensity, by means of the first four equations, and tables for the correction of the observed intensities may be constructed by means of these equations. For this purpose, equation (3.) should be used when the dip is large, and the others when the dip is small.

“The values of  $a$  and  $b$  may be determined very readily, and probably with great accuracy, from observations of the horizontal intensity with the ship's head on the four principal compass courses. For if  $H_n, H_w, H_s, H_e$  represent the values so observed, then

$$a \tan \theta = \frac{H_n - H_s}{H_n + H_s}, \dots \dots \dots (15.)$$

$$b = \frac{H_w + H_e}{2 \sqrt{H_w H_s}} \dots \dots \dots (16.)$$

“If observations are made at equal intervals of time with the ship's head successively on the N., W., S., E., and N. points, the values of  $a$  and  $b$  thus determined will be independent of any regular increase or diminution of the intensity. If  $n, w, s, e$  represent the number of vibrations in equal times, on the four principal courses, of the same horizontal needle, beginning to vibrate in the same arc, and corrected for temperature alone,

$$a \tan \theta = \frac{n^2 - s^2}{n^2 + s^2}, \dots \dots \dots (17.)$$

$$b = \frac{w^2 + e^2}{2 n s} \dots \dots \dots (18.)$$

“The true declination may be found independently of the dip and of the constant  $a$ , by means of observations of the true azimuth of the ship's head on two courses. Let  $\psi$  represent the declination, which is considered positive when the north end of the needle is to the west of the true north,  $\omega$  the true azimuth of the ship's head, which is positive when the ship's head is to the west of the true north; so that  $\zeta = \omega - \psi$ . And let  $\omega_1, \zeta'_1$  and  $\omega_2, \zeta'_2$  represent the observed values of  $\omega$  and  $\zeta'$  on the two courses,

$$\tan \left( \psi - \frac{\omega_1 + \omega_2}{2} \right) = \frac{b \sin (\zeta'_1 + \zeta'_2)}{2 \sin \zeta'_1 \sin \zeta'_2 - b \sin (\zeta'_1 - \zeta'_2) \cot \frac{\omega_1 - \omega_2}{2}}$$

“If the observations are made with the ship's head on exactly opposite courses,  $\omega_1 - \omega_2 = 180^\circ$ ; and we have

$$\tan (\omega_1 - \psi) = \frac{2 \sin \zeta'_1 \sin \zeta'_2}{b \sin (\zeta'_1 + \zeta'_2)};$$

if at equal azimuths on each side of the magnetic north,

$$\psi = \frac{\omega_1 + \omega_2}{2}.$$

“The formula fails if  $\zeta'_1 + \zeta'_2 = 180^\circ$ , the denominator becoming zero; the true value of  $\tan\left(\psi - \frac{\omega_1 + \omega_2}{2}\right)$  in that case is

$$\frac{b}{\sin 2 \zeta'_1 + b \cos 2 \zeta'_1 \cot \frac{\omega_1 - \omega_2}{2}}$$

*Corrections for the Erebus.*—We will seek in the first instance the values of the constants  $a$  and  $b$ , because they are those which can be obtained with the greatest degree of exactness, being derived from observations with the compass needle, which are made with greater precision than those with the inclination or intensity needles. Before the Expedition quitted England, a suitable position in the midship line was chosen for magnetic observations on board ship, and the effect of the ship’s attraction on a standard compass placed in that spot, was ascertained by observations with the ship’s head turned successively on each of the thirty-two principal points. This was done in September 1839 at Gillingham near Chatham, where  $\theta$ , or the Inclination, was at that epoch  $69^\circ 05'$ .\*

The observations in the Erebus gave results as follows :—

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N.	+0 06	w.	+4 19	s.	+0 28	E.	-3 42
N. by w.	+1 12	w. by s.	+4 40	s. by E.	-0 19	E. by N.	-4 53
N.N.W.	+2 01	w.s.w.	+4 03	s.s.E.	-0 48	E.N.E.	-3 46
N.W. by N.	+2 10	s.w. by w.	+3 24	s.E. by s.	-1 23	N.E. by E.	-3 18
N.W.	+3 03	s.w.	+2 45	s.E.	-1 53	N.E.	-2 59
N.W. by w.	+3 28	s.w. by s.	+2 08	s.E. by E.	-2 21	N.E. by N.	-2 16
w.N.W.	+3 51	s.s.w.	+1 34	E.S.E.	-2 50	N.N.E.	-1 39
w. by N.	+4 09	s. by w.	+0 52	E. by s.	-3 17	N. by E.	-0 49

We perceive by this Table that, allowance being made for slight irregularities in the observations, the masses of iron which acted on the compass needle of the Erebus in its standard position were distributed symmetrically, or very nearly so, on either side of the vertical plane, passing through the longitudinal midship section. We may therefore safely employ, in computing the corrections, the more simple formulæ which are applicable under this condition.

To obtain the constants  $a$  and  $b$  of these formulæ we may arrange equations on the several points, from the observations in the Table, of the form

$$\cos \zeta \sin \zeta' - b \sin \zeta \cos \zeta' = - a \tan \theta \sin \zeta'.$$

\* Reports of the British Association, 1838.

N. by W.	·1905	—	·2115	<i>b</i> =	—	0·510	<i>a</i>	
N.N.W.	·3482	—	·3834	<i>b</i> =	—	1·001	<i>a</i>	
N.W. by N.	·4481	—	·4916	<i>b</i> =	—	1·454	<i>a</i>	
N.W.	·4727	—	·5258	<i>b</i> =	—	1·850	<i>a</i>	
N.W. by W.	·4193	—	·4798	<i>b</i> =	—	2·175	<i>a</i>	
N.N.W.	·2954	—	·3626	<i>b</i> =	—	2·417	<i>a</i>	
W. by N.	·1212	—	·1936	<i>b</i> =	—	2·566	<i>a</i>	
	+	2·2954	—	2·6483	<i>b</i> =	—	11·973	<i>a</i> . . . . . (1.)

W. by S.	—	·2689	+	·1876	<i>b</i> =	—	2·566	<i>a</i>
W.S.W.	—	·4130	+	·3423	<i>b</i> =	—	2·417	<i>a</i>
S.W. by W.	—	·5021	+	·4427	<i>b</i> =	—	2·175	<i>a</i>
S.W.	—	·5233	+	·4754	<i>b</i> =	—	1·850	<i>a</i>
S.W. by S.	—	·4729	+	·4359	<i>b</i> =	—	1·454	<i>a</i>
S.S.W.	—	·3574	+	·3301	<i>b</i> =	—	1·001	<i>a</i>
S. by W.	—	·1919	+	·1768	<i>b</i> =	—	0·510	<i>a</i>
	—	2·7295	+	2·3908	<i>b</i> =	—	11·973	<i>a</i> . . . . . (2.)

S. by E.	·1915	—	·1860	<i>b</i> =	0·510	<i>a</i>		
S.S.E.	·3563	—	·3366	<i>b</i> =	1·001	<i>a</i>		
S.E. by S.	·4693	—	·4451	<i>b</i> =	1·454	<i>a</i>		
S.E.	·5161	—	·4832	<i>b</i> =	1·850	<i>a</i>		
S.E. by E.	·4900	—	·4489	<i>b</i> =	2·175	<i>a</i>		
E.S.E.	·3953	—	·3459	<i>b</i> =	2·417	<i>a</i>		
E. by S.	·2462	—	·1888	<i>b</i> =	2·566	<i>a</i>		
	+	2·6647	—	2·4345	<i>b</i> =	11·973	<i>a</i> . . . . . (3.)	

E. by N.	—	·1088	+	·1939	<i>b</i> =	2·566	<i>a</i>	
E.N.E.	—	·2967	+	·3625	<i>b</i> =	2·417	<i>a</i>	
N.E. by E.	—	·4214	+	·4789	<i>b</i> =	2·175	<i>a</i>	
N.E.	—	·4732	+	·5252	<i>b</i> =	1·850	<i>a</i>	
N.E. by N.	—	·4494	+	·4888	<i>b</i> =	1·454	<i>a</i>	
N.N.E.	—	·3492	+	·3780	<i>b</i> =	1·001	<i>a</i>	
N. by E.	—	·1908	+	·2050	<i>b</i> =	0·510	<i>a</i>	
	—	2·2895	+	2·6323	<i>b</i> =	11·973	<i>a</i> . . . . . (4.)	

From (1.) and (4.), changing the signs of (1.) and summing, we have

$$- 4·5849 + 5·2806 b = + 23·946 a. . . . . (5.)$$

From (2.) and (3.), changing the signs of (3.) and summing, we have

$$- 5·3942 + 4·8253 b = - 23·946 a; . . . . . (6.)$$

whence  $10·1059 b = + 9·9791$ ; and  $b = + ·9875$ ;

From (5.) and (6.), changing the signs of (6.) and summing, we have

$$47.892 a = .4553 b + .8093 ; \quad a = + .0263.$$

We have also the equations at east and west ;

$$\text{East} \quad . \quad . \quad . \quad . \quad . \quad 2.617 a = + .0645$$

$$\text{West} \quad . \quad . \quad . \quad . \quad . \quad -2.617 a = - .0753 ;$$

whence

$$a = \frac{.1398}{5.234} = + .0267 ;$$

or including the observations at east and west in the general sum, we have  $a = + .0264$ .

After the arrival of the Expedition at Hobarton, and before it sailed to the Antarctic Circle, a similar series of observations was made in the Erebus, on the 29th October 1840, and again repeated on her return to Hobarton the following autumn, viz. on the 29th June 1841. The south end of the needle being now the one which dipped below the horizon ( $\theta$  being  $-70^\circ 40'$ ), the deviation of the compass was found to take place in the contrary direction to that which had been observed at Gillingham, the disturbance being towards the *west* as the ship's head went round from north by east to south, and towards the *east* as her head passed from south through west to north.

The line of no deviation was not found to correspond accurately with the north and south points of the compass on either of the occasions at Hobarton, but in 1840 coincided more nearly with the north by west and south by east, and in 1841 with the north by east and south by west. We may perhaps ascribe with probability irregularities of this nature to slight modifications in the distribution of the iron at different periods, which we cannot but view as of not unlikely occurrence ; for example, such as might be occasioned by the ship being secured at different times by the starboard or the larboard chain cable. In looking through the observations of the Erebus, it is evident that there was no systematic or constant deviation of the plane of the ship's attraction from that of her principal section ; but that the points of no disturbance were sometimes a little on the one side, and sometimes a little on the other, of the north and south points. It appears, therefore, not improper to class these irregularities with those others of accidental occurrence which occasion small discordances in partial results, and are usually ranged under the general technical head of errors of observation.

If, further, we compare generally the deviations in 1840 with those of April 1841, the latter appear systematically rather the more considerable in amount. Viewed as a single fact, this circumstance might be regarded simply as indicating that some change had taken place in the interim in the arrangement and distribution of the ship's iron, and an easy and natural explanation might appear to be afforded. It is however one of several facts which have presented themselves in the course of a careful examination of the observations of the first two years of Captain Ross's expedition, which seem to point to the possibility of a somewhat different cause, viz. that when



a ship changes her magnetic latitude, the corresponding change in the magnetism of the ship, or more strictly in that portion of it which is derived from induction, follows, but does not always, or altogether, take place instantaneously. It would accord with this supposition, that the disturbance of the compass should be less in the Erebus on her first arrival at Hobarton in 1840, than on her return there in 1841, because in 1840 she had recently passed through the lowest magnetic latitudes, and in 1841 she came immediately from the highest. The observations in 1840 give a less value for  $a \tan \theta$  than those of 1841, and taking the dip at Hobarton as the value of  $\theta$ , to which the induced magnetism of the ship on both occasions should strictly correspond, we should have a less value for  $a$  in 1840 than in 1841; whereas if with the same dip we take a mean between the disturbances of the compass on the first arrival and on the return, by which we may be conceived to neutralize in a great measure the temporary influences which have been supposed, we find the value of  $a$  to be almost identical with the result of the former experiments at Gillingham. From this accordance in the value of the constant in dips which differ so greatly as from  $+69^\circ$  to  $-70^\circ$ , we should infer the probability,—first, that the local attraction of the Erebus was due to induced magnetism alone, the influence of any portions of iron which, in the strict sense of the term, were permanently magnetic, being insensible;—and secondly, that no material change affecting the standard compass had taken place in the distribution of her iron. These inferences are by no means inconsistent with the supposition above suggested, that some portions of her iron might be of a quality intermediate between that of perfectly soft iron which undergoes instantaneous change, and that of iron which acquires permanent magnetism, and that such portions should be liable, in regard to their magnetic condition, to be more or less in arrear of the ship's magnetic position. I abstain from entering further into this question at present, because a fitter opportunity of doing so will be afforded when the whole of the observations of the Expedition shall be collected, including those which have yet to be made at Rio de Janeiro on the return from the high latitudes of the south, and in England after passing through the low magnetic latitudes of the equatorial region. Should it prove that the induced magnetism of a ship due to any particular dip requires time for its full development, more or less according to the various quality of her iron, the corrections to be applied may possibly in some ships be considerably complicated thereby: fortunately in the Erebus the difference in the amount of the disturbance on the two occasions at Hobarton, which gave rise to this discussion, is not of any serious consequence; and we may employ without any material inconvenience for our present purpose the mean of the two series as applicable generally between their respective dates, for which interval we specially desire the corrections.

Ship's head by compass.	Disturbance towards the west.			Ship's head by compass.	Disturbance towards the west.		
	1840.	1841.	Mean.		1840.	1841.	Mean.
N.	+1 10	-0 26	+0 22	s.	-0 49	+0 43	-0 03
N. by w.	+0 24	-1 14	-0 25	s. by E.	-0 01	+2 32	+1 15
N.N.W.	-0 40	-2 01	-1 20	s.S.E.	+0 38	+3 06	+1 52
N.W. by N.	-1 54	-2 34	-2 14	s.E. by s.	+1 12	+3 51	+2 32
N.W.	-2 10	-2 55	-2 32	s.E.	+1 35	+4 34	+3 04
N.W. by w.	-2 58	-3 13	-3 05	s.E. by E.	+2 35	+5 01	+3 48
w.N.W.	-3 18	-3 51	-3 35	E.S.E.	+3 17	+4 45	+4 01
w. by N.	-3 39	-4 32	-4 06	E. by s.	+3 12	+5 21	+4 17
w.	-4 15	-4 59	-4 37	E.	+3 38	+5 07	+4 22
w. by s.	-4 13	-4 56	-4 35	E. by N.	+3 54	+4 46	+4 20
w.s.w.	-4 27	-4 41	-4 34	E.N.E.	+3 30	+4 06	+3 48
s.w. by w.	-4 39	-4 19	-4 29	N.E. by E.	+3 21	+3 45	+3 33
s.w.	-4 06	-3 40	-3 53	N.E.	+3 12	+3 08	+3 10
s.w. by s.	-3 36	-2 50	-3 13	N.E. by N.	+2 50	+2 39	+2 45
s.s.w.	-2 30	-2 15	-2 22	N.N.E.	+2 26	+1 30	+1 58
s. by w.	-1 39	-0 19	-0 59	N. by E.	+2 19	+0 38	+1 28

Employing the same formula as before, and forming equations from the observations on the twenty-eight points, being all the points excepting the north, south, east and west, we obtain

$$10\cdot1036 b = + 9\cdot9673$$

$$b = + \cdot9865 ;$$

and from the sum of the thirty equations, including those at east and west, we have

$$+ 57\cdot89 a = + 1\cdot0439 + \cdot537 b,$$

$$a = \frac{1\cdot0439 + \cdot5297}{57\cdot89} = + \cdot0272.$$

On the passage from Hobarton to the Antarctic Circle, the Expedition stopped at Auckland Island for the purpose of observing on the term day of November 1840. The Erebus was not swung at this station, but with the value of  $\theta$  observed on shore  $- 73^\circ 10'$ , and the declination observed on board whilst at anchor, with the ship's head on the east and west points, and on the E.N.E. and W.N.W. points, we may obtain a satisfactory value for  $a$ . On the supposition of the symmetrical distribution of the iron on either side of the longitudinal midship section, the deviation occasioned by it should be the same in amount, but with opposite signs, at east and west, and also at E.N.E. and W.N.W.; the amount, however, being slightly different at east and west from that at E.N.E. and W.N.W.

From the observations at east and west we have

$$\psi' = - 12^\circ 52' \text{ at east, and } \psi' = - 22^\circ 55' \text{ at west ;}$$

$$\psi = \frac{\psi' + \psi'}{2} = - 17^\circ 53'\cdot5, \text{ and}$$

$$\delta = \pm 5^\circ 01'\cdot5 ; \text{ whence } a = + \cdot0265.$$

From the observations at E.N.E. and W.N.W.,

$$\psi = -13^{\circ} 36' \text{ at E.N.E., and } -22^{\circ} 06' \text{ at W.N.W. ;}$$

$$\psi = -17^{\circ} 51' ; \zeta' = 67^{\circ} 30', \text{ and } \zeta = 63^{\circ} 15' ; \text{ whence } a = \cdot 0261.$$

The mean of the two pairs of observations gives  $a = + \cdot 0263$ .

Whilst within the Antarctic Circle only a single opportunity occurred of observing the inclination otherwise than on board, and thus of obtaining  $a$  from  $a \tan \theta$  by having an assured value of  $\theta$ . This was on the 8th of January 1841, in lat.  $-68^{\circ} 30'$ , long.  $176^{\circ} 35'$ , where the inclination observed on the ice with a needle in which the observation was complete by the reversal of the poles, was found to be  $-83^{\circ} 35'$ . The declination was observed on board on the same afternoon and following morning, as nearly as could be in the same geographical position, with the ship's head on several points, from which we may select for a determination of  $a$  those nearest to the east and west points. We have then the following observations:—

- |  |  |
|--|--|
| 1. At W. $\frac{3}{4}$ N. $\psi = -46^{\circ} 02'$       | 4. At E. $\frac{3}{4}$ N. $\psi = -20^{\circ} 51'$       |
| 2. At W. by S. $\psi = -46^{\circ} 32'$                  | 5. At E. by S. $\frac{1}{2}$ S. $\psi = -19^{\circ} 58'$ |
| 3. At W. by S. $\frac{1}{2}$ S. $\psi = -47^{\circ} 17'$ | 6. At E. by S. $\frac{3}{4}$ S. $\psi = -20^{\circ} 22'$ |

$$\left. \begin{array}{l} \text{From 1. and 4. we have } \psi = \frac{\psi + \psi}{2} = -33^{\circ} 27' \cdot 5 \\ \text{From 3. and 5. we have } \psi = \frac{\psi + \psi}{2} = -33^{\circ} 37' \cdot 5 \end{array} \right\} \text{Mean } -33^{\circ} 32' \cdot 5.$$

Hence

$$\begin{array}{ll} \delta_1 = -12^{\circ} 29' \cdot 5 & \delta_4 = +12^{\circ} 41' \cdot 5 \\ \delta_2 = -12^{\circ} 59' \cdot 5 & \delta_5 = +13^{\circ} 34' \cdot 5 \\ \delta_3 = -13^{\circ} 44' \cdot 5 & \delta_6 = +13^{\circ} 10' \cdot 5 ; \end{array}$$

and having thereby the values of  $\zeta$ , as we have those of  $\zeta'$  by observation, we obtain

$$\begin{array}{ll} a_1 = + \cdot 0249 & a_4 = + \cdot 0259 \\ a_2 = + \cdot 0274 & a_5 = + \cdot 0275 \\ a_3 = + \cdot 0274 & a_6 = + \cdot 0266 \\ \text{Means . . . } \underline{\underline{+ \cdot 0266}} & \underline{\underline{+ \cdot 0267}} \end{array}$$

The deviation of the compass observed on board the Erebus during the stay of the Expedition at Christmas Harbour, Kerguelen Island, in July 1840, when the ship's head was on the N.E., S.E., N.W., and S.W. points, and at the points on either side of those points, viz. N.E. by N., N.E. by E., S.E. by S., S.E. by E., &c., will furnish an additional determination of the value of  $b$ :

	$\delta$ .	$\zeta'$ .	$\zeta$ .
N.W. by N.	-2.12	33 45	31 33
N.W.	-2.07	45 00	42 53
N.W. by W.	-2.42	56 15	53 33
S.W. by W.	-3.52	123 45	119 53
S.W.	-3.28	135 00	131 32
S.W. by S.	-2.38	146 15	143 37
S.E. by S.	+2.45	213 45	216 30
S.E.	+3.16	225 00	228 16
S.E. by E.	+3.47	236 15	240 02
N.E. by E.	+2.08	303 45	305 53
N.E.	+2.05	315 00	317 05
N.E. by N.	+1.27	326 15	327 42

Employing these values of  $\zeta'$  and  $\zeta$  in the formula

$$\cos \zeta \sin \zeta' - b \cos \zeta' \sin \zeta + a \tan \theta \sin \zeta' = 0,$$

and eliminating  $a \tan \theta \sin \zeta'$ , we have

$$5.7471 b = 5.6233; \quad b = .9785.$$

Collecting now in one view the values of  $a$ , we have as follows:—

1. From the observations at Gillingham near Chatham  $a = +.0264$
2. From the observations at Hobarton . . . . .  $a = +.0272$
3. From the observations at Auckland Island . . .  $a = +.0263$
4. From the observations in lat.  $-68^\circ 30'$ , long.  $176^\circ 35'$   $a = +.0267$

Mean. . . . +.0267

From this near accordance in the values of  $a$ , obtained in dips varying from  $+69^\circ 05'$  to  $-83^\circ 35'$ , we are warranted in regarding the local attraction in the Erebus as due to induced magnetism; and in employing the formulæ derived from M. POISSON'S fundamental equations, which are based on the hypothesis of induced magnetism only, in computing corrections for the observations made on board that ship.

For the value of  $b$  we have

- From the observations at Gillingham . . . . .  $b = +.9874$
- From the observations at Hobarton . . . . .  $b = +.9865$
- From the observations at Kerguelen Island . . .  $b = +.9785$

Mean . . . +.9841

With these values of  $a$  and  $b$ , a table of double entry was formed, having for arguments  $\zeta'$  and  $\theta$ ;  $\zeta'$  being the compass direction of the ship's head when an azimuth was observed, and  $\theta$  the inclination taken from the chart formed from the observations of that element on board ship, corrected in the manner that will be shown hereafter; the corrections for the ship's local attraction in the general Table of Declinations observed in the Erebus have been taken from the Table thus formed.

In geographical positions, where the inclination made a very near approximation to  $-90^\circ$ , and when azimuths observed on the same day at places sufficiently near to each other included observations on the east and west points, or on points but little removed from them, on which the corrections for the deviation might have the same, or nearly the same, value, but with opposite signs, the inclination with which the corrections have been computed has been derived from the azimuths themselves in preference to being taken from the chart. In such cases, and when  $a$  and  $b$  have been elsewhere satisfactorily determined for the ship, the amount of disturbance which her iron produces on the compass needle furnishes itself a measure of the inclination, exceeding in precision that of the dipping needle used on board. If the ship's magnetism should have already conformed to the terrestrial dip, the inclination corresponding to the disturbance of the compass is that belonging to the geographical position, and the ship herself, with merely her compass needle, would become in such rare situations an inclinometer of great delicacy. But if the change in the magnetism of the ship from that due to a former magnetic locality be not yet fully developed, the inclination thus furnished by the compass needle is on that account also preferable to that which might be taken from the chart, or to the dip observed with the dipping needle either on board or on shore, for the correction of other azimuths observed at the same time. Whenever the inclination used for the declination corrections has been thus derived, a notice is annexed in its proper place in the general table. It may be useful to give an example, and I select for that purpose the observations on the afternoon of the 16th February 1841, when, from the amount of the declination ( $-112^\circ$  or  $-113^\circ$ ), the Expedition had without doubt penetrated to the south of the latitude of the magnetic pole; the particular observations are as follow:—

Latitude.	Longitude.	Ship's head. Z'.	Declination observed. ψ'.
$-76^\circ 35'$	$166^\circ 17'$	E. by S. $\frac{1}{2}$ S.	$-64^\circ 23'$
$76^\circ 36'$	$166^\circ 17'$	N.N.W. $\frac{1}{2}$ W.	$-136^\circ 19'$
$-76^\circ 36'$	$166^\circ 17'$	W.N.W.	$-150^\circ 04'$
$-76^\circ 36'$	$166^\circ 16'$	N.W. by N.	$-138^\circ 24'$
$-76^\circ 36'$	$166^\circ 16'$	W.	$-158^\circ 51'$
$-76^\circ 36'$	$166^\circ 16'$	W. by S. $\frac{1}{2}$ S.	$-156^\circ 58'$
$-76^\circ 36'$	$166^\circ 16'$	S.W. $\frac{1}{4}$ W.	$-156^\circ 05'$
$-76^\circ 36'$	$166^\circ 17'$	S.W. by N.	$-154^\circ 06'$
$-76^\circ 36'$	$166^\circ 17'$	S.W. $\frac{1}{4}$ S.	$-142^\circ 54'$
$-76^\circ 37'$	$166^\circ 16'$	E.N.E.	$-67^\circ 01'$
$-76^\circ 37'$	$166^\circ 16'$	E. by S.	$-67^\circ 53'$
$-76^\circ 37'$	$166^\circ 16'$	E. by S.	$-66^\circ 32'$
$-76^\circ 37'$	$166^\circ 16'$	E.S.E.	$-73^\circ 45'$
$-76^\circ 37'$	$166^\circ 35'$	S.E. by E.	$-73^\circ 40'$

From the observations at W., and E. by S., we have the approximate values of  $\psi = \frac{\psi' + \psi'}{2} = -113^\circ 01'$ ;  $\delta$  at W. =  $-45^\circ 50'$ ;  $\tan \theta = \frac{\sin \delta}{.0267}$ ; whence  $\theta = -87^\circ 52'$ .

With this approximate inclination we compute  $\delta$  at E. by S. =  $+45^{\circ} 04'$ ; and with this correction, and the same observations as before, we have more precisely

$$\psi = -112^{\circ} 38'; \delta \text{ at W.} = -46^{\circ} 13'; \text{ and } \theta = -87^{\circ} 53'.$$

Substituting this value of  $\theta$  in the formula

$$\sin \delta = \frac{2a}{1+b} \tan \theta \sin \zeta' + \frac{1-b}{1+b} \sin (\zeta' + \zeta),$$

we have the corrections and the corrected declination as follows:—

E. by S. $\frac{1}{2}$ S.	Correction $-46^{\circ} 03'$ ;	$\psi' = -64^{\circ} 23'$ ;	$\psi = -108^{\circ} 26'$
N.N.W. $\frac{1}{2}$ W.	Correction $+19^{\circ} 46'$ ;	$\psi' = -136^{\circ} 19'$ ;	$\psi = -116^{\circ} 33'$
N.N.W.	Correction $+41^{\circ} 38'$ ;	$\psi' = -150^{\circ} 04'$ ;	$\psi = -108^{\circ} 26'$
N.W. by N.	Correction $+23^{\circ} 31'$ ;	$\psi' = -138^{\circ} 24'$ ;	$\psi = -114^{\circ} 53'$
W.	Correction $+46^{\circ} 13'$ ;	$\psi' = -158^{\circ} 51'$ ;	$\psi = -112^{\circ} 38'$
W. by S. $\frac{1}{2}$ S.	Correction $+44^{\circ} 03'$ ;	$\psi' = -156^{\circ} 58'$ ;	$\psi = -112^{\circ} 55'$
S.W. $\frac{1}{4}$ W.	Correction $+33^{\circ} 04'$ ;	$\psi' = -156^{\circ} 05'$ ;	$\psi = -123^{\circ} 01'$
S.W. by W.	Correction $+37^{\circ} 32'$ ;	$\psi' = -154^{\circ} 06'$ ;	$\psi = -116^{\circ} 34'$
S.W. $\frac{1}{4}$ S.	Correction $+29^{\circ} 45'$ ;	$\psi' = -142^{\circ} 54'$ ;	$\psi = -113^{\circ} 09'$
E.N.E.	Correction $-41^{\circ} 38'$ ;	$\psi' = -67^{\circ} 01'$ ;	$\psi = -108^{\circ} 39'$
E. by S.	Correction $-45^{\circ} 19'$ ;	$\psi' = -66^{\circ} 32'$ ;	$\psi = -111^{\circ} 51'$
E. by S.	Correction $-45^{\circ} 19'$ ;	$\psi' = -67^{\circ} 53'$ ;	$\psi = -113^{\circ} 12'$
E.S.E.	Correction $-42^{\circ} 18'$ ;	$\psi' = -73^{\circ} 45'$ ;	$\psi = -116^{\circ} 03'$
S.E. by E.	Correction $-37^{\circ} 32'$ ;	$\psi' = -73^{\circ} 40'$ ;	$\psi = -111^{\circ} 12'$
			Mean . . . $-113^{\circ} 23'$

On comparing the values of  $\psi$  thus obtained from the observations on the easterly points, with those on the westerly points, it is evident that the remaining differences in the individual results are not occasioned by faults in the corrections, but that they are actual differences in the observations of azimuth. In the extreme circumstances to which the Expedition had attained, when by reason of the great amount of dip, the terrestrial force acting on the compass needle, and directing it to one part of the horizon in preference to another, was reduced to  $\frac{1}{27}$ th part of the whole amount of the terrestrial magnetic force in the same locality, the degree of accordance which was still preserved assuredly surpasses expectation\*. The result at S.W.  $\frac{1}{4}$  W. is the only one which presents an excessive discordance; and after a careful examination of the whole of the observations which the general table contains, it must be regarded

\* The compass used in the Erebus was the first of the new naval compasses made under the direction of a Committee appointed by the Admiralty "for the improvement of ships' compasses." The magnet was composed of several thin plates of clock-spring suitably arranged, giving very considerable magnetic force, with a suspension improved both in mode and materials. This compass appears to have answered remarkably well in the very trying circumstances in which it was employed. Captain Ross was himself the Chairman of the Committee, which gave its services gratuitously: the other members were Captain BEAUFORT, R.N., Mr. CHRISTIE, Major JERVIS, Captain EDWARD JOHNSON, R.N., and Lieut.-Colonel SABINE.

as a case of very unusual observation error. Were we to omit this result, the mean would become  $-112^{\circ} 39'$ . When the corrections for local attraction become so great, it is necessary to be very accurate in noting the direction of the ship's head at the same instant that the azimuth is observed, as at the points where the changes of  $\delta$  for changes of  $\zeta'$  are very great, an error of a degree in the direction of the ship's head will make nearly the same error in the correction; on such occasions therefore the result is liable to an additional source of observation error of serious magnitude.

We have seen that when the inclination is  $-87^{\circ} 53'$ , the sum of the deviations at east and west amounted to  $92^{\circ} 26'$ ; with  $10'$  increase in the dip, their joint amount would have become  $126^{\circ} 52'$ . The scale which the compass needle presents for the deduction of the inclination is consequently a very large one, when the inclination is so great as that which we are now considering; and it continues to increase in magnitude, until the compass ceases altogether to indicate the direction of the horizontal component of the terrestrial force, and points unchangingly, under every alteration of the ship's head, to the direction of the general resultant of the ship.

The terrestrial dip observed with a dipping-needle on board on the 16th of February, and corrected for the ship's attraction, was  $-88^{\circ} 20'$ ; that corresponding to the magnetism of the ship was, as we have seen,  $-87^{\circ} 53'$ , being a little in arrear, in a magnetic sense, of her then position.

For the constants  $c$  and  $d$  in the formula for the correction of the inclination, we have to take into account, in the first instance, a series of observations of the inclination with the ship's head successively on the sixteen principal points of the compass, made on board the Erebus at Hobarton in November 1840, before her departure for the Antarctic Circle, and a similar series made at the same place in June 1841 on her return from the south. The inclination observed on shore was  $-70^{\circ} 40'$ .

Ship's head by compass.	Inclination observed.			Ship's head by compass.	Inclination observed.		
	1840.	1841.	Mean.		1840.	1841.	Mean.
N.	$-71^{\circ} 52'$	$-71^{\circ} 59'$	$-71^{\circ} 55.5'$	S.	$-69^{\circ} 49'$	$-69^{\circ} 19'$	$-69^{\circ} 34'$
N.N.W.	$-71^{\circ} 55'$	$-72^{\circ} 00'$	$-71^{\circ} 57.5'$	S.S.E.	$-70^{\circ} 00'$	$-69^{\circ} 41'$	$-69^{\circ} 50.5'$
N.W.	$-72^{\circ} 03'$	$-71^{\circ} 45'$	$-71^{\circ} 54.0'$	S.E.	$-70^{\circ} 22'$	$-70^{\circ} 04'$	$-70^{\circ} 13'$
W.N.W.	$-71^{\circ} 30'$	$-71^{\circ} 24'$	$-71^{\circ} 27'$	E.S.E.	$-70^{\circ} 45'$	$-70^{\circ} 33'$	$-70^{\circ} 39'$
W.	$-71^{\circ} 16'$	$-70^{\circ} 55'$	$-71^{\circ} 05.5'$	E.	$-70^{\circ} 58'$	$-71^{\circ} 08'$	$-71^{\circ} 03'$
W.S.W.	$-70^{\circ} 55'$	$-70^{\circ} 30'$	$-70^{\circ} 42.5'$	E.N.E.	$-71^{\circ} 33'$	$-71^{\circ} 32'$	$-71^{\circ} 32.5'$
S.W.	$-70^{\circ} 20'$	$-69^{\circ} 56'$	$-70^{\circ} 08.5'$	N.E.	$-71^{\circ} 35'$	$-71^{\circ} 57'$	$-71^{\circ} 46'$
S.S.W.	$-70^{\circ} 07'$	$-69^{\circ} 44'$	$-69^{\circ} 55.5'$	N.N.E.	$-71^{\circ} 42'$	$-71^{\circ} 56'$	$-71^{\circ} 49'$

Employing for the observations between N.N.W. and S.S.W., and N.N.E. and S.S.E. the formula

$$c \cos \zeta + d \tan \theta = b \sin \zeta \operatorname{cosec} \zeta' \tan \theta',$$

and for the other points

$$c \cos \zeta + d \tan \theta = (\cos \zeta + a \tan \theta) \sec \zeta' \tan \theta',$$

and using the values of  $\zeta$  computed by means of the constants  $a$  and  $b$  already determined, we have the following equations:—

N. + 1·0000 $c$ - 2·850 $d$ = - 2·830	S. - 1·0000 $c$ - 2·850 $d$ = - 2·888
N.N.W. + ·9327 $c$ - 2·850 $d$ = - 2·845	S.S.E. - ·9110 $c$ - 2·850 $d$ = - 2·906
N.W. + ·7351 $c$ - 2·850 $d$ = - 2·868	S.E. - ·6617 $c$ - 2·850 $d$ = - 2·902
N.S.W. + ·4418 $c$ - 2·850 $d$ = - 2·848	E.S.E. - ·3139 $c$ - 2·850 $d$ = - 2·880
W. + ·0761 $c$ - 2·850 $d$ = - 2·864	E. + ·0761 $c$ - 2·850 $d$ = - 2·858
W.S.W. - ·3139 $c$ - 2·850 $d$ = - 2·889	E.N.E. + ·4418 $c$ - 2·850 $d$ = - 2·862
S.W. - ·6617 $c$ - 2·850 $d$ = - 2·922	N.E. + ·7351 $c$ - 2·850 $d$ = - 2·845
S.S.W. - ·9110 $c$ - 2·850 $d$ = - 2·888	N.N.E. + ·9327 $c$ - 2·850 $d$ = - 2·822

Summing these equations,  $c$  is eliminated, and  $d = \frac{45·917}{45·604} = 1·0069$ ; and changing the signs in the equations from W. to E.S.E. inclusive and summing, we have  $c = \frac{+·361}{9·9924} = +·0361$ .

A similar series of observations made at Auckland Island on the passage from Hobarton to the Antarctic Circle, furnishes values of  $c$  and  $d$  differing but slightly from the preceding. The inclination observed on shore was  $- 73^\circ 10'$ .

Ship's head by compass.	Inclination observed.	Ship's head by compass.	Inclination observed.
N.	$-74^\circ 24'$	S.	$-72^\circ 00'$
N.N.W.	$-74 34$	S.S.W.	$-72 17$
N.N.E.	$-74 09$	S.S.E.	$-72 05$
N.W.	$-74 16$	S.W.	$-72 36$
N.E.	$-74 13$	S.E.	$-72 38$
W.N.W.	$-74 08$	W.S.W.	$-73 09$
E.N.E.	$-73 43$	E.S.E.	$-73 02$
W.	$-73 32$	E.	$-73 26$

Treating these observations in a similar manner to those at Van Diemen Island, we obtain

$$c = +·045; d = + 1·0039.$$

Giving double weight to the observations at Hobarton, as representing a double series, we have  $c = +·039$ ; and  $d = + 1·006$ .

With these values of the constants in the formulæ

$$\tan \theta' = \frac{c}{b} \left( \frac{d}{c} \tan \theta + \cos \zeta \right) \sin \zeta' \operatorname{cosec} \zeta, \text{ from N.E. to S.E., and from N.W. to S.W.}$$

$$\tan \theta' = c \frac{\left( \frac{d}{c} \tan \theta + \cos \zeta \right) \cos \zeta'}{a \tan \theta + \cos \zeta} \text{ on other points,}$$

a table of double entry was formed for the corrections of the observations of in-



clination in the Erebus, having for arguments  $\theta$  and  $\zeta'$ ; the corrections in the general Table of the inclination observations were thus obtained.

We may compute the value of the remaining constant  $A'$  from the variations of the magnetic intensity observed on board the Erebus at Hobarton with Mr. Fox's intensity apparatus, with the ship's head on the sixteen principal points of the compass; two series of such observations were made, one in October 1840 with needle R. F. 4, the other in July 1841 with needle R. F. 5; expressing the value of the intensity on shore by  $1.82 = \phi$ , the several values on board ship are shown in the following Table:—

Ship's head by compass.	Intensity.		
	October 1840.	July 1841.	Means.
N.	1.792	1.806	1.799 1.799 = $\phi'$
N.N.E.	1.787	1.803	1.795 } 1.835 = $\phi'$
N.N.W.	1.807	1.818	1.812 }
N.E.	1.789	1.813	1.801 } 1.805 = $\phi'$
N.W.	1.803	1.816	1.809 }
E.N.E.	1.816	1.821	1.818 } 1.8245 = $\phi'$
W.N.W.	1.830	1.832	1.831 }
E.	1.828	1.823	1.826 } 1.828 = $\phi'$
W.	1.832	1.829	1.830 }
E.S.E.	1.830	1.829	1.830 } 1.836 = $\phi'$
W.S.W.	1.848	1.837	1.842 }
S.E.	1.842	1.853	1.848 } 1.853 = $\phi'$
S.W.	1.862	1.855	1.858 }
S.S.E.	1.858	1.859	1.859 } 1.8595 = $\phi'$
S.S.W.	1.863	1.857	1.860 }
S.	1.864	1.864	1.864 1.864 = $\phi'$

Employing the formula

$$\frac{\phi'}{A' \phi} \sin \theta' = c \cos \theta \cos \zeta + d \sin \theta$$

with the values of  $\theta'$  and  $\zeta$  computed by means of the constants  $a$ ,  $b$ ,  $c$  and  $d$ , already deduced, and with the observed values of  $\phi$ ,  $\theta$ , and  $\phi'$ , we have  $A'$  as follows:—

At	N.	$A' = 0.997$
At	N.N.E. and N.N.W.	$A' = 0.996$
At	N.E. and N.W.	$A' = 0.998$
At	E.N.E. and W.N.W.	$A' = 0.993$
At	E. and W.	$A' = 0.998$
At	E.S.E. and W.S.W.	$A' = 1.002$
At	S.E. and S.W.	$A' = 1.000$
At	S.S.E. and S.S.W.	$A' = 1.002$
At	S.	$A' = 1.002$
	Mean. . . .	<u>0.999</u>

We obtain the same result if we employ the *observed* values of  $\theta'$  instead of the

computed values; in this case the inclination and total intensity being both furnished at the several points by observation with Mr. Fox's apparatus, we have the ratios of the horizontal intensity  $\frac{\phi' \cos \theta'}{\phi \cos \theta}$  on board as follows:—

N.	= 0·9262;	E.N.E. }	= 0·9608;	S.S.E. }	= 1·0615;
N.N.E. }	= 0·9308;	W.N.W. }	= 0·9608;	S.S.W. }	= 1·0615;
N.N.W. }	= 0·9340;	E. }	= 0·9838;	S.E. }	= 1·0432;
N.E. }	= 0·9340;	W. }	= 0·9838;	S.W. }	= 1·0432;
N.W. }	= 0·9340;	S.	= 1·0800;	E.S.E. }	= 1·0084;
				W.S.W. }	= 1·0084;

From which by the formula

$$H = A' (\cos \zeta \cos \zeta' + b \sin \zeta \sin \zeta' + a \tan \theta \cos \zeta'),$$

we have

$$\text{At N.} \quad A' = \frac{0\cdot9262}{0\cdot9239} = 1\cdot003$$

$$\text{At N.N.E. and N.N.W.} \quad A' = \frac{0\cdot9308}{0\cdot9270} = 1\cdot004$$

$$\text{At N.E. and N.W.} \quad A' = \frac{0\cdot9340}{0\cdot9374} = 0\cdot996$$

$$\text{At E.N.E. and W.N.W.} \quad A' = \frac{0\cdot9608}{0\cdot9555} = 1\cdot006$$

$$\text{At E. and W.} \quad A' = \frac{0\cdot9838}{0\cdot9917} = 0\cdot992$$

$$\text{At E.S.E. and W.S.W.} \quad A' = \frac{1\cdot0084}{1\cdot0122} = 0\cdot996$$

$$\text{At S.E. and S.W.} \quad A' = \frac{1\cdot0432}{1\cdot0433} = 0\cdot999$$

$$\text{At S.S.E. and S.S.W.} \quad A' = \frac{1\cdot0615}{1\cdot0673} = 0\cdot994$$

$$\text{At S.} \quad A' = \frac{1\cdot0800}{1\cdot0761} = 1\cdot004$$

$$A' = 0\cdot999 \text{ Mean.}$$

The correction for the ship's attraction in the general table of the intensities observed in the Erebus, have been computed with this value of  $A'$  used in the formula  $A' \bar{c} \left( \frac{d}{c} \tan \theta + \cos \zeta \right) \cos \theta \operatorname{cosec} \theta'$ ;  $\theta$  being taken from the chart formed from the observations of the inclination, and  $\theta'$  and  $\zeta$  from the tables with the arguments  $\theta$  and  $\zeta'$ .

*Deduction of the Constants in Her Majesty's Ship Terror.*—For these we have, in the first place, the observations at Gillingham, in September 1839, as follows :  $\theta = 69^{\circ} 05'$ .

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N.	+0.11	w.	+5.55	s.	-0.8	E.	-5.22
N. by w.	+1.35	w. by s.	+5.17	s. by E.	-0.51	E. by N.	-5.50
N.N.W.	+2.31	w.s.w.	+4.39	s.s.E.	-1.42	E.N.E.	-5.22
N.w. by N.	+3.9	s.w. by w.	+3.50	s.E. by s.	-2.30	N.E. by E.	-4.27
N.W.	+3.58	s.w.	+3.8	s.E.	-3.9	N.E.	-3.37
N.W. by w.	+4.39	s.w. by s.	+2.24	s.E. by E.	-3.40	N.E. by N.	-2.37
W.N.W.	+5.8	s.s.w.	+1.38	E.S.E.	-4.34	N.N.E.	-1.40
w. by N.	+5.35	s. by w.	+0.55	E. by s.	-4.57	N. by E.	-0.33

We perceive by this Table that the masses of iron acting on the compass needle of the Terror were distributed, as in the Erebus, symmetrically, or very nearly so, on either side of the vertical plane passing through the longitudinal midship section. Using the formula

$$\cos \zeta \sin \zeta' - b \sin \zeta \cos \zeta' = a \tan \theta \sin \zeta',$$

and forming equations for the several points, we have from the sum of those from N. by W. to W. by N., and from N. by E. to E. by N.,

$$- 4.4516 + 5.3295 b = + 23.946 a ;$$

and for the sum of the equations on the points from S. by W. to W. by S., and from S. by E. to E. by S.,

$$- 5.5092 + 4.7551 b = - 23.946 a ,$$

whence we derive  $b = + .9877$ , and  $a = + .0339$  ; or including the observations at east and west  $a = .0343$ .

We have next to consider a similar series of observations made in the River Derwent, near Hobarton, in Van Diemen Island, on October 20th, 1840, soon after the first arrival of the Expedition at that station ; they were as follows :—

Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.	Ship's head by compass.	Attraction towards the west.
N.	+0 42.4	w.	-4 36.6	s.	-0 11.6	E.	+4 24.4
N. by w.	-0 23.6	w. by s.	-4 44.6	s. by E.	+0 52.4	E. by N.	+4 11.4
N.N.W.	-1 20.6	w.s.w.	-4 52.6	s.s.E.	+1 56.4	E.N.E.	+4 07.4
N.w. by N.	-2 20.6	s.w. by w.	-5 22.6	s.E. by s.	+2 38.4	N.E. by E.	+3 27.4
N.W.	-3 25.6	s.w.	-4 23.6	s.E.	+3 29.4	N.E.	+3 02.4
N.W. by w.	-3 56.6	s.w. by s.	-3 31.6	s.E. by E.	+4 00.4	N.E. by N.	+2 37.4
W.N.W.	-4 01.6	s.s.w.	-2 03.6	E.S.E.	+4 43.4	N.N.E.	+2 11.4
w. by N.	-4 06.6	s. by w.	-1 37.6	E. by s.	+4 28.4	N. by E.	+1 26.4

In the Terror, as in the Erebus, the disturbance had changed its sign in passing from the northern to the southern hemisphere : the symmetrical distribution of the

iron on either side of the principal axis of the ship continued as at Gillingham, the observations showing only those very small differences in the exact points of no disturbance, which have been remarked in the Erebus, and which we may be content to view as accidental differences. From these observations, pursuing the usual course, we obtain  $b = + \cdot 9873$ , and  $a = + \cdot 0292$ . Here also, as in the case of the Erebus, the observations on the first arrival at Hobarton give a somewhat less value for  $a \tan \theta$  than those at Gillingham. It is possible that a similar series of experiments may have been repeated in the Terror on the return to the same station in 1841, but no record of it has been received in England, and the observations of 1840 are expressly referred to, in a note appended to them, as furnishing the corrections for the declinations observed between the months of October 1840 and April 1841. I think it not improbable that if the ship were swung in 1841, the resulting value of  $a \tan \theta$  will prove, as in the Erebus, to be somewhat greater than in 1840, and that the mean value of  $a$  at Hobarton will thereby come into a closer accord with its value at Gillingham.

The practical effect of so small a difference is however unimportant, and I have taken  $a$  in round numbers for the declinations under consideration =  $+ \cdot 030$ , and  $b = + \cdot 9875$ , and have computed with these values the Tables from which the corrections for the Terror's declinations have been taken.

Part of the materials required for the correction of the observations of inclination and intensity, made in the Terror during the voyage under notice, not having yet reached England, the deduction of the constants  $c$ ,  $d$ , and  $A'$  for that ship has been postponed.

*Index Correction of Needle R. F. 4 for the Observations of the Inclination in the Erebus.*—The observations of the inclination at sea on board the "Erebus," were made with Mr. Fox's apparatus for determining the magnetic inclination and intensity, and one needle, R. F. 4, was used throughout the observations which are now under consideration. The poles were not reversed; the circle was used with the face east only, and the needle with its marked side towards the observer. An index correction is therefore required for all the sea observations, and must be sought by comparing the inclination shown by the same circle and needle when observed with in the same manner on shore, at stations where the inclination was otherwise determined in an independent and complete manner, viz. by needles of which the poles were reversed, and the needle and circle used in the eight ordinary positions.

The determinations of this description made by the Expedition at the Magnetic Observatory at Van Diemen Island in 1840 and 1841, at Auckland Island in November and December 1840, at Campbell's Island in December 1840, and on the ice in lat.  $- 68^{\circ} 28'$ , long.  $176^{\circ} 32'$ , on the 8th of January 1841,—furnishing the required comparison,—were as follows:—

## Observations of the Inclination, with Needles whose Poles were reversed, made at the Magnetic Observatory in Van Diemen Island in 1840, 1841.

Date.	Hour.	Needle.	Poles. $\alpha$ direct. $\beta$ reversed.	Mean.	Remarks.	
1840. September 12.	h m 11 00 A.M.	R G 1	$\alpha -70 \ 32.1$ $\beta -70 \ 42.1$	$-70 \ 37.1$	} Needles belonging to H.M.S. Erebus.	
14.	11 20 A.M.	R G 2	$\alpha -70 \ 35.6$ $\beta -70 \ 40.9$	$-70 \ 38.2$		
21.	11 30 A.M.	R 4	$\alpha -70 \ 39.7$ $\beta -70 \ 35.5$	$-70 \ 37.6$		
21.	1 30 P.M.	R 10	$\alpha -70 \ 49.8$ $\beta -70 \ 53.7$	$-70 \ 51.7$		
22.	11 20 A.M.	R 6	$\alpha -70 \ 46.5$ $\beta -70 \ 45.2$	$-70 \ 45.8$		
22.	2 00 P.M.	R 7	$\alpha -70 \ 46.4$ $\beta -70 \ 45.2$	$-70 \ 45.8$		
October 5.	11 00 A.M.	R 6	$\alpha -70 \ 42.4$ $\beta -70 \ 44.0$	$-70 \ 43.2$		} Needles belonging to Sir JOHN FRANKLIN.
5.	2 00 P.M.	R 7	$\alpha -70 \ 43.3$ $\beta -70 \ 40.4$	$-70 \ 42.0$		
15.	2 00 P.M.	D 1	$\alpha -70 \ 31.4$ $\beta -71 \ 11.1$	$-70 \ 51.2$		
16.	11 00 A.M.	D 2	$\alpha -70 \ 08.4$ $\beta -71 \ 06.4$	$-70 \ 37.4$		} Needles belonging to H.M.S. Terror.
19.	10 20 A.M.	C 1	$\alpha -70 \ 42.0$ $\beta -70 \ 34.5$	$-70 \ 38.3$		
19.	11 00 A.M.	C 2	$\alpha -70 \ 34.3$ $\beta -70 \ 41.2$	$-70 \ 37.7$		
1841. April 14.	11 20 A.M.	R 4	$\alpha -70 \ 38.6$ $\beta -70 \ 38.8$	$-70 \ 38.7$	} Needles belonging to H.M.S. Erebus.	
14.	2 00 P.M.	R 10	$\alpha -70 \ 46.5$ $\beta -70 \ 39.3$	$-70 \ 42.9$		
15.	10 50 A.M.	R 6	$\alpha -70 \ 34.7$ $\beta -70 \ 43.3$	$-70 \ 39.0$		
15.	3 30 P.M.	R 7	$\alpha -70 \ 40.6$ $\beta -70 \ 33.9$	$-70 \ 37.2$		
16.	1 30 P.M.	R G 1	$\alpha -70 \ 34.4$ $\beta -70 \ 38.2$	$-70 \ 36.3$		
17.	11 20 A.M.	R G 2	$\alpha -70 \ 35.7$ $\beta -70 \ 39.0$	$-70 \ 37.3$		
24.	11 00 A.M.	C 1	$\alpha -70 \ 41.1$ $\beta -70 \ 35.0$	$-70 \ 38.0$		} Needles belonging to H.M.S. Terror.
24.	Noon.	C 1	$\alpha -70 \ 49.3$ $\beta -70 \ 37.0$	$-70 \ 43.1$		
24.	2 00 P.M.	C 2	$\alpha -70 \ 36.9$ $\beta -70 \ 31.9$	$-70 \ 34.4$		
30.	Noon.	C 1	$\alpha -70 \ 31.2$ $\beta -70 \ 41.7$	$-70 \ 36.4$		
30.	Noon.	C 2	$\alpha -70 \ 33.0$ $\beta -70 \ 46.0$	$-70 \ 39.5$		
May 10.	2 20 P.M.	R 4	$\alpha -70 \ 46.6$ $\beta -70 \ 39.1$	$-70 \ 42.9$	} Needles belonging to H.M.S. Erebus.	
10.	4 15 P.M.	R 10	$\alpha -70 \ 53.9$ $\beta -70 \ 34.0$	$-70 \ 43.9$		
11.	10 30 A.M.	R 4	$\alpha -70 \ 46.2$ $\beta -70 \ 38.6$	$-70 \ 42.4$		
18.	10 45 A.M.	R 4	$\alpha -70 \ 45.4$ $\beta -70 \ 36.3$	$-70 \ 40.9$		
18.	2 15 P.M.	R 10	$\alpha -70 \ 47.1$ $\beta -70 \ 33.1$	$-70 \ 40.5$		
June 21.	9 45 A.M.	R 10	$\alpha -70 \ 45.8$ $\beta -70 \ 35.1$	$-70 \ 40.4$		
21.	10 45 A.M.	R 4	$\alpha -70 \ 45.1$ $\beta -70 \ 36.5$	$-70 \ 40.8$		
				$-70 \ 40.7$	General Mean.	

Observations of the Inclination with Needles whose poles were reversed, made at the  
Magnetic Observatory at Auckland Island.

Date.	Hour.	Needle.	Poles. $\alpha$ direct. $\beta$ reversed.	Mean.	Remarks.	
1840. November 23.	h m 10 20 A.M.	R 4	$\alpha -73 \overset{\circ}{17} \cdot 9$ $\beta -73 \overset{\circ}{08} \cdot 2$	} $-73 \overset{\circ}{13} \cdot 1$	} Needles belonging to H.M.S. Erebus.	
23.	1 00 P.M.	R 10	$\alpha -73 \overset{\circ}{14} \cdot 4$ $\beta -73 \overset{\circ}{12} \cdot 4$			} $-73 \overset{\circ}{13} \cdot 4$
23.	2 40 P.M.	R 6	$\alpha -73 \overset{\circ}{15} \cdot 7$ $\beta -73 \overset{\circ}{12} \cdot 9$	} $-73 \overset{\circ}{14} \cdot 3$		
23.	3 30 P.M.	R 7	$\alpha -73 \overset{\circ}{14} \cdot 7$ $\beta -73 \overset{\circ}{11} \cdot 6$			} $-73 \overset{\circ}{13} \cdot 2$
25.	11 00 A.M.	R G 1	$\alpha -73 \overset{\circ}{06} \cdot 6$ $\beta -73 \overset{\circ}{17} \cdot 0$	} $-73 \overset{\circ}{11} \cdot 8$		
25.	1 00 P.M.	R G 2	$\alpha -73 \overset{\circ}{04} \cdot 0$ $\beta -73 \overset{\circ}{11} \cdot 6$			} $-73 \overset{\circ}{07} \cdot 8$
27.	3 00 P.M.	C 1	$\alpha -73 \overset{\circ}{08} \cdot 7$ $\beta -73 \overset{\circ}{02} \cdot 9$	} $-73 \overset{\circ}{05} \cdot 8$		
27.	4 00 P.M.	C 2	$\alpha -73 \overset{\circ}{08} \cdot 2$ $\beta -72 \overset{\circ}{55} \cdot 5$			} $-73 \overset{\circ}{01} \cdot 8$
December 4.	1 40 P.M.	R G 1		} $-73 \overset{\circ}{12} \cdot 2$		
				$-73 \overset{\circ}{10} \cdot 4$		General Mean.

Observations of the Inclination with Needles whose poles were reversed, at Campbell  
Island.

Date.	Hour.	Needle.	Poles. $\alpha$ direct. $\beta$ reversed.	Mean.	Remarks.
1840. December 15.	h m 9 30 A.M.	C 1	$\alpha -73 \overset{\circ}{55} \cdot 7$ $\beta -73 \overset{\circ}{48} \cdot 4$	} $-73 \overset{\circ}{52} \cdot 1$	} Needles belonging to H.M.S. Terror.
15.	10 30 A.M.	C 2	$\alpha -73 \overset{\circ}{51} \cdot 2$ $\beta -73 \overset{\circ}{43} \cdot 4$		
15.	10 30 A.M.	R 4	$\alpha -73 \overset{\circ}{56} \cdot 5$ $\beta -73 \overset{\circ}{50} \cdot 7$	} $-73 \overset{\circ}{50} \cdot 6$	
15.	11 00 A.M.	R 10	$\alpha -74 \overset{\circ}{01} \cdot 5$ $\beta -73 \overset{\circ}{57} \cdot 2$		
15.	Noon.	R 6	$\alpha -73 \overset{\circ}{45} \cdot 8$ $\beta -73 \overset{\circ}{49} \cdot 5$	} $-73 \overset{\circ}{47} \cdot 7$	
15.	1 00 P.M.	R 7	$\alpha -73 \overset{\circ}{49} \cdot 5$ $\beta -73 \overset{\circ}{53} \cdot 3$		} $-73 \overset{\circ}{51} \cdot 4$
				$-73 \overset{\circ}{51} \cdot 4$	

Inclination observed on Ice, in latitude  $-68^{\circ} 28'$ , longitude  $176^{\circ} 32'$ , with a Needle  
the poles of which were reversed.

Date.	Hour.	Needle.	Poles. $\alpha$ direct. $\beta$ reversed.	Mean.	Remarks.
1841. January 8.	h m 3 20 P.M.	R 4	$\alpha -83 \overset{\circ}{35} \cdot 3$ $\beta -83 \overset{\circ}{35} \cdot 8$	} $-83 \overset{\circ}{35} \cdot 6$	H. M. S. Erebus.

The inclinations observed at the four preceding stations with needle R. F. 4, with the face of the circle east, and the marked side of the needle facing the observer, were as follows:—

Van Diemen Island	— 71 06.5	; true inclination	— 70 40.7	; index correction	— 25.8
Auckland Island . .	— 73 41.3	; true inclination	— 73 10.4	; index correction	— 30.9
Campbell Island . .	— 74 20.3	; true inclination	73 51.4	; index correction	— 28.9
On ice, Jan. 8, 1841	— 84 02.9	; true inclination	— 83 36.6	; index correction	— 27.3
				Mean . . .	— 28.2

An index correction of — 28' has therefore been applied in the general table to the mean of the observations on each day with needle R. F. 4, in order to give the true or correct inclination, as it would have been observed by a needle in which the complete process of observation had been gone through.

*Elements of Calculation of the Intensity Observations.*—Of the intensity observations made with Mr. Fox's apparatus on board the Erebus, during the period under consideration, a large proportion was of the angles of deflection produced by deflecting magnets. A spare needle belonging to the apparatus was used as a deflector, and was fitted into a cylindrical case having screws at both ends, so that the needle could be applied either as “deflector N” with its north pole opposite that division of the circle which the north pole of the dipping needle had previously indicated as the dip, —or as “deflector S” with its south pole similarly applied to the opposite division of the circle.

The deflectors belonging to the apparatus, being too weak to produce sufficient deflections when used separately, were employed only conjointly, and are designated as “deflectors N and S.” The angles of deflection varied in different localities during the voyage in round numbers as follows: deflector S from 50° to 45°; deflector N from 48° to 43°; and N and S from 23° to 20°.

To obtain the equivalent weight to the deflecting force of the deflectors at these angles, we have comparative observations of the angles produced by the deflectors and by weights at Hobarton, Auckland, and Campbell Islands, on the ice on the 8th January in lat. — 68° 28', long. 176° 32', and on five different occasions on board ship when the weather and other circumstances were favourable, viz. on February 8th and 10th, March 22nd, April 1st and 6th. These were exclusive of an attempt on the 1st of February, which failed on account of the ship having too much motion.

Hobarton is necessarily the primary station of the whole series of observations made in this portion of the voyage, being the only station at which an independent determination of the intensity has been made. It is also very suitable for a base station, because we may expect that the absolute as well as relative intensity will be determined with great precision at the magnetic observatory established there, and will ultimately furnish a correction, should one be needed, for the provisional value which must for the present be employed.

Captain Ross commenced the experiments for measuring the absolute horizontal intensity at Hobarton, by obtaining five results with the large magnets of his observatory magnetometers on different days whilst the Expedition was refitting there. The details of these will be published with the other magnetometric observations of the voyage; the results, which have been computed by Lieutenant GOODENOUGH of the Royal Artillery from the data received from Captain Ross, are as follows:—

October 13, 1840 . . . . .	4·491	}	Mean 4·573*.
May 3, 1841 . . . . .	4·626		
May 21, 1841 . . . . .	4·602		
June 5, 1841 . . . . .	4·579		
June 25, 1841 . . . . .	4·566		

The dip being  $-70^{\circ} 40'$  at Hobarton, and the approximate value of the absolute horizontal intensity at Woolwich  $3\cdot72\ddagger$  with the dip of  $69^{\circ} 03'$ , the corresponding value of the total intensity at Hobarton in the arbitrary scale (London =  $1\cdot372$ ) is  $1\cdot821$ . The previous *relative* observations, collected in No. I. of these Contributions, had given  $1\cdot819$  as the mean of three determinations, viz.

FITZROY . . . . .	1836	1·817	}	Mean 1·819.
FRANKLIN and	1837	1·810		
SABINE . . . . .	1838			
WICKHAM . . . . .	1838			

The closeness in the accordance of the mean results by the two methods can only be viewed as accidental, because the probable error of the absolute determination, estimated from the differences in the partial results, is far greater than the difference of the two methods; but it fully warrants  $1\cdot82$  being now taken as a provisional value of the total intensity at Hobarton, as the base station of the observations which form the subject of this number, regarding  $1\cdot82 + e$  as the true value, and  $e$  as a small correction to be determined hereafter, applicable to the whole series.

The weights employed in deflecting the intensity needle were from half a grain to six grains. It was soon found that half a grain was too small to give satisfactory results, and observations with that weight were discontinued. I have not therefore taken the observations made with it into account, except at Hobarton, where they

\* Since these pages were written I have received the results of twenty-two monthly determinations of the absolute horizontal intensity at the magnetic observatory at Hobarton (ten in 1841 and twelve in 1842) made and computed by Lieutenant KAY, R.N., and the naval officers under his direction. The mean in 1841 is  $4\cdot553$ , the partial results varying from  $4\cdot601$  to  $4\cdot509$ ; and the mean in 1842,  $4\cdot513$ , the partial results varying from  $4\cdot443$  to  $4\cdot568$ . The discordance in the partial results of these observations is scarcely less than in those of Captain Ross: there is also a considerable disagreement in the means of the three series, which may not improbably be diminished when the particulars of the several observations shall have been carefully examined, though the partial results must still be expected to differ much more widely than could be desired. It is hoped that such differences will be reduced within much smaller limits by the use of the improved apparatus which has recently been supplied to the Hobarton as well as to the other colonial observatories.

† Philosophical Transactions, 1843, Art. X.



assist in computing the angles corresponding to the weights of 4, 5, and 6 grains, which were not commenced with so soon. The observations with the weights on the days above stated, when the weights and deflecting magnets were employed in comparison, are collected in one view and given in the subjoined Table, in which are also shown the angles of deflection produced by the deflecting magnets on the same occasions.

1840.	Latitude.	Longitude.	Weights.		Thermo- meter.	Intensity deduced.	Angles of deflection by		
			Grains.	Angles of deflection.			Deflector S.	Deflector N.	Deflectors N and S.
Sept. 18.	Hobarton. -42 52   147 24		1/2	2 41.4	52	1.820	50 01	Notobserved	Notobserved.
			1	5 22.7					
			1 1/2	8 14.6					
			2	10 49.6					
			3	16 15					
			4	22 06					
Nov. 24.	Auckland Island. -50 33   166 19		1	5 18.4	52	1.844	49 29	46 50.2	Notobserved.
			1 1/2	8 02.2	1.867				
			2	10 36.8	1.856				
			3	15 58.3	1.851				
Dec. 14.	Campbell Island. -52 44   169 10		2	10 12.1	52	1.930	49 20.5	46 10.5	Notobserved.
			3	15 30.2		1.906			
15.			1	4 59.2		1.963	49 17	46 45.7	Notobserved.
			2	10 12.6		1.929			
1841.	On ice.		3	14 34.3	42	2.024	47 16	44 17	21 55
			6	30 38.7		2.015			
Feb. 8.	-77 47   187 18		2	9 15.6	32	2.124	47 03	44 23	22 03
			3	14 14.6		2.071			
			6	30 30.9		2.023			
Feb. 10.	-77 39   187 06		2	9 31	34	2.067	46 55.5	44 14	21 55.9
			3	14 37		2.019			
			6	30 34.7		2.019			
Mar. 22.	-63 09   139 28		2	9 39	40	2.040	46 54	44 22	22 00
			3	14 13		2.074			
			3	14 18.6		2.062			
			4	19 24.1		2.045			
			5	25 11.2		2.012			
April 1.	-58 13   135 18		2	9 26.2	40	2.086	46 55	44 41	22 30
			3	14 07.7		2.086			
			4	19 39.7		2.035			
			5	25 28.5		1.990			
April 6.	-43 41   146 03		6	31 08.5	58	1.987	50 01	46 40	23 17
			1	5 14.2		1.870			
			2	10 37.2		1.885			
			3	15 59.4		1.850			
			4	21 21		1.881			
			5	26 29.7		1.919			
6	32 58.5	1.887							

With the angles of deflection at Hobarton produced by the weights 1/2, 1, 1 1/2, 2 and 3 grains, we obtain the equivalent weight 8.15 grains to the angle  $v = 50^\circ 01'$  of deflector S at the same station; and thence the value of the constant  $\frac{w}{I \sin v} = 5.84$

in the formula for the equivalent weights to the force of the deflector observed elsewhere, viz.

$$w' = 5.84 I' \sin v'.$$

From the values of  $w'$  thus obtained, the subjoined Table has been formed of  $w'$  for each 20' of  $v$  for deflector N and deflector S, in the manner described in No. III. of these Contributions\*; and with these values of  $w'$  we have the intensities  $I'$  relative to the force 1.820 at Hobarton computed by means of the formula

$$I' = \frac{I \sin v}{w} \cdot w' \operatorname{cosec} v' = .171 w' \operatorname{cosec} v'.$$

Deflector S.		Deflector N.	
$v'$ .	$w'$ .	$v'$ .	$w'$ .
50 0'	gr. 8.15	47 20'	gr. 7.90
49 40	8.23	47 00	7.95
49 20	8.30	46 40	8.00
49 00	8.37	46 20	8.06
48 40	8.44	46 00	8.11
48 20	8.51	45 40	8.16
48 00	8.56	45 20	2.21
47 40	8.61	45 00	8.25
47 20	8.65	44 40	8.30
47 00	8.70	44 20	8.33
46 20	8.65	44 00	8.37

The results with the original magnets of the apparatus used conjointly, and designated as “N and S,” are much inferior in precision to those obtained with the spare intensity needle used as a deflector. The angles of deflection were much less, owing to the force of the magnets, even when used conjointly, being very much inferior to that of the spare needle. The observations are of course given in the Table with the others, but as their results present on the one hand no systematic difference from those with the stronger deflector, and on the other hand are of inferior value, by reason of the extent of their fluctuation,—and as they could only tend therefore to impair the individual accuracy of the results with the stronger deflector and with the weights,—they have been omitted in the means.

Comparison of the Intensities deduced by the Weights and by the Deflectors at the Stations at which both were employed.

Station.	Latitude.	Longitude.	Deflector S.	Deflector N.	Weights.
Auckland Island..	−50 33	166 19	1.862	1.873	1.852
Campbell Island ..	−52 41	169 10	1.875	1.898	1.927
On ice.....	−68 28	176 32	2.021	2.044	2.017
At sea.....	−77 17	187 18	2.034	2.038	2.053
At sea.....	−77 39	187 06	2.041	2.047	2.053
At sea.....	−63 00	139 28	2.043	2.039	2.041
At sea.....	−58 13	135 18	2.042	2.017	2.037
At sea.....	−43 41	146 03	1.820	1.884	1.885

\* Philosophical Transactions for 1842, Art. II.

*General Remarks.*—The Tables of the declination observations in the Erebus and Terror, and of the inclination and intensity observations in the Erebus, furnish a full opportunity, for those who may desire it, to examine how far the corrections computed in the manner which has been described fulfil their purpose.

The three charts which accompany this number of the “Contributions,” exhibit to the eye the determinations contained in the Tables, arranged in their respective localities, by which their general harmony may be, in some measure, judged of. The faint lines, representing the principal curves of the magnetic elements, are drawn in approximate conformity with the observations, and are designed merely to assist the eye in taking a first general view of the results. When the determinations of the succeeding voyages shall have been laid down in a similar manner on a south polar chart, they will furnish the means of judging of the course of the magnetic curves more comprehensively and accurately, and of tracing them accordingly.

Rather more attention has been bestowed on the lines in the chart of the inclination than in the other two charts, because it has been used for the values of  $\theta$  in the declination-corrections. Having had experience in drawing similar charts on former occasions, and particularly those of the Magnetic Survey of the British Islands, I have no hesitation in recognising with Captain Ross, that as great, and greater, discrepancies are to be looked for, and must frequently be experienced, in magnetic surveys conducted on land, than in those made at sea. The chart of the inclination which accompanies this paper, constructed from observations made at sea, and certainly not under the most favourable circumstances, except in the skill of the observers, exhibits by no means a greater measure of discrepancy than the magnetic chart of Scotland or of Ireland: and it may be further noticed, that the only results which have been excluded altogether from the chart, by reason of their excessive discordance as well with each other as with the general body of results, are some that were made on islands which presented themselves in the course of the voyage.

I cannot close this section without calling the attention of all who take interest in the results of these researches, to the invaluable aid for which magnetical science is indebted to Mr. Fox. Without his instrument and method, which render observations of inclination and intensity made at sea nearly or altogether equal to those which could be made on land or on ice, such were the difficulties of the navigation, and such the inaccessible though magnificent character of the coast that was discovered, that two of the three charts herewith presented, and especially that of the intensity, must have offered an appearance very different from that which they now exhibit.

To enter into a lengthened comparison of the results now communicated with those of preceding observers, which have been embodied in magnetic maps constructed either directly from the phenomena, or by means of the mathematical theory of M. GAUSS, would be to anticipate the more proper opportunity which will present itself, when the whole of the materials collected by the Antarctic Expedition shall be

available for the comparison. A few remarks however on prominent points may be looked for on the present occasion.

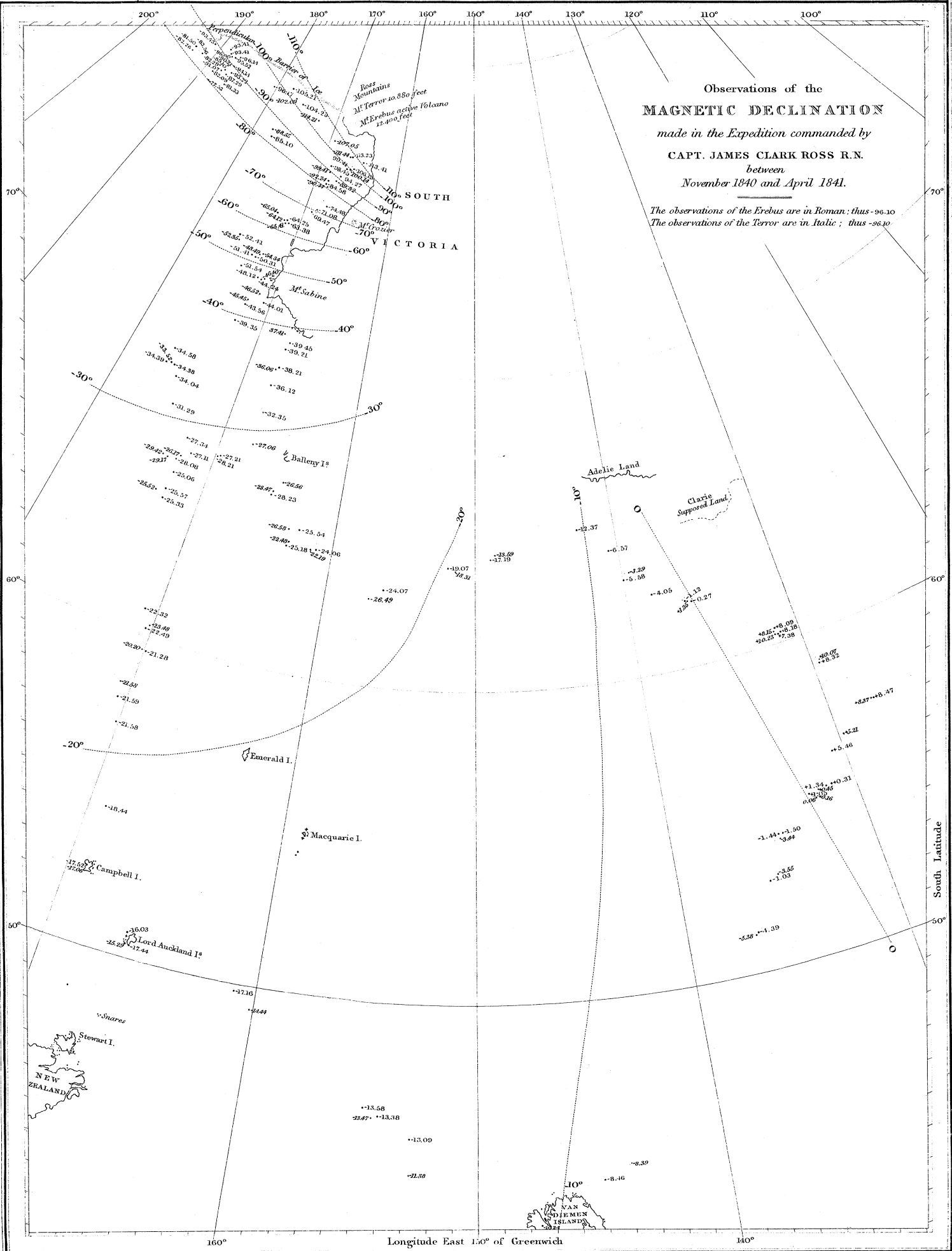
1. The observations of declination, particularly those which point out the course of the lines of 0 and of  $10^\circ$  east, indicate a more westerly position than the one assigned by M. GAUSS in the "Atlas des Erdmagnetismus" for the spot in which all the lines of declination unite. The progression of the lines in the southern hemisphere generally, from secular change, is from east to west; the difference consequently is in the direction in which a change should be found in comparing earlier with more recent determinations.

2. The general form of the curves of higher inclination in the southern hemisphere is much more analogous to that in the northern, than appears in M. GAUSS's maps. For example, the isoclinical line of  $-85^\circ$  instead of being nearly circular, as represented in the 3<sup>te</sup> Abtheilung of Pl. XVI. of the "Atlas des Erdmagnetismus," is an elongated ellipse, much more nearly resembling in form and dimensions the ellipse of  $85^\circ$  of inclination in the northern hemisphere in the same work, Pl. XVI. 2<sup>te</sup> Abtheilung. The analogy between the two hemispheres in the characteristic feature of the elliptical form of the higher isoclinical lines is the more important to notice, on account of the particular relation which appears to subsist in the northern hemisphere, between the change in the geographical direction of the greater axis of the ellipse, and the secular changes of the inclination generally throughout the hemisphere. The present direction of the greater axis in the northern hemisphere is nearly N.N.W. and S.S.E., or that of a line passing through the two foci of maximum intensity. In the southern hemisphere the present direction of the greater axis differs little from E.S.E. and W.N.W.

3. Captain Ross's observations of the intensity do not appear to indicate the existence anywhere in the southern hemisphere of a higher intensity than would be expressed by 2.1 of the arbitrary scale. In this respect also the analogy between the two hemispheres appears to be closer than is shown in M. GAUSS's maps, Atlas, Pl. XVIII. With respect to the direction of so much of the line of highest intensity (2.0) as it has been possible to draw with any degree of confidence from the observations now communicated, it will be found to be in almost exact parallelism with the isodynamic line of 1.7 in Plate III. of my memoir "On the Variations of the Magnetic Intensity" in the Reports of the British Association for 1838; which line was the highest of which the position could be assigned, for any considerable distance, by the aid of the then existing determinations.

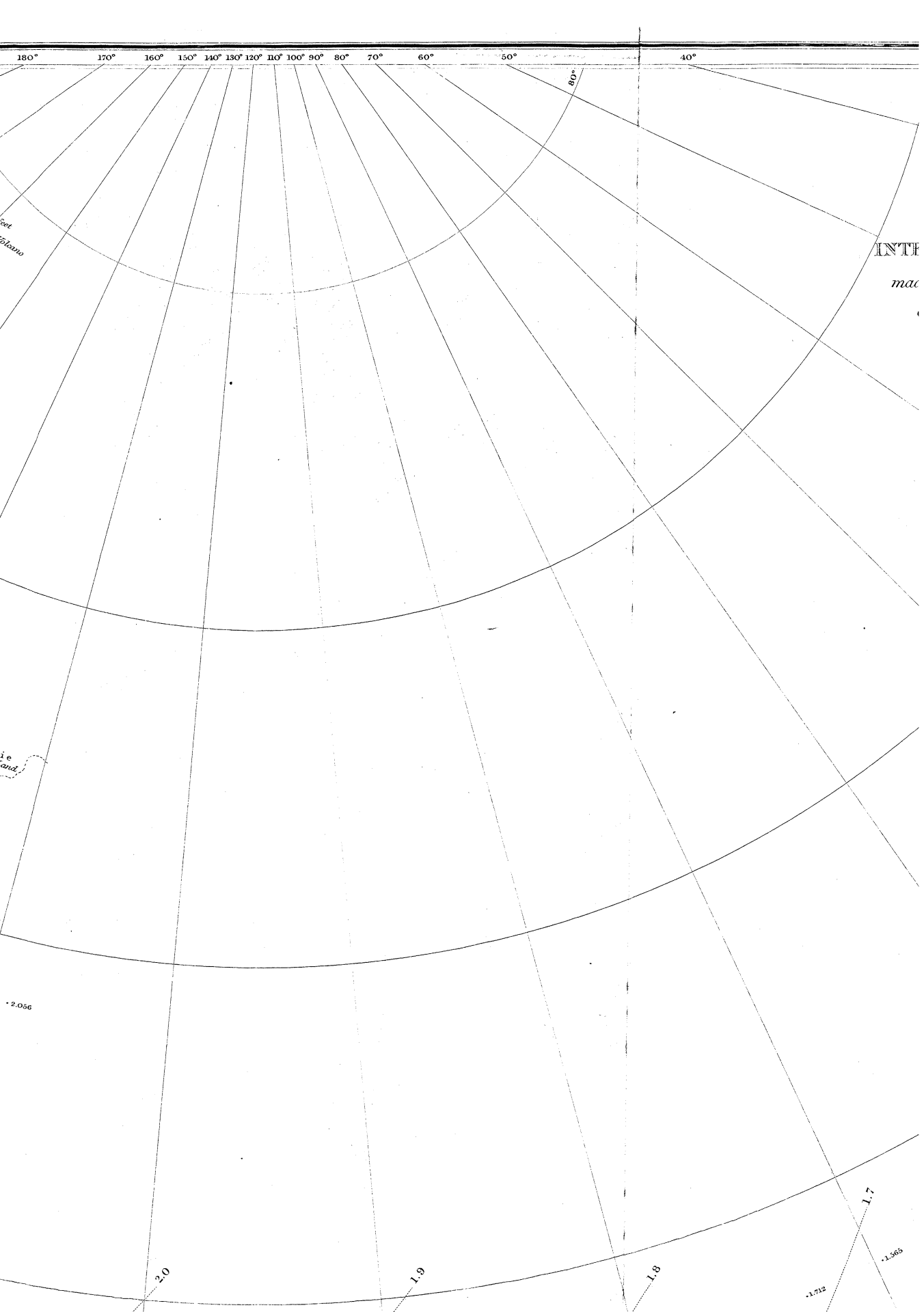
Observations of the  
MAGNETIC DECLINATION  
made in the Expedition commanded by  
CAPT. JAMES CLARK ROSS R.N.  
between  
November 1840 and April 1841.

The observations of the Erebus are in Roman; thus -96.10  
The observations of the Terror are in Italic; thus -96.10



South Latitude







Observations of the  
**INTENSITY OF THE MAGNETIC FORCE.**  
*made in the expedition commanded by*  
**CAPT. JAMES CLARK ROSS R.N.**  
*between*  
**July 1840, and April 1841.**

South Latitude

Kingman Reef I.  
1.565

1.7

1.565

1.576

1.601

1.6

1.574

1.589

1.5

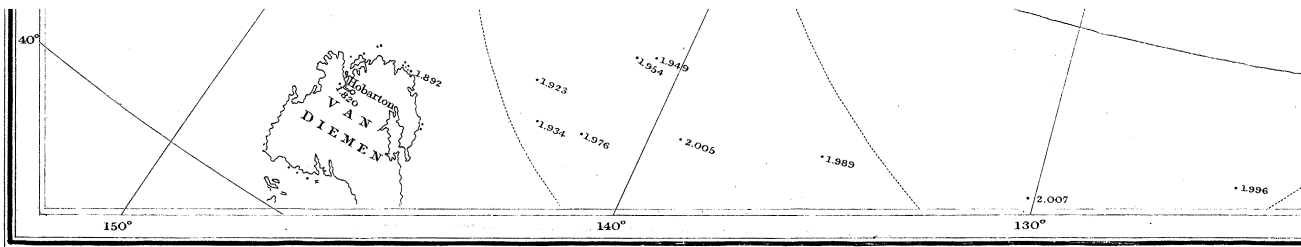
40°

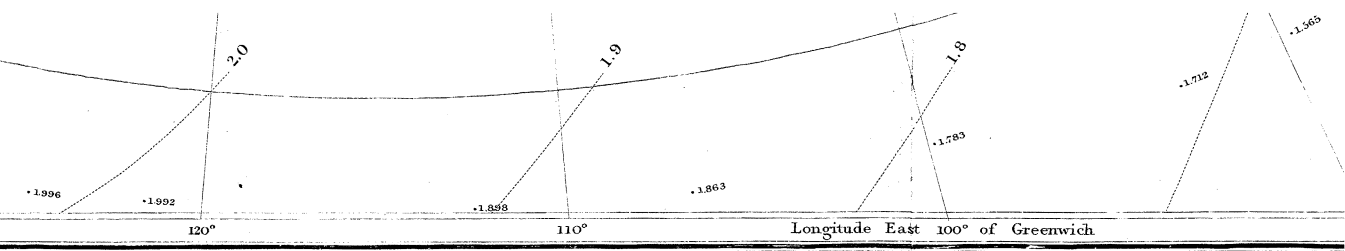
50°

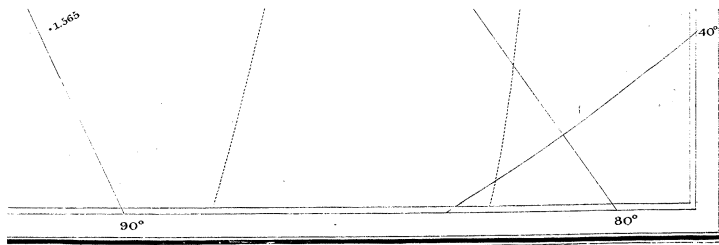
70°

80°

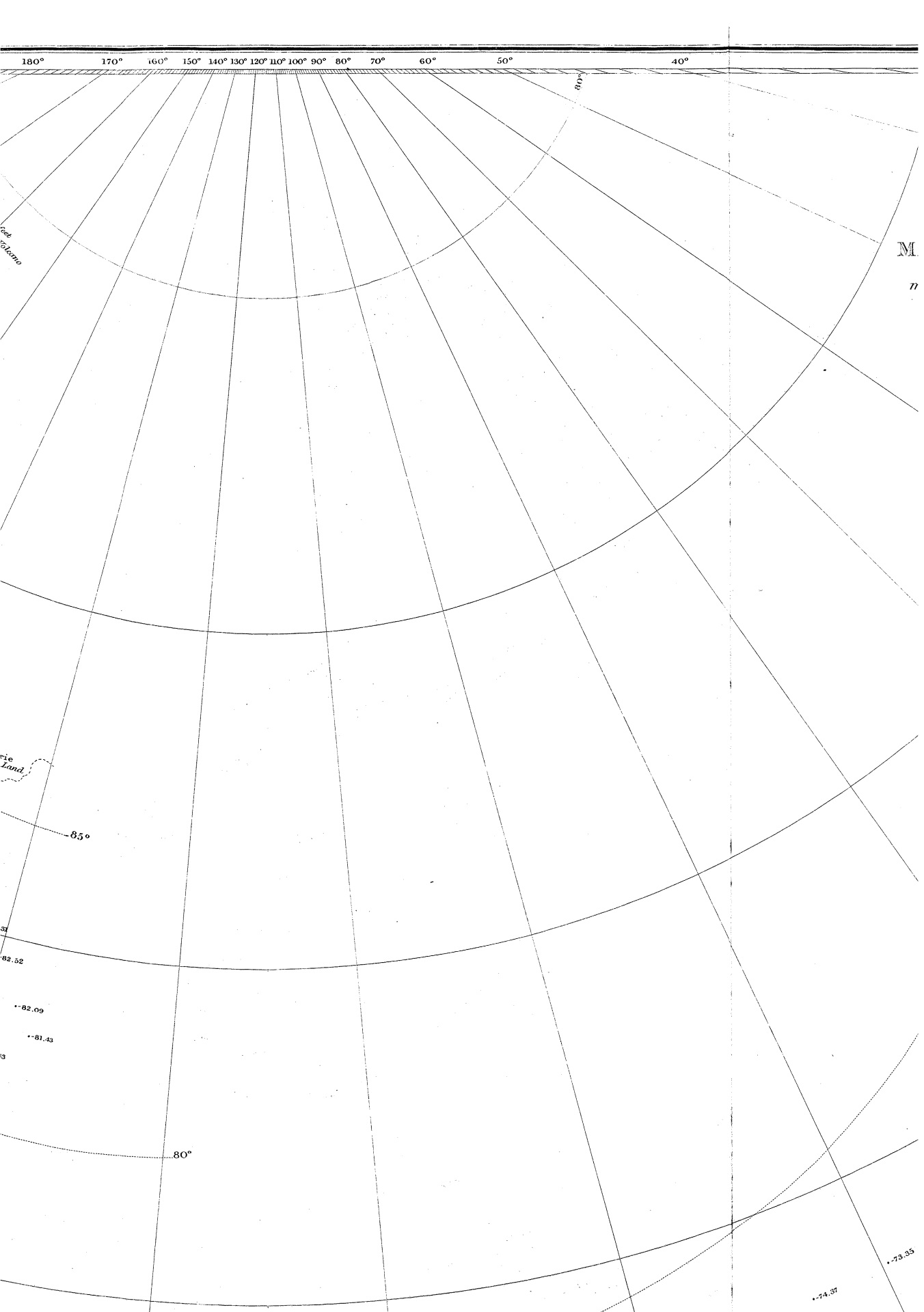












180° 170° 160° 150° 140° 130° 120° 110° 100° 90° 80° 70° 60° 50° 40°

ie Land

M

n

ie Land

85°

80°

80°

82.52

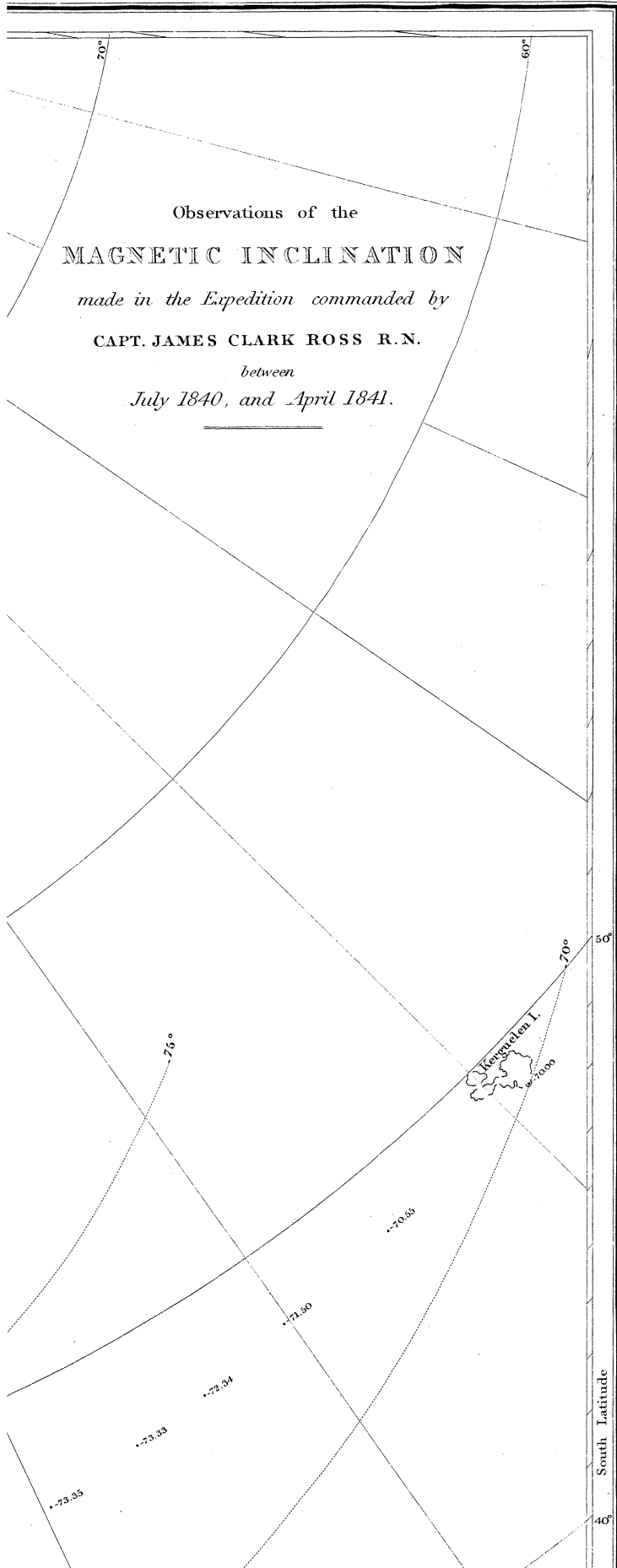
82.09

81.43

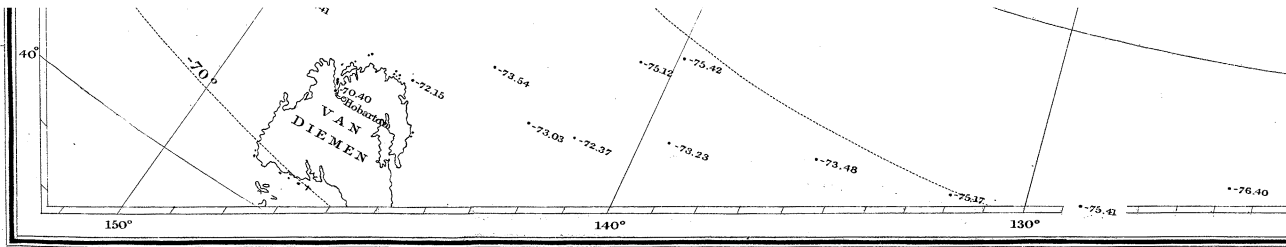
73.35

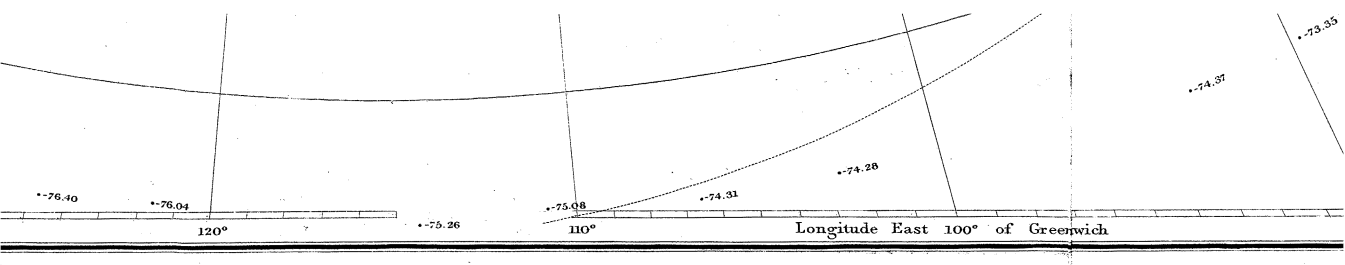
74.37

Observations of the  
**MAGNETIC INCLINATION**  
*made in the Expedition commanded by*  
**CAPT. JAMES CLARK ROSS R.N.**  
*between*  
*July 1840, and April 1841.*

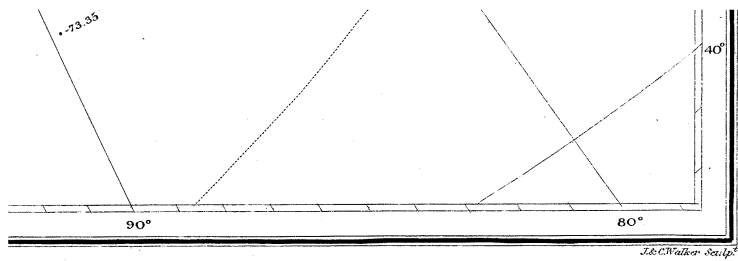


South Latitude









§ 9. *Observations of the Magnetic Inclination and Intensity made on board Her Majesty's ship Erebus on the passage from Kerguelen Island to Van Diemen Island in July and August 1840.*

These observations were made with Mr. Fox's apparatus, and with the same needle F which had been employed in the determinations made at sea on the passage from England to Kerguelen Island, discussed in § 5 and § 6 of these Contributions\*. The inclinations at sea were observed with the face of the circle always to the east: the index correction for needle F in this position of the instrument has been derived by comparing similar observations made with it at the magnetic observatory at Kerguelen Island, with the results obtained at the same spot with other needles which had their poles reversed. These are contained in the following Table:—

Observations of the Inclination with needles whose poles were reversed, made at the Magnetic Observatory at Kerguelen Island, July 1840.

1840.	Hours.	Needle.	Poles. $\alpha$ direct. $\beta$ reversed.	Mean.	Remarks.
July 4.	h m	C 1	$\alpha$ —69 59·7	—69 59·0	Needles belonging to H. M. S. Terror. Observers, { Captain CROZIER, Lieut. KAY.
	10 A.M.		$\beta$ —69 58·4		
6.	6 P.M.	C 2	$\alpha$ —69 59·0	—69 54·6	
			$\beta$ —69 50·2		
6.	6 15 P.M.	C 1	$\alpha$ —69 59·8	—70 00·7	
			$\beta$ —70 01·6		
6.	6 30 P.M.	C 2	$\alpha$ —69 59·7	—69 54·2	
			$\beta$ —69 48·7		
6.	7 20 P.M.	C 2	$\alpha$ —69 47·8	—69 54·4	
			$\beta$ —70 01·0		
8.	1 45 P.M.	R 4	$\alpha$ —70 03·1	—70 02·5	
			$\beta$ —70 02·0		
9.	5 30 P.M.	R G 1	$\alpha$ —69 54·3	—69 59·1	Needles belonging to H. M. S. Erebus. Observer, Captain Ross.
			$\beta$ —70 03·8		
9.	7 30 P.M.	R G 2	$\alpha$ —69 57·7	—70 00·8	
			$\beta$ —70 04·0		
10.	9 A.M.	R 10	$\alpha$ —70 13·9	—70 11·4	
			$\beta$ —70 08·9		
				—69 59·6	General Mean.

The inclination observed with needle F at the same spot with the face of the circle towards the east was  $-69^{\circ} 57' \cdot 9$ ; whence the index correction is  $-1' \cdot 7$ .

The intensity of the magnetic force was determined in this portion of the voyage, on every day that the weather permitted, by the angles of deflection caused by a deflecting magnet. The observations were a continuation of the series of which the earlier portion is given in § 5 and § 6. The deflecting magnet employed was the deflector S. Tables are given, in the sections referred to, of the values of  $w'$  for this deflector corresponding to angles of deflection from  $42^{\circ}$  to  $25^{\circ}$ , derived from a comparison with the deflections produced by weights. The increase of the terrestrial force, in the passage between Kerguelen and Van Diemen Islands, brought the angle

\* Philosophical Transactions, 1842, Art. II.

of deflection with deflector S down nearly to  $20^\circ$ . The weather was too unsettled to admit of any comparison being made with the weights at sea, and an accident which befel the needle on or before the arrival at Hobarton prevented the comparison which otherwise would have been made there. The values of  $w'$  corresponding to the angles of deflection from  $25^\circ$  to  $20^\circ$  have, therefore, been supplied, by continuing the rate of progression at which the deflecting force of the magnet S had been found by experiment, in angles from  $36^\circ$  to  $25^\circ$ , to increase as the angle diminished, viz. 0.033 gr. for each degree; we have thus the following values:—

$v' = 26$ ;	$w' = 2.594$
$v' = 25$ ;	$w' = 2.628$
$v' = 24$ ;	$w' = 2.661$
$v' = 23$ ;	$w' = 2.694$
$v' = 22$ ;	$w' = 2.727$
$v' = 21$ ;	$w' = 2.760$
$v' = 20$ ;	$w' = 2.793$ .

At Kerguelen Island we have the angle of deflection with the magnet S =  $26^\circ 21'3 = v$ ; the equivalent weight =  $2.58 = w$ ; and (§ 6.)  $I = 1.465$  (London = 1.372); whence in other localities

$$I' = I \frac{w' \sin v}{w \sin v'} = .2521 w' \operatorname{cosec} v',$$

$v'$  being furnished by the observation and  $w'$  taken from the preceding Table.

The last observation recorded to have been made with needle F was on the 11th of August, 1840, in lat. —  $44^\circ 16'$ , long.  $142^\circ 38'$ ; when the angle of deflection being  $21^\circ 06'5$ ,

$I' = 1.929$  uncorrected for the ship's attraction, or (the course being E. by N.  $\frac{1}{2}$  N.),  $I' = 1.934$  corrected.

On the return of the Expedition from the Antarctic Circle in the following year, the ships regained their former track, and on the 5th of April, 1841, Captain Ross repeated the observations with different instruments within a few miles of the spot on which he had observed on the 11th of August, 1840: these observations gave  $I' = 1.927$  in lat. —  $45^\circ 02'$ , long.  $143^\circ 10'$ . If we examine the map in which the intensity observations are inserted, we perceive that the direction of the two geographical positions in relation to each other is very nearly that of the isodynamic lines in that quarter; and if we refer generally to the Tables, we see that the difference in the resulting intensity on the two occasions is within the limits of the differences of partial determinations with the same instrument at one spot. As far as circumstances permit us to judge, therefore, we may view the observations of the two voyages as forming parts of one connected series.

As the ship's head during the run under consideration varied but little on any occasion from her direct course, and as that course is one on which the corrections, both of inclination and intensity, are small, I have taken them from the Table computed by means of the constants deduced in the preceding section.

Observations of the Inclination with Needle F on board H.M.S. Erebus, between July 22nd and August 11, 1840, on her passage from Christmas Harbour, Kerguelen Island, to Hobarton, Van Diemen Island.

1840.	Latitude.	Longitude.	Method employed.	Inclination. Face east.	Ship's head.	Corrections for ship's attraction.	Corrected inclination.	Remarks.				
June 26.	Magnetic Observatory, Kerguelen Island. -48 41      68 54		Direct.	-70 02.8	} Observed } on shore. }	.....	-69 59.6	} Remark by Captain Ross. "From these observations the Index error of Needle F.(face east), as used on board ship, may be obtained."				
			S.	-69 56.3								
			S. and N.	-69 48.3								
			N.	-70 04.2								
July 22.	-48 29      76 55		Direct.	-70 34.5	} s.e. by E.	-18	-70 55					
			S.	-70 36								
			23.	-48 17      80 15		Direct.	-71 48		} s.e. by E. $\frac{1}{2}$ E.	-12	-71 50	
						S.	-71 34.4					
			24.	-47 55      83 51		Direct.	-72 10		} s.e. by E. $\frac{1}{2}$ E.	-13	-72 34	
						S.	-72 29					
			25.	-47 46      86 18		Direct.	-73 4.5		} s.e. by E. $\frac{1}{2}$ E.	-15	-73 33	
						S.	-73 28.5					
			26.	-47 12      89 45		Direct.	-73 13		} s.e. by E. $\frac{1}{2}$ E.	-15	-73 35	} Considerable swell.
						S.	-73 24.5					
			27.	-47 03      93 0		Direct.	-74 11.3		} s.e. by E. $\frac{1}{2}$ E.	-16	-74 37	} A high sea.
						S.	-74 27.5					
			28.	-47 13      97 07		Direct.	-73 14.5		} s.e. by E. $\frac{1}{2}$ E.	.....	.....	} Too much motion to continue.
						S.	-73 14.5					
30.	-47 39      102 42		Direct.	-74 15	} E.S.E.	- 8	-74 28					
			S.	-74 22.5								
31.	-47 35      106 26		Direct.	-74 15.2	} E.S.E.	- 8	-74 31					
			S.	-74 26.4								
Aug. 1.	-47 45      110 39		Direct.	-74 48	} E.S.E.	- 9	-75 08	} Much motion.				
			S.	-75 6								
			2.	-47 34      114 15		Direct.	-75 20.5		} E. by s. $\frac{1}{2}$ S.	- 1	-75 26	
						S.	-75 6					
			4.	-47 41      121 30		Direct.	-76 9.8		} E. by s.	+ 6	-76 04	} Much motion.
						S.	-76 6.3					
			5.	-47 34      124 43		Direct.	-76 49.2		} E. $\frac{1}{2}$ S.	+13	-76 40	} Very unsteady.
						S.	-76 53.7					
			6.	-46 44      128 26		Direct.	-76 1.6		} E.	+21	-75 41	
						S.	-75 59					
			7.	-46 13      132 0		Direct.	-75 43.7		} E. $\frac{1}{2}$ N.	+29	-75 17	
S.	-75 45											
8.	-45 59      135 38		Direct.	-74 33.5	} E. by N.	+36	-73 48					
			S.	-74 11								
9.	-45 17      139 19		Direct.	-74 17.5	} E.N.E.	+48	-73 23					
			S.	-74 0.4								
10.	-44 24      141 39		Direct.	-73 39.15	} N.E. by E.	+59	-72 37					
			S.	-73 33								
11.	-44 16      142 38		Direct.	-73 37.15	} E. by N. $\frac{1}{2}$ N.	+42	-73 03					
			S.	-73 49								

The index correction - 1.7 has been applied in the final column.

Observations of the Magnetic Intensity with Needle F, on board H.M.S. Erebus, between July 22nd and August 11th, 1840, in her passage from Christmas Harbour, Kerguelen Island, to Hobarton, Van Diemen Island.

1840.	Latitude.	Longitude.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Corrections for ship's attraction.	Corrected intensity. London = 1.372.	Remarks.
June 26 and 28.	On shore at Kerguelen Island.		W. 1½ gr.	14 48.6	34.5	} Observed } } on shore. }	1.465		1.465	At the Magnetic Observatory.
		68 54	W. 2 grs.	20 19.6	34.5					
July 22.	-48 41		S.	26 21.3	34	S.E. by E.	1.563	-.024	1.539	
23.	-48 29	76 55	S.	25 0.3	33	S.E. by E. ½ E.	1.594	-.020	1.574	
24.	-48 17	80 15	S.	24 39.4	33	S.E. by E. ½ E.	1.621	-.020	1.601	
25.	-47 55	83 51	S.	24 20	39	S.E. by E. ½ E.	1.595	-.020	1.575	
26.	-47 46	86 18	S.	24 38.5	35	S.E. by E. ½ E.	1.585	-.020	1.565	
27.	-47 12	89 45	S.	24 46.5	34	S.E. by E. ½ E.	1.732	-.020	1.712	
28.	-47 03	93 0	S.	23 04	44	S.E. by E. ½ E.	1.732	-.020	1.712	
29.	-47 13	97 07	S.	23 04	44	S.E. by E. ½ E.	1.872	-.017	1.855	
30.	-47 39	102 42	S.	21 37.5	43	E.S.E.	1.880	-.017	1.863	
31.	-47 35	106 26	S.	21 33.6	44	E.S.E.	1.832	-.017	1.815	
Aug. 1.	-47 45	110 39	S.	22 01.7	35	E.S.E.	1.984	-.014	1.970	Much motion.
	-47 34	114 15	S.	20 37	42	E. by S. ½ S.	2.002	-.010	1.992	
2.	-47 41	121 30	S.	20 27.7	40	E. by S.	2.002	-.006	1.996	Very unsteady. Very unsteady.
4.	-47 34	124 43	S.	20 28.2	41	E. ½ S.	2.037	-.003	2.034	
5.	-46 44	128 26	S.	20 10.5	42	E.	1.980	0	1.980	
6.	-46 13	132 0	S.	20 39.2	49	E. ½ N.	1.987	+0.02	1.989	
7.	-45 59	135 38	S.	20 34.7	51	E. by N.	1.997	+0.08	2.005	
8.	-45 17	139 19	S.	20 31.1	55	E.N.E.	1.962	+0.14	1.976	
9.	-44 24	141 39	S.	20 48.7	50	N.E. by E.	1.929	+0.05	1.934	
10.	-44 16	142 38	S.	21 06.5	48	E. by N. ½ N.				

DECLINATIONS observed on board Her Majesty's Ship Erebus between November 15, 1840, and April 6, 1841.

The Observers are distinguished in the column of Initials as follows:—R. Captain ROSS; S. Lieut. SIBBALD; W. Lieut. WOOD; T. Mr. TUCKER, Master; SM. Mr. SMITH, and O. Mr. OAKLEY, Mates; Y. Mr. YULE, Second Master. East Declination is characterised by the sign —.

1840.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.				
	Lat.	Long.												
Nov. 15. P.M.	—45 33	152 49	R.	— 8 55	E.S.E.	—71 40	— 4 39	—13 34	—13 09					
	—45 33	152 49	T.	— 8 37	E.S.E.		— 4 39	—13 16						
	—45 33	152 49	R.	— 8 23	E.S.E.		— 4 39	—13 02						
	—45 33	152 49	T.	— 8 25	E.S.E.		— 4 39	—13 04						
	—45 38	152 55	SM.	— 8 10	E.S.E.		— 4 39	—12 49						
	—45 38	152 55	R.	— 8 32	E.S.E.		— 4 39	—13 11						
	—45 38	152 55	R.	— 8 22	E.S.E.		— 4 39	—13 01						
	—45 40	153 02	R.	— 8 40	E.S.E.		— 4 39	—13 19						
	16 A.M.	—46 05	154 11	T.	— 8 31		S.E. by E. 1/2 E.	—72 04			— 4 34	—13 05	—13 38	
		—46 05	154 11	Y.	— 8 39		S.E. by E. 1/2 E.				— 4 34	—13 13		
		—46 05	154 11	S.	— 8 56		S.E. by E.				— 4 23	—13 19		
		—46 09	154 14	S.	— 9 17		S.E. by E. 1/2 E.				— 4 34	—13 51		
—46 09		154 14	Y.	— 9 23	S.E. by E. 1/2 E.	— 4 34	—13 57							
—46 09		154 14	T.	— 9 40	S.E. by E. 1/2 E.	— 4 34	—14 14							
16 P.M.	—46 09	154 14	T.	— 8 31	S.E. by E. 1/2 E.	—72 04	— 4 34	—13 05	—13 58					
	—46 15	154 28	S.	— 9 50	S.E. by E. 1/2 E.		— 4 34	—14 24						
	—46 30	154 54	T.	—13 29	N.		0 00	—13 29						
	—46 30	154 54	S.	—14 55	N. by E.		— 0 46	—15 41						
	—46 30	154 54	T.	—12 57	N.N.E.		— 1 30	—14 27						
	—46 30	154 54	T.	— 8 05	S.E. by E. 1/2 E.		— 4 34	—12 39						
18 P.M.	—46 30	154 54	R.	— 9 12	S.E. by E. 1/2 E.	—72 04	— 4 34	—13 46	—13 53					
	—46 30	154 54	R.	— 9 15	S.E. by E. 1/2 E.		— 4 34	—13 49						
	—46 32	155 01	T.	— 9 19	S.E. by E. 1/2 E.		— 4 34	—13 53						
	—49 36	160 52	R.	—13 11	E.S.E.		—74 00	— 5 19			—17 16	—17 16		
	—49 42	160 56	R.	—12 27	E.S.E.									
	—49 48	161 00	R.	—11 49	E.S.E.									
—49 49	161 00	T.	—12 18	E.S.E.										
—49 49	161 00	T.	—12 03	E.S.E.										
—49 49	161 00	T.	—12 06	E.S.E.										
Dec. 5. A.M.	—49 52	161 08	R.	—11 18	E.S.E.	.....	+ 4 05	—18 24	.....					
	—49 52	161 08	S.	—10 27	E.S.E.						.....	+ 4 05	—18 21	.....
P.M.	At anchor.	.....	.....	—22 29	S.W.	.....	.....	.....	.....	Declination observed on shore with the Magnetometers of the Observatory.				
	At anchor.	.....	.....	—22 26	S.W.	.....	.....	.....	.....					
	Auckland Island.	—50 32	166 12	R.	—17 49	Observed on shore.	.....	.....	.....		—17 44.1			
					—17 44									
					—17 45									
					—17 42									
					—17 43									
	At anchor.	.....	.....	—16 44	S.	.....	0 00	—16 44	.....					
	At anchor.	.....	.....	—16 20	S.S.W.	.....	+ 2 17	—14 03	.....					
	8 P.M.	At anchor.	.....	T.	—20 26	N.N.W.	.....	+ 1 39	—18 47		.....			
—22 35					N.W.	.....	+ 3 10	—19 25	.....					
—20 17					N.N.W.	.....	+ 1 39	—18 38	.....					
—19 56					N.N.W. 1/2 W.	.....	+ 2 03	—17 53	.....					
—19 54					N.N.W.	.....	+ 1 39	—18 15	.....					
—15 38					N.N.E.	.....	— 1 39	—17 17	.....					
—15 46					N.E.	.....	— 3 10	—18 56	.....					
At anchor.	.....	.....	—13 36	E.N.E.	.....	— 4 23	—17 59	.....						
At anchor.	.....	.....	—12 52	E.	—73 15	— 5 05	—17 57	—17 53	Mean declination observed on board at anchor.					

Observations of Declination. (Continued.)

1840.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Dec. 11. A.M.	Auckland Island. At anchor.		T.	-22° 06'	w.n.w.	-73 15	+ 4 23	-17 43	-17 53	
			T.	-21 39	N.W. by W.		+ 3 50	-17 49		
			T.	-22 49	w.		+ 5 05	-17 44		
			T.	-23 19	w. by N.		+ 4 50	-18 29		
			T.	-23 01	w.		+ 5 05	-17 56		
			T.	-22 26	w. by N.		+ 4 50	-17 36		
			T.	-21 32	N.W. ½ N.		+ 2 48	-18 44		
12 A.M.	-50 33	166 24	R.	-12 33	S.E. by E.	-73 30	- 4 46	-17 19	-16 03	
	-50 33	166 24	S.	-12 15	S.E. by E. ½ E.		- 4 58	-17 13		
	-50 33	166 24	T.	-12 30	S.E. by E.		- 4 46	-17 16		
13 A.M.	-50 48	166 42	T.	-10 15	S.E. by E.	-73 52	- 4 46	-15 01	-17 52	
	-50 48	166 43	S.	-11 06	S.E. by E.		- 4 46	-15 52		
	-50 48	166 43	Y.	- 9 46	S.E. by E.		- 4 46	-14 32		
16 P.M.	-52 14	166 43	S.	-10 37	S.E. ½ E.	-73 52	- 4 28	-15 05	-17 52	
	-52 33	169 09	R.	-22 19	S.W. ½ W.		+ 4 32	-17 47		
18 A.M.	Campbell Island, at anchor.		R.	-23 14	w.s.w.	-74 46	+ 5 17	-17 57	-18 44	
			R.	-15 53	S.S.E.		- 2 29	-18 22		
			S.	-15 41	S.S.E.		- 2 29	-18 10		
			R.	-15 21	S.S.E. ½ E.		- 3 00	-18 21		
19 A.M.	-54 12	169 06	R.	-17 31	S.S.E.	-75 30	- 2 29	-20 00	-21 58	
	-54 16	169 06	T.	-17 31	S.S.E.		- 2 29	-20 00		
	-54 16	169 07	S.	-15 42	S.S.E.		- 2 29	-18 11		
21 A.M.	-55 22	169 38	S.	-18 47	S. ½ W.	-77 00	+ 0 40	-18 07	-21 59	
-57 25	170 21	Sm.	-20 40	S.S.E.	- 3 01		-23 41			
-57 25	170 21	T.	-19 39	S.S.E.	- 3 01		-22 40			
-57 27	170 21	Y.	-20 43	S.S.E.	- 3 01		-23 44			
-57 27	170 21	T.	-18 18	S.S.E.	- 3 01		-21 19			
-57 31	170 21	Sm.	-20 43	S.S.E.	- 3 01		-23 44			
-57 35	170 21	S.	-17 09	S.S.E.	- 3 01		-20 10			
-57 35	170 21	O.	-19 06	S. ½ E.	- 0 44		-19 50			
-57 36	170 21	T.	-20 00	s. by E. ½ E.	- 2 15		-22 15			
-57 38	170 27	R.	-21 54	s.	0 00		-21 54			
-57 38	170 27	S.	-17 43	S.S.E.	- 3 01		-20 44			
-57 40	170 28	R.	-24 54	S. ½ E.	- 0 44		-25 38			
-57 45	170 28	S.	-23 29	s. by w. ½ w.	+ 2 15	-21 14				
-57 45	170 28	O.	-24 32	s. by w. ½ w.	+ 2 15	-22 17				
22 A.M.	-59 00	170 55	T.	-19 34	S.S.E.	-78 04	- 3 12	-22 46	-21 28	
-59 01	170 51	T.	-19 08	S.E. by S.	- 4 29		-23 37			
-59 36	170 08	T.	-23 25	s. by w. ½ w.	+ 2 30		-20 55			
23 A.M.	-59 45	170 02	Y.	-21 54	S. ¾ W.	-78 33	+ 1 15	-20 39	-22 49	
-59 47	170 02	Y.	-21 12	s. by w.	+ 1 40		-19 32			
-59 42	169 16	R.	-17 57	S.E. by S.	- 4 39		-22 36			
23 P.M.	-59 43	169 17	T.	-17 19	S.S.E.	-78 53	- 3 18	-20 37	-22 49	
-49 45	169 19	T.	-15 01	S.E. ¼ E.	- 6 03		-21 04			
24 A.M.	-60 10	170 24	Sm.	-20 07	S.S.E.		- 3 21	-23 28		
-60 10	170 24	T.	-20 17	s. by E.	- 1 43		-22 00			
-60 10	170 24	T.	-21 33	s.	0 00		-21 33			
-60 10	170 24	T.	-21 38	S. ¼ W.	+ 0 25		-21 13			
-60 12	170 24	Y.	-20 01	S.E.	- 6 03		-26 04			
-60 12	170 24	S.	-18 03	s. by E. ½ E.	- 2 30		-20 33			
-60 12	170 24	O.	-20 21	S.S.E.	- 3 21		-23 42			
-60 12	170 24	T.	-21 27	s. by E.	- 1 43		-23 10			
-60 18	170 27	R.	-20 13	S.S.E.	- 3 21	-23 34				
-60 20	170 27	R.	-19 31	S.S.E.	- 3 21	-22 52				

Observations of Declination. (Continued.)

1840.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.				
	Lat.	Long.												
Dec. 24 P.M.	-60 42	170 55	R.	-16 49	S.E.	-79 06	- 6 06	-22 55	-22 32					
	-60 42	170 55	R.	-18 03	S.E. by S.		- 4 52	-22 55						
	-60 46	170 55	R.	-18 06	S.E. by S.		- 4 52	-22 58						
	-60 46	170 55	R.	-18 23	S.E. by S.		- 4 52	-23 15						
	-60 46	170 55	S.	-19 37	S. by E. 1/2 E.		- 2 40	-22 17						
	-60 46	170 55	T.	-18 42	S.S.E.		- 3 25	-22 07						
	-60 48	170 55	R.	-18 02	S.E. by S.		- 4 52	-22 54						
	-60 48	170 55	T.	-17 35	S.E. by S.		- 4 52	-22 27						
	-60 48	170 40	S.	-17 33	S.E. by S.		- 4 52	-22 25						
	-60 50	170 44	R.	-17 57	S.E. by S.		- 4 52	-22 49						
	-60 55	170 41	S.	-16 46	S.S.E. 1/2 E.		- 4 07	-20 53						
	29 P.M.	-64 10	172 28	R.	-30 28		S.S.W.	-81 03			+ 4 06	-26 22	-25 33	
		-64 10	172 28	R.	-29 24		S.S.W.				+ 4 06	-25 18		
		-64 10	172 28	R.	-27 34		S. by W.				+ 2 06	-25 28		
-64 12		172 29	SM.	-25 30	S. 1/2 W.	+ 1 02	-24 28							
30 A.M.	-64 12	172 29	S.	-25 32	S. 1/2 W.	-81 11	+ 1 02	-24 30	-25 57					
	-64 12	172 29	S.	-23 32	S.E.		+ 7 24	-30 56						
	-64 27	172 36	S.	-30 04	S.W. 1/2 S.		+ 6 44	-23 20						
	-64 27	172 36	S.	-31 18	S.W. 1/2 S.		+ 6 44	-24 34						
	-64 27	172 36	T.	-32 36	S.W.		+ 7 30	-25 06						
	-64 37	172 40	Y.	-31 01	S.W. 1/2 W.		+ 8 04	-22 57						
	-64 37	172 40	SM.	-31 54	S.S.W.		+ 4 11	-27 43						
	-64 37	172 40	R.	-23 26	S.		0 00	-23 26						
30 P.M.	-64 37	172 40	T.	-24 08	S.	-81 16	0 00	-24 08	-25 06					
	-64 37	172 40	S.	-26 01	S.		0 00	-26 01						
	-64 44	172 50	R.	-25 03	S.S.E.		- 4 11	-29 14						
	-64 46	172 50	R.	-23 04	S.S.E.		- 4 11	-27 15						
31 A.M.	-64 48	172 50	R.	-22 43	S.S.E.	-81 45	- 4 11	-26 54	-25 06					
	-65 22	172 25	S.	-22 13	S.S.E.		- 4 25	-26 38						
	-65 22	172 25	O.	-19 39	S.S.E. 1/2 E.		- 5 24	-25 03						
	-65 23	172 21	S.	-22 06	S. by E. 1/2 E.		- 3 20	-25 26						
	-65 25	172 21	O.	-21 33	S. by E.		- 2 15	-23 48						
	-65 25	172 21	S.	-22 15	S. by E.		- 2 15	-24 30						
	-65 30	172 16	T.	-22 36	S. by E.		- 2 15	-24 51						
	-65 30	172 16	T.	-23 00	S. 1/2 E.		- 1 05	-24 05						
31 P.M.	-65 31	172 16	Y.	-27 33	S. 1/2 W.	-82 30	+ 1 05	-26 28	-27 11					
	-65 31	172 16	S.	-22 33	S.		0 00	-22 33						
	-65 32	172 14	T.	-24 02	S.		0 00	-24 02						
	-66 04	171 34	T.	-29 03	S.		0 00	-29 03						
	-66 07	171 34	SM.	-29 23	S. 1/2 W.		+ 1 13	-28 10						
	-66 07	171 34	S.	-30 05	S. 1/2 W.		+ 1 13	-28 52						
1841.	-66 07	171 34	T.	-30 38	S. 1/2 W.	-82 30	+ 1 13	-29 25	-28 21					
	-66 09	171 32	R.	-30 39	S. by W.		+ 2 30	-28 09						
	Jan. 1 A.M.	-66 09	171 32	W.	-35 45		N.W. by W.	+ 9 18			-26 27			
	1 P.M.	-66 20	170 32	S.	-32 20		S.S.W.	+ 4 50			-27 30			
	2 A.M.	-66 28	170 48	R.	-32 44		S.S.W.	-82 30			+ 4 50	-27 54	-28 21	
		-66 20	169 13	T.	-20 18		S.E.				- 8 47	-29 05		
		-66 20	169 13	T.	-17 35		E.S.E.				-11 11	-28 46		
		-66 20	169 13	SM.	-22 21		S.E.				- 8 47	-31 08		
		-66 20	169 13	T.	-18 44		S.E. by E.				-10 11	-28 55		
		-66 20	169 13	Y.	-17 53		S.E. by E.				-10 11	-28 04		
		-66 20	169 41	S.	-17 08		S.E. by E.				-10 11	-27 19		
		-66 20	169 41	T.	-17 01		E.S.E.				-11 11	-28 12		
-66 20		169 43	R.	-16 33	E.S.E.	-11 11	-27 44							
-66 24		169 44	R.	-17 52	E.S.E.	-11 11	-29 03							



Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.			
	Lat.	Long.											
Jan. 2 A.M.	-66 30	169 44	T.	-35 14	W.N.W. $\frac{1}{2}$ W.	-82 30	+ 10 55	-24 19	-27 21				
	-66 30	169 44	W.	-35 45	N.W. by W.		+ 9 18	-26 27					
	-66 30	169 46	R.	-35 31	N.W. by W.		+ 9 18	-26 13					
	-66 30	169 46	S.	-34 28	N.N.W. $\frac{1}{2}$ W.		+ 5 11	-29 17					
	-66 29	169 48	O.	-31 46	N.N.W.		+ 4 11	-27 35					
4 A.M.	-65 28	171 47	S.	-20 09	S.E. by S.	-82 0	- 6 35	-26 44	-27 34				
	-65 28	171 47	O.	-18 33	S.E.		- 8 15	-26 48					
	-65 28	171 47	W.	-19 43	S.E. by E.		- 9 33	-29 16					
	-65 28	171 47	T.	-17 46	E. by S. $\frac{3}{4}$ S.		-10 38	-28 24					
	-65 28	171 47	T.	-17 28	E. by S. $\frac{3}{4}$ S.		-10 38	-28 06					
4 P.M.	-65 28	171 56	W.	-16 43	E. by S. $\frac{1}{2}$ S.	-81 45	-10 45	-27 28	-28 08				
	-65 26	172 50	R.	-15 21	S. 79° E.		-11 00	-26 21					
	-65 26	172 50	R.	-15 44	S. 74° E.		-10 45	-26 29					
	-65 26	173 06	T.	-16 14	E. by S.		-11 00	-27 14					
	-65 26	173 06	T.	-17 00	E.S.E.		-10 30	-27 30					
	-65 27	173 32	R.	-18 22	S. 67° E.		-10 30	-28 52					
	-65 27	173 32	W.	-14 08	E.S.E.		-10 12	-24 20					
	-65 27	173 32	R.	-17 26	S. 72° E.		-10 17	-27 43					
	-65 27	173 32	R.	-18 59	S. 63° E.		- 9 45	-28 44					
	-65 27	173 32	Sm.	-18 35	E.S.E.		-10 12	-28 47					
	-65 27	173 32	T.	-17 55	E.S.E.		-10 12	-28 07					
	-65 29	173 55	R.	-18 08	S. 68° E.		-10 12	-28 20					
	-65 30	173 55	R.	-19 42	S.E. by E. $\frac{1}{2}$ E.		- 9 45	-29 27					
	-65 40	173 55	Y.	-19 16	S.E. $\frac{1}{2}$ E.		- 8 38	-27 54					
	-65 32	173 55	T.	-23 49	S. by E. $\frac{1}{2}$ E.		- 3 21	-27 10					
5 A.M.	-65 34	173 55	R.	-22 48	S.E.	-82 30	- 7 56	-30 44	-31 29				
	-66 39	174 14	Y.	-29 46	S.E. by S.		- 7 04	-36 50					
	-66 39	174 14	Sm.	-21 41	S.E.		- 8 47	-30 28					
	5 P.M.	-67 12	174 41	R.	-28 05		S.S.E.	-83 00		- 5 11	-33 16	-34 04	
		-67 12	174 42	T.	-29 49		S. by E.			- 2 42	-32 31		
-67 12		174 42	Y.	-30 10	S. $\frac{3}{4}$ E.	- 2 01	-32 11						
-67 12		174 42	Y.	-27 59	S.S.E. $\frac{1}{2}$ E.	- 6 25	-34 24						
-67 23		174 42	R.	-18 03	E.S.E.	-11 57	-30 00						
6 A.M.	-67 23	174 42	T.	-17 25	E.S.E.	-83 30	-11 57	-29 22	-34 04				
	-67 23	174 42	T.	-18 05	S.E. by E.		-10 53	-28 58					
	-67 23	174 42	T.	-17 13	E.S.E.		-11 57	-29 10					
	-67 23	174 42	R.	-18 07	E.S.E.		-11 57	-30 04					
	-67 27	174 42	R.	-18 44	E.S.E.		-11 57	-30 41					
	-67 28	174 51	R.	-21 06	S.E.		- 9 23	-30 29					
	-67 28	174 51	T.	-26 53	S.S.E.		- 5 11	-32 04					
	-67 29	174 51	R.	-29 42	S. $\frac{3}{4}$ E.		- 2 01	-31 43					
	-67 30	174 51	R.	-26 31	S.S.E.		- 5 11	-31 42					
	-67 50	175 00	O.	-29 01	S.S.E.		-83 30	- 5 33		-34 34	-34 04		
	-67 50	175 00	S.	-29 09	S.S.E.			- 5 33		-34 42			
	-67 52	175 01	S.	-31 48	S.S.E.			- 5 33		-37 21			
	-67 52	175 01	O.	-27 53	S.S.E.			- 5 33		-33 26			
	-68 00	175 00	T.	-26 11	S.S.E. $\frac{1}{2}$ E.			- 6 46		-32 57			
	-68 00	175 00	Y.	-27 00	S.S.E.			- 5 33		-32 33			
-68 00	175 00	S.	-27 01	S.S.E.	- 5 33	-32 34							
-68 00	175 00	T.	-27 42	S.S.E.	- 5 33	-33 15							
-68 05	175 10	W.	-26 58	S.S.E. $\frac{1}{2}$ E.	- 6 46	-33 44							
-68 05	175 10	T.	-28 18	S.S.E.	- 5 33	-33 51							
-68 05	175 14	R.	-29 51	S.S.E.	- 5 33	-35 24							
-68 05	175 14	R.	-43 7	N.W.	+ 9 09	-34 38							
-68 12	175 14	R.	-24 56	S.E. $\frac{1}{2}$ S.	- 9 02	-33 58							

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Jan. 7 P.M.	-68 32	175 49	T.	-46 02	w. 3/4 N.	-83 35	+13 25	-32 37	-33 52	Observed on ice.
	-68 32	175 49	T.	-47 05	w. by s. 1/2 s.		+13 20	-33 45		
	-68 32	175 49	W.	-46 07	w. by s.		+13 39	-32 28		
	-68 32	175 49	SM.	-24 06	s.e. 1/2 e.		-11 02	-35 08		
	-68 32	175 49	T.	-46 57	w. by s.		+13 39	-33 18		
	-68 32	175 49	R.	-25 49	s.e. 1/2 s.		-9 12	-35 01		
8 A.M.	-68 32	175 49	R.	-47 29	w. by s. 1/2 s.	+13 20	-34 09	-34 39.1		
	-68 32	175 55	T.	-30 21	s. by e. 3/4 e.	-5 30	-35 51			
	-68 30	176 35	T.	-20 22	s.e. by e. 3/4 e.	-12 44	-33 06			
	-68 30	176 35	S.	-20 51	e. 3/4 n.	-13 25	-34 16			
	-68 30	176 35	T.	-20 22	e. by s. 3/4 s.	-13 10	-33 32			
	-68 30	176 35	Y.	-19 58	e. by s. 1/2 s.	-13 20	-33 18			
8 P.M.	-68 28	176 32	R.	-34 39.1						
9 A.M.	-68 55	176 24	S.	-29 26	s.s.e.	-83 45	-5 45	-35 11	-34 58	
	-68 55	176 24	Y.	-29 38	s.s.e.		-5 45	-35 23		
	-68 55	176 24	O.	-28 49	s.s.e.		-5 45	-34 34		
	-68 55	176 18	T.	-29 09	s.s.e.		-5 45	-34 54		
10 P.M.	-68 55	176 18	W.	-29 04	s.s.e.	-5 45	-34 49	-39 35		
	-70 31	173 17	R.	-41 12	s.	0 00	-41 12			
	-70 32	172 56	R.	-47 04	s. 27° w.	+8 34	-38 30			
	-70 34	172 53	R.	-47 35	s. 25° w.	+8 00	-39 35			
	-70 34	172 53	S.	-49 34	s.s.w. 1/2 w.	+8 43	-40 51			
	-70 34	172 52	R.	-59 05	w.	+17 50	-41 12			
11 A.M.	-70 34	172 52	R.	-49 12	s.w.	+13 03	-36 09	-43 56		
	-70 52	172 25	T.	-44 19	s.	0 00	-44 19			
	-70 52	172 25	Y.	-44 35	s.	0 00	-44 35			
	-70 55	172 27	SM.	-45 31	s.	0 00	-45 31			
	-71 02	172 27	T.	-43 11	s.	0 00	-43 11			
	-71 02	172 27	SM.	-43 48	s.	0 00	-43 28			
	-71 02	172 27	T.	-46 48	s. 1/2 w.	+2 08	-44 40			
	-71 02	172 27	S.	-43 43	s.	0 0	-43 43			
	-71 02	172 27	O.	-44 36	s. 1/2 w.	+2 08	-42 28			
	-71 12	172 15	R.	-43 29	s.	0 0	-43 29			
11 P.M.	-71 21	170 52	R.	-48 45	s. by w.	+4 20	-44 25	-44 01		
	-71 21	170 52	T.	-50 10	s. by w. 1/2 w.	+6 28	-43 42			
	-71 21	170 52	W.	-47 35	s. by w. 1/2 w.	+6 28	-41 07			
	-71 21	170 52	Y.	-51 03	s. by w. 1/2 w.	+6 28	-44 35			
	-71 22	170 56	T.	-51 09	s. by w. 1/2 w.	+6 28	-44 41			
	-71 22	170 56	S.	-47 45	s. by w.	+4 20	-43 25			
	-71 22	170 56	O.	-49 33	s. by w. 1/2 w.	+6 28	-43 05			
	-71 24	170 56	T.	-51 42	s. by w. 1/2 w.	+6 28	-45 14			
	-71 24	170 56	S.	-59 57	s.w.	+15 50	-44 07			
	-71 19	171 06	T.	-28 17	n.e. by e.	-17 36	-45 53			
12 P.M.	-71 52	171 11	S.	-27 44	n.e. 1/2 n.	-13 38	-41 22	-44 24		
	-71 52	171 11	W.	-30 36	n.e. 1/2 n.	-13 38	-44 14			
13 P.M.	-72 07	172 18	S.	-27 40	e. by n. 1/2 n.	-21 06	-48 46	-48 12		
15 A.M.	-71 46	171 57	O.	-49 22	s. by w. 1/2 w.	+6 40	-42 42			
	-71 46	171 57	S.	-48 22	s. by w. 1/2 w.	+6 40	-41 42			
-71 46	171 55	T.	-51 34	s. by w. 1/2 w.	+6 40	-44 54				
-71 46	171 55	S.	-51 24	s.s.w.	+8 52	-42 32				
-71 54	172 17	T.	-24 13	e. by s.	-22 11	-46 24				
-71 54	172 17	R.	-24 51	e. by s.	-22 11	-47 02				
-71 54	172 17	T.	-25 00	e. by s.	-22 11	-47 11				
-71 54	172 17	W.	-23 32	e. by s. 1/2 s.	-21 36	-45 08				
-71 55	172 17	R.	-24 15	e. 1/2 s.	-22 19	-46 34				

\*  $\psi'$  at West = -59° 05' } Diff. 17° 53' = ship's attraction at West:  
 $\psi'$  at South = -41 12 }

$$\frac{\sin 17^\circ 53'}{a} = \tan \theta; \quad \frac{\sin 17^\circ 53'}{0.267} = 1.150 = \tan 85^\circ 02'.$$

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Jan. 15 P.M.	71° 53'	172° 01'	S.	29° 28'	E. $\frac{1}{2}$ S.	-86° 00'	-22° 19'	51° 47'	-48° 12'	
	71° 53'	172° 01'	O.	27° 43'	E. $\frac{3}{4}$ N.		-22° 00'	49° 43'		
	71° 53'	172° 01'	T.	25° 33'	E. $\frac{1}{2}$ N.		-22° 08'	47° 41'		
	71° 53'	172° 01'	W.	26° 08'	E.		-22° 27'	48° 35'		
	71° 58'	171° 36'	R.	59° 31'	s.s.w. $\frac{1}{2}$ W.		+10° 50'	48° 41'		
17 P.M.	72° 00'	171° 32'	R.	26° 05'	E. $\frac{1}{2}$ S.	-86° 00'	-22° 19'	48° 24'	-51° 41'	
	72° 14'	174° 00'	W.	33° 28'	S.E. by E.		-19° 02'	52° 30'		
	72° 15'	174° 02'	T.	31° 37'	S.E. $\frac{3}{4}$ E.		-18° 20'	49° 57'		
	72° 16'	174° 10'	T.	32° 41'	S.E. $\frac{1}{2}$ E.		-17° 40'	50° 21'		
	72° 17'	174° 14'	T.	35° 05'	S.E. $\frac{1}{2}$ E.		-17° 40'	52° 45'		
18 P.M.	72° 17'	174° 14'	S.	35° 58'	S.E. $\frac{1}{2}$ E.	-86° 10'	-17° 40'	53° 38'	-52° 41'	
	72° 17'	174° 14'	O.	33° 15'	S.E. $\frac{1}{2}$ E.		-17° 40'	50° 55'		
	73° 00'	176° 14'	R.	35° 12'	E.S.E.		-22° 02'	57° 14'		
	73° 02'	176° 10'	T.	65° 04'	s.w. by s.		+13° 23'	51° 41'		
	73° 02'	176° 10'	R.	64° 35'	s.w. by s.		+13° 23'	51° 12'		
	73° 02'	176° 10'	S.	65° 52'	s.w. by s.		+13° 23'	52° 29'		
	73° 02'	176° 10'	O.	65° 50'	s.s.w. $\frac{1}{2}$ W.		+11° 18'	54° 32'		
	73° 02'	176° 03'	R.	65° 54'	s.w. by s.		+13° 23'	52° 31'		
	73° 02'	176° 03'	T.	68° 09'	s.w. $\frac{1}{2}$ S.		+15° 11'	52° 58'		
	73° 02'	175° 57'	R.	65° 02'	s.s.w. $\frac{1}{2}$ W.		+11° 18'	53° 44'		
19 A.M.	73° 02'	175° 51'	R.	63° 34'	s.s.w. $\frac{1}{2}$ W.	-86° 00'	+11° 18'	52° 16'	-50° 31'	
	73° 01'	175° 38'	R.	63° 37'	s.s.w. $\frac{1}{2}$ W.		+11° 18'	52° 16'		
	73° 01'	175° 38'	R.	63° 37'	s.w. by s.		+13° 23'	50° 14'		
	73° 00'	175° 24'	R.	62° 45'	s.s.w. $\frac{1}{2}$ W.		+11° 18'	51° 27'		
	72° 59'	175° 11'	R.	64° 15'	s.s.w. $\frac{3}{4}$ W.		+12° 22'	51° 53'		
	72° 36'	173° 40'	T.	66° 21'	s.w.		+16° 15'	50° 06'		
	72° 36'	173° 40'	W.	66° 12'	s.w. $\frac{1}{2}$ W.		+17° 37'	48° 35'		
	72° 36'	173° 40'	Y.	64° 49'	s.w. by s.		+12° 49'	52° 00'		
	72° 36'	173° 40'	T.	64° 11'	s.w. $\frac{3}{4}$ S.		+13° 45'	50° 26'		
	72° 35'	173° 39'	T.	67° 43'	s.w.		+16° 15'	51° 28'		
19 P.M.	72° 31'	173° 40'	O.	53° 57'	N. by w. $\frac{1}{2}$ W.	-86° 10'	+6° 27'	47° 30'	-51° 54'	
	72° 34'	173° 42'	T.	43° 53'	s. by E. $\frac{1}{2}$ E.		-6° 55'	50° 48'		
	72° 34'	173° 42'	T.	44° 43'	s. by E. $\frac{1}{2}$ E.		-6° 55'	51° 38'		
	72° 34'	173° 45'	Y.	41° 10'	S.S.E.		-9° 14'	50° 24'		
	72° 34'	173° 45'	O.	43° 34'	S.S.E.		-9° 14'	52° 48'		
	72° 34'	173° 45'	R.	43° 43'	S.S.E.		-9° 14'	52° 57'		
	72° 36'	173° 40'	R.	48° 22'	s. by E.		-4° 39'	53° 01'		
	72° 50'	173° 10'	R.	49° 15'	s. by E. $\frac{1}{2}$ E.		-6° 55'	56° 10'		
	74° 10'	169° 28'	S.	34° 25'	E. $\frac{3}{4}$ S.		-28° 37'	63° 02'		
	74° 10'	169° 28'	O.	31° 47'	E. $\frac{1}{4}$ S.		-28° 53'	60° 40'		
22 A.M.	73° 53'	170° 57'	S.	88° 12'	W. by N. $\frac{1}{2}$ N.	-86° 50'	+27° 11'	61° 01'	-63° 38'	
	73° 53'	170° 57'	S.	78° 56'	N.N.W.		+10° 28'	68° 28'		
	73° 53'	170° 57'	S.	35° 43'	E. by N.		-28° 08'	63° 51'		
	73° 57'	171° 40'	T.	48° 46'	N.N.E. $\frac{3}{4}$ E.		-14° 12'	62° 58'		
	73° 57'	171° 40'	T.	38° 00'	E. by N.		-28° 08'	66° 08'		
22 P.M.	73° 57'	171° 40'	T.	36° 56'	E. $\frac{3}{4}$ N.	-86° 50'	-28° 22'	65° 18'	-64° 25'	
	73° 54'	171° 55'	Y.	37° 13'	E. by s.		-28° 29'	65° 42'		
	73° 54'	171° 55'	T.	35° 59'	E. by s. $\frac{1}{2}$ S.		-27° 41'	63° 40'		
	73° 54'	172° 00'	O.	31° 25'	E. by s. $\frac{1}{2}$ S.		-27° 41'	59° 06'		
	73° 55'	172° 04'	O.	36° 52'	E.S.E.		-26° 53'	63° 45'		
	73° 58'	172° 16'	S.	61° 29'	s.		0° 00'	61° 29'		
	73° 59'	171° 58'	S.	65° 50'	s. by w.		+5° 39'	60° 11'		
	73° 59'	171° 58'	T.	67° 45'	s. $\frac{1}{2}$ W.		+2° 49'	64° 56'		
	74° 00'	171° 43'	R.	66° 08'	s. by w.		+5° 39'	60° 29'		
	74° 00'	171° 43'	R.	69° 22'	s. by w.		+5° 39'	63° 43'		
74° 01'	171° 34'	R.	38° 31'	E. $\frac{1}{2}$ S.	-28° 45'	67° 16'				
74° 04'	171° 27'	R.	40° 04'	E. by s. $\frac{1}{2}$ S.	-27° 41'	67° 45'				
74° 04'	171° 27'	T.	36° 00'	E. $\frac{3}{4}$ S.	-28° 37'	64° 37'				
74° 04'	171° 27'	W.	38° 52'	E. $\frac{1}{2}$ N.	-28° 33'	67° 25'				
74° 04'	171° 27'	T.	37° 46'	E. by s.	-28° 29'	66° 15'				

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.	
	Lat.	Long.									
Jan. 25 A.M.	-74 36	168 06	T.	- 78 32	s. by w. $\frac{1}{2}$ w.	-87 20	+ 9 21	- 69 11	- 69 47		
	-74 36	168 06	T.	- 77 36	s. by w. $\frac{1}{2}$ w.		+ 9 21	- 68 15			
	-74 36	168 06	T.	- 37 17	s.e. by e. $\frac{3}{4}$ e.		-31 38	- 68 55			
	-74 40	169 38	T.	- 37 25	s.e. by e.		-29 07	- 66 32			
	-74 41	169 42	Y.	- 39 15	e.s.e.		-32 28	- 71 43			
	-74 41	169 42	Sm.	- 39 54	s.e. by e. $\frac{1}{2}$ e.		-30 45	- 70 39			
	-74 41	169 42	T.	- 43 14	s.e. by e. $\frac{1}{4}$ e.		-30 00	- 73 14			
	25 P.M.	-74 45	169 32	R.	- 81 36		s.s.w.	+12 23		- 69 13	- 71 08
		-74 45	169 32	R.	- 81 08		s.s.w.	+12 23		- 68 45	
		-74 47	168 51	R.	- 86 28		s.s.w. $\frac{1}{2}$ w.	+15 13		- 71 15	
		-74 47	168 51	S.	- 87 19		s.s.w.	+12 23		- 74 56	
		-74 47	168 51	T.	- 85 35		s. by w. $\frac{1}{2}$ w.	+15 13		- 70 22	
-74 44		168 22	R.	- 85 15	s.s.w.	+12 23	- 72 52				
-74 44		168 22	R.	- 93 49	s.w. $\frac{1}{2}$ w.	+25 10	- 68 39				
-74 44		168 10	T.	- 91 01	s.w. by s.	+20 33	- 70 28				
-74 40		168 08	R.	- 43 39	s.e. $\frac{1}{2}$ e.	-25 10	- 68 49				
26 A.M.		-74 55	168 25	T.	- 94 09	s.w. by s.	+18 03	- 76 06			
27 A.M.		-75 44	168 50	S.	- 75 49	s.s.e.	-15 04	- 90 53	- 84 58		
		-75 44	168 50	T.	- 77 04	s.s.e.	-15 04	- 92 08			
	-75 44	168 50	S.	-100 55	s.s.w. $\frac{1}{2}$ w.	+18 32	- 82 23				
	-75 36	168 23	R.	-100 26	s.s.w.	+15 04	- 85 22				
	-75 36	168 23	Y.	- 99 06	s.s.w.	+15 04	- 84 02				
	-75 36	168 23	T.	- 45 19	e.s.e.	-37 42	- 83 01				
	-75 36	168 23	R.	- 46 18	s.e. by e. $\frac{1}{2}$ e.	-35 40	- 81 58				
	-75 36	168 23	S.	- 47 55	s.e. by e. $\frac{1}{2}$ e.	-35 40	- 83 35				
	-75 38	168 33	R.	- 47 41	s.e. by e.	-33 37	- 81 18				
	29 A.M.	-77 37	175 43	Sm.	-104 19	n. $\frac{1}{2}$ e.	- 2 48	-107 07		-104 25	
		-77 40	175 59	T.	-105 44	n. $\frac{1}{4}$ w.	+ 1 24	-104 20			
		-77 40	175 59	T.	-114 11	n. by w. $\frac{1}{2}$ w.	+ 8 20	-105 51			
-77 43		176 00	T.	-118 53	n.n.w. $\frac{1}{2}$ w.	+13 38	-105 15				
-77 43		176 00	S.	-108 20	n. by w. $\frac{1}{2}$ w.	+ 8 20	-100 00				
-77 43		176 00	T.	-116 26	n. by w. $\frac{1}{2}$ w.	+ 8 20	-108 06				
-77 43		176 00	T.	-104 30	n. $\frac{3}{4}$ w.	+ 4 12	-100 18				
29 P.M.		-77 49	177 30	T.	- 90 54	s.e. by s.	-15 22	-106 16	-105 21		
		-77 49	177 46	T.	-104 52	n. $\frac{1}{4}$ w.	+ 1 15	-103 37			
		-77 50	178 13	R.	-110 07	n. $\frac{1}{2}$ w.	+ 2 30	-107 37			
		-77 51	178 33	R.	-100 10	n. $\frac{3}{4}$ e.	- 3 45	-103 55			
		30 A.M.	-77 47	180 34	S.	-106 52	n.n.w. $\frac{1}{2}$ w.	+10 35			- 96 17
	31 A.M.		-77 37	186 41	S.	- 70 55	n.e. $\frac{1}{2}$ n.	-13 39		- 84 34	
			-77 50	188 00	T.	- 60 57	n.e. by e. $\frac{1}{4}$ e.	-19 13		- 80 10	
	-77 50		188 00	T.	- 66 38	n.e. by n.	-11 58	- 78 36			
	-77 50		188 00	Sm.	- 68 56	n.n.e.	- 8 10	- 77 06			
	31 P.M.		-77 08	189 57	S.	- 72 35	n.n.e. $\frac{1}{2}$ e.	-10 04		- 82 39	
			-77 08	189 57	R.	- 74 06	n.n.e. $\frac{1}{2}$ e.	-10 04		- 84 10	
	Feb. 1 A.M.		-77 11	189 01	Sm.	-103 58	s.w. by w. $\frac{1}{2}$ w.	+20 02		- 83 56	- 82 29
-77 11			189 01	T.	-102 56	s.w. by w.	+19 02	- 83 54			
-77 11			189 00	T.	-103 52	w. by s. $\frac{1}{2}$ s.	+21 36	- 82 16			
-77 11			189 00	T.	- 90 06	n.n.w.	+ 8 10	- 81 56			
-77 11			189 00	O.	- 70 58	s.e. by s.	-12 49	- 83 47			
-77 08		189 05	S.	- 73 58	s.e. by s.	-12 49	- 86 47				
1 P.M.		-77 08	188 26	R.	- 85 52	s. by e.	- 4 17	- 90 09			
		-77 08	188 26	R.	- 84 25	s.s.e.	- 8 30	- 92 55			
		-77 09	188 24	R.	- 79 49	s.e. by s.	-12 18	- 92 07			
		-77 09	188 24	R.	- 66 58	e. $\frac{1}{4}$ s.	-21 27	- 88 25			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Feb. 1 P.M.	-77° 09'	188° 24'	R.	-70° 19'	E.S.E.	-85° 50'	-20° 13'	-90° 32'	-91° 07'	
	-77° 09'	188° 24'	R.	-75° 38'	S.E.		-15° 37'	-91° 15'		
	-77° 09'	188° 24'	R.	-82° 22'	S.S.E.		-8° 30'	-90° 52'		
	-77° 09'	188° 15'	R.	-79° 56'	S.E. by S.		-12° 18'	-92° 14'		
	-77° 09'	188° 15'	T.	-79° 14'	S.E. by S.		-12° 18'	-91° 32'		
	2 A.M.	-77° 34'	186° 56'	S.	-72° 39'		E.S.E.	-22° 02'		-94° 41'
		-77° 34'	186° 03'	O.	-70° 42'		S.E. by E. 1/2 E.	-20° 58'		-91° 40'
		-77° 34'	186° 15'	S.	-69° 05'		E.	-23° 36'		-92° 41'
		-77° 34'	186° 15'	O.	-71° 39'		E.S.E.	-22° 02'		-93° 41'
		-77° 35'	186° 55'	T.	-72° 32'		S.E. by E. 1/4 E.	-20° 27'		-92° 59'
		-77° 35'	186° 55'	T.	-73° 09'		S.E. by E. 1/2 E.	-20° 58'		-94° 07'
	2 P.M.	-77° 35'	186° 55'	T.	-75° 37'		S.E.	-17° 00'		-92° 37'
-77° 35'		186° 55'	S.	-76° 49'	S.E.	-17° 00'	-93° 49'			
-77° 43'		186° 50'	W.	-72° 04'	E.S.E.	-22° 02'	-94° 06'			
-77° 45'		187° 00'	R.	-69° 50'	S.E. by E.	-19° 55'	-89° 45'			
-77° 45'		187° 00'	R.	-72° 25'	S.E. by E. 1/2 E.	-20° 58'	-93° 23'			
-77° 47'		186° 52'	T.	-69° 57'	E. by S. 1/2 S.	-22° 39'	-92° 36'			
-77° 47'		186° 52'	Sm.	-72° 53'	E.S.E.	-22° 02'	-94° 55'			
-77° 45'		186° 52'	R.	-73° 10'	E.S.E.	-22° 02'	-95° 12'			
-77° 45'		186° 52'	R.	-72° 56'	E. by S. 1/2 S.	-22° 39'	-95° 35'			
-77° 46'		186° 51'	S.	-74° 47'	E.S.E.	-22° 02'	-96° 49'			
-77° 46'		186° 51'	T.	-74° 38'	S.E. by E. 1/2 E.	-20° 58'	-95° 36'			
-77° 47'		186° 51'	R.	-75° 01'	E.S.E.	-22° 02'	-97° 03'			
-77° 56'	186° 51'	T.	-72° 32'	E. 1/2 N.	-23° 16'	-95° 48'				
-77° 57'	186° 44'	R.	-71° 21'	E.	-23° 36'	-94° 57'				
-77° 57'	186° 44'	R.	-75° 38'	E.N.E.	-21° 23'	-97° 01'				
-77° 57'	186° 44'	T.	-74° 27'	E 1/4 N.	-23° 26'	-97° 53'				
-77° 59'	186° 47'	R.	-72° 03'	E.	-23° 36'	-95° 39'				
-78° 00'	186° 45'	R.	-72° 10'	E.S.E.	-22° 02'	-94° 12'				
3 A.M.	-77° 32'	186° 00'	Sm.	-117° 40'	W. by S. 1/2 S.	+22° 40'	-95° 00'			
	-77° 32'	186° 00'	T.	-118° 47'	W.S.W.	+22° 02'	-96° 45'			
4 A.M.	-77° 05'	192° 32'	S.	-77° 52'	S. by E.	-4° 18'	-82° 10'			
	-77° 06'	192° 33'	T.	-77° 44'	S. 1/4 E.	-1° 04'	-78° 48'			
	-77° 06'	192° 33'	O.	-76° 31'	S. 1/2 E.	-2° 08'	-78° 39'			
	-77° 54'	192° 30'	Y.	-62° 21'	E.N.E.	-19° 31'	-81° 52'			
	-77° 54'	192° 30'	S.	-60° 36'	E.N.E.	-19° 31'	-80° 07'			
	-77° 54'	192° 30'	O.	-63° 11'	N.E. by E.	-17° 24'	-80° 35'			
4 P.M.	-76° 57'	192° 37'	T.	-59° 54'	N.E. by E. 1/2 E.	-18° 27'	-78° 21'			
	-77° 6'	192° 34'	R.	-61° 29'	E. by N. 1/2 N.	-19° 24'	-80° 53'			
	-77° 9'	192° 43'	R.	-62° 14'	E. by N.	-20° 04'	-82° 18'			
	-77° 9'	192° 43'	T.	-62° 31'	E. by N.	-20° 04'	-82° 35'			
	-77° 13'	192° 51'	R.	-68° 53'	E. by N. 1/2 N.	-19° 24'	-88° 17'			
	-77° 13'	192° 51'	T.	-67° 45'	N.E. by E. 3/4 E.	-18° 13'	-85° 58'			
5 A.M.	-77° 13'	192° 49'	R.	-93° 17'	S.S.W. 1/2 W.	+10° 00'	-83° 17'			
	-77° 24'	192° 56'	S.	-81° 22'	S.	0° 00'	-81° 22'			
	-77° 8'	192° 59'	O.	-63° 33'	E.	-20° 38'	-84° 11'			
	-77° 8'	192° 59'	T.	-77° 06'	S. by E.	-4° 08'	-81° 14'			
	-77° 8'	192° 59'	T.	-83° 12'	S.	0° 00'	-83° 12'			
	-77° 8'	192° 59'	T.	-92° 23'	S.S.W. 1/2 W.	+10° 01'	-82° 22'			
-77° 8'	192° 59'	W.	-92° 16'	S.S.W. 1/2 W.	+10° 01'	-82° 15'				
5 P.M.	-77° 19'	192° 50'	T.	-83° 00'	S. 1/4 W.	+1° 00'	-82° 00'			
	-77° 16'	191° 32'	R.	-89° 26'	S. by W. 1/2 W.	+6° 10'	-83° 16'			
	-77° 16'	191° 32'	R.	-80° 06'	S. by E. 1/2 E.	-6° 10'	-86° 16'			
	-77° 16'	191° 32'	R.	-70° 42'	S.E. 1/2 S.	-13° 26'	-84° 08'			
	-77° 16'	191° 32'	R.	-63° 24'	E. 1/2 S.	-20° 30'	-83° 54'			
	-77° 16'	191° 32'	R.	-66° 30'	S.E. by E.	-17° 34'	-84° 04'			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Feb. 6 A.M.	-77° 14'	190° 2'	S.	- 87° 49'	s. by w.	- 86 00	+ 4' 28"	- 83° 21'	- 82 09	
	-77° 05'	189° 2'	T.	- 88 18	s. by w.		+ 4 28	- 83 50		
7 A.M.	-77° 09'	188° 50'	Sm.	- 83 07	s. $\frac{3}{4}$ w.	- 86 05	+ 3 20	- 79 47	- 81 33	
	-77° 09'	188° 50'	T.	- 85 52	s. $\frac{3}{4}$ w.		+ 3 20	- 82 32		
	-77° 09'	188° 50'	T.	- 58 23	E. by N.		- 21 50	- 80 13		
	-77° 04'	188° 40'	T.	- 80 58	s. $\frac{1}{2}$ E.		- 2 14	- 83 12		
	-76° 58'	186° 40'	T.	- 94 54	S.S.W. $\frac{1}{4}$ w.		+ 10 02	- 84 52		
	-76° 58'	186° 40'	T.	- 91 17	S.S.W.		+ 9 02	- 82 15		
	-76° 58'	186° 40'	T.	- 87 10	s. by w. $\frac{1}{2}$ w.		+ 6 45	- 80 25		
	-76° 58'	186° 40'	T.	- 59 46	E. $\frac{1}{2}$ S.		- 22 52	- 82 38		
	-76° 56'	186° 39'	S.	- 59 16	E. $\frac{1}{2}$ S.		- 22 52	- 82 08		
	-76° 56'	186° 39'	O.	- 56 07	E. $\frac{1}{4}$ N.		- 22 53	- 79 00		
7 P.M.	-76° 56'	186° 39'	T.	- 57 38	E. $\frac{1}{2}$ S.	- 86 00	- 22 52	- 80 30	- 87 29	
	-76° 56'	186° 39'	O.	- 57 12	E. by S.		- 22 43	- 79 55		
	-76° 57'	186° 36'	S.	- 60 09	E. by S. $\frac{1}{2}$ S.		- 22 06	- 82 15		
	-77° 11'	187° 03'	T.	- 68 38	E. by S. $\frac{1}{4}$ S.		- 21 54	- 80 32		
	-77° 11'	187° 03'	R.	- 68 31	E. by S. $\frac{1}{2}$ S.		- 21 36	- 90 07		
	-77° 12'	187° 03'	T.	- 70 01	S.E. by E. $\frac{1}{2}$ E.		- 20 02	- 90 03		
	-77° 12'	187° 03'	T.	- 66 16	S.E. by E.		- 19 02	- 85 18		
	-77° 12'	187° 03'	R.	- 67 27	S.E. by E.		- 19 02	- 86 29		
	-77° 12'	187° 03'	R.	- 81 21	S.S.E.		- 8 52	- 90 13		
	-77° 14'	187° 01'	R.	- 74 43	S.E. by S.		- 12 49	- 87 32		
8 A.M.	-77° 14'	187° 01'	R.	- 72 20	S.E.	- 86 00	- 16 15	- 88 35	- 89 19	
	-77° 14'	187° 01'	T.	- 72 00	S.E.		- 16 15	- 88 15		
	-77° 13'	186° 54'	W.	- 71 29	S.E.		- 16 15	- 87 44		
	-77° 24'	186° 19'	S.	- 65 24	E.S.E.		- 21 02	- 86 26		
	-77° 24'	186° 19'	O.	- 65 32	E.S.E.		- 21 02	- 86 34		
	-77° 21'	186° 22'	T.	- 68 19	E. by S. $\frac{1}{2}$ S.		- 21 37	- 89 56		
	-77° 21'	186° 22'	Y.	- 67 35	E. $\frac{1}{2}$ S.		- 22 19	- 89 54		
	-77° 21'	186° 22'	Y.	- 71 43	E.S.E.		- 21 02	- 92 45		
	-77° 21'	186° 22'	T.	- 69 19	E.S.E.		- 21 02	- 90 21		
	-77° 21'	186° 22'	O.	- 67 29	E.S.E.		- 21 02	- 88 31		
8 P.M.	-77° 21'	186° 22'	S.	- 67 38	E.S.E.	- 86 00	- 21 02	- 88 40	- 90 21	
	-77° 30'	186° 40'	T.	- 71 42	E.S.E.		- 21 02	- 91 44		
	-77° 30'	186° 40'	W.	- 70 31	E.S.E.		- 21 02	- 91 33		
	-77° 30'	186° 40'	T.	- 69 39	E.		- 22 27	- 92 06		
	-77° 37'	186° 36'	R.	- 67 40	E. by N.		- 21 50	- 89 30		
	-77° 47'	187° 18'	R.	- 72 51	E. by N. $\frac{1}{2}$ N.		- 21 6	- 93 57		
	-77° 47'	187° 10'	S.	- 74 04	E.N.E.		- 20 23	- 94 27		
	-77° 48'	187° 29'	O.	- 74 17	E.N.E.		- 20 23	- 94 40		
	-77° 48'	187° 29'	T.	- 75 35	E.N.E.		- 20 23	- 95 58		
	-77° 50'	187° 35'	T.	- 76 38	N.E. by E. $\frac{1}{2}$ E.		- 19 18	- 95 56		
9 A.M.	-77° 50'	187° 35'	W.	- 79 50	E.N.E.	- 86 00	- 20 23	- 100 13	- 96 00	
	-77° 49'	187° 25'	R.	- 76 04	E.N.E.		- 20 23	- 96 27		
	-77° 49'	187° 25'	T.	- 79 29	N.E. by E.		- 18 11	- 97 40		
	-77° 50'	187° 31'	R.	- 75 32	N.E. by E.		- 18 11	- 93 43		
	-77° 51'	187° 36'	R.	- 77 19	N.E. by E. $\frac{1}{2}$ E.		- 19 18	- 96 37		
	-77° 53'	187° 44'	R.	- 80 42	N.E.		- 15 20	- 96 02		
	-77° 57'	188° 06'	T.	- 95 31	N.		0 00	- 95 31		
	-77° 52'	191° 16'	W.	- 108 01	S.W. $\frac{1}{2}$ S.		+ 13 57	- 94 04		
	-77° 52'	191° 16'	T.	- 109 17	S.W. $\frac{1}{2}$ S.		+ 13 57	- 95 20		
	-77° 52'	191° 07'	Y.	- 108 43	S.W. $\frac{1}{2}$ S.		+ 13 57	- 94 46		
	-77° 52'	191° 07'	T.	- 103 50	S.W. by S.	- 85 50	+ 12 18	- 91 32	- 93 43	
	-77° 48'	190° 23'	T.	- 101 26	S.S.W.		+ 8 30	- 92 56		

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Feb. 9 P.M.	-77 57	188 30	R.	-102 30	s.s.w.	-86 00	+ 8 52	- 93 38	- 93 41	
	-77 56	188 40	R.	-110 29	s.w. 1/2 s.		+14 32	- 95 57		
	-77 56	188 40	R.	-106 13	s.s.w. 3/4 w.		+11 50	- 94 23		
	-77 54	188 36	R.	-105 51	s.w. by s.		+12 49	- 93 02		
	-77 54	188 36	S.	-103 13	s.s.w. 1/2 w.		+10 50	- 92 23		
	-77 51	188 24	R.	-103 18	s.s.w. 1/2 w.		+10 50	- 92 28		
	-77 50	188 06	R.	- 94 04	s. 1/4 w.		+ 1 04	- 93 00		
10 A.M.	-77 50	188 06	S.	- 94 38	s.	0 0	- 94 38	- 93 41		
	-77 35	187 59	S.	- 94 12	s.	0 0	- 94 12			
	-77 57	187 38	T.	-110 56	s.w. 1/2 w.	+17 38	- 93 18			
	-77 38	188 07	Y.	- 97 53	s. by w.	+ 4 28	- 93 25			
	-77 38	188 07	T.	-101 54	s.s.w.	+ 8 52	- 93 02			
	-77 40	188 00	SM.	-108 00	s.w. by s.	+12 49	- 95 11			
	-77 48	188 00	S.	-108 49	s.w. by s.	+12 49	- 96 00			
11 A.M.	-77 48	188 00	O.	-105 38	s.w. 1/2 s.	+14 32	- 91 06	- 77 53		
	-77 48	188 04	T.	-106 04	s.w. by s.	+12 49	- 93 15			
	-76 45	189 06	O.	- 74 47	s. 1/4 E.	- 1 06	- 75 53			
	-76 46	188 40	S.	- 86 56	s. by w. 1/2 w.	+ 6 40	- 80 16			
	-76 46	188 40	S.	- 80 11	s.	0 00	- 80 11			
	-76 46	188 40	S.	- 95 11	s.w. 1/2 s.	+14 32	- 80 39			
	-76 14	187 11	S.	- 86 06	N.W. 1/2 N.	+13 39	- 72 27			
11 P.M.	-76 23	178 25	S.	- 98 02	s. by w. 1/2 w.	+ 8 50	- 89 12	- 85 10		
	-76 24	176 26	R.	- 91 24	s. by w. 3/4 w.	+10 17	- 81 07			
14 A.M.	-76 03	168 56	R.	- 85 31	s. by E. 1/4 E.	-10 13	- 95 44	- 98 45		
	-76 05	168 56	S.	- 88 32	s. by E. 1/2 E.	-12 13	-100 45			
	-76 05	168 56	O.	- 86 55	s. by E. 1/2 E.	-12 13	- 99 08			
15 P.M.	-76 16	168 11	R.	- 85 10	s. by E. 3/4 E.	-14 13	- 99 23	- 106 13		
	-76 20	165 33	S.	- 60 54	E. 1/2 N.	-45 47	-106 41			
	-76 20	165 33	T.	- 69 12	S.E. by E.	-37 32	-106 44			
	-76 20	165 33	O.	- 67 08	S.E. by E.	-37 32	-104 40			
	-76 20	165 33	Y.	- 65 20	E.S.E.	-42 18	-107 38			
	-76 20	165 33	T.	- 64 59	E.S.E.	-42 18	-107 17			
	-76 30	166 39	R.	- 58 06	E.	-46 13	-104 19			
16 A.M.	-76 35	166 17	R.	- 64 23	E. by s. 1/2 s.	-44 03	-108 26	-113 23		
	-76 36	166 17	R.	-136 19	N.N.W. 1/2 w.	+19 46	-116 33			
	-76 36	166 17	Y.	-150 04	W.N.W.	+41 38	-108 26			
	-76 36	166 16	T.	-138 24	N.W. by N.	+23 31	-114 53			
	-76 36	166 16	Y.	-158 51	w.	+46 13	-112 38			
	-76 36	166 16	Y.	-156 58	w. by s. 1/2 s.	+44 03	-112 55			
	-76 36	166 16	T.	-156 05	s.w. 1/4 w.	+33 04	-123 01			
	-76 36	166 17	R.	-154 06	s.w. by w.	+37 32	-116 34			
	-76 36	166 17	R.	-142 54	s.w. 1/4 s.	+29 45	-113 09			
	-76 37	166 16	R.	- 67 01	E.N.E.	-41 38	-108 39			
	-76 37	166 16	R.	- 67 53	E. by s.	-45 19	-111 51			
	-76 37	166 16	S.	- 66 32	E. by s.	-45 19	-113 12			
	-76 37	166 16	T.	- 73 45	E.S.E.	-42 18	-116 03			
-76 37	166 35	R.	- 73 40	S.E. by E.	-37 32	-111 12				

\* The inclination on the 16th of February is computed from the observed declinations with the head West - 158° 51', and E. by S. - 67° 12'. From these we have the approximate inclination  $\theta = - 87^\circ 52'$ . With this value of  $\theta$ ,  $\psi' = - 66^\circ 27'$  at East. Whence  $\psi = - \frac{158^\circ 51' + 66^\circ 27'}{2} = - 112^\circ 39'$ ;  $\delta$  at East or West =  $46^\circ 12'$ ; and  $\tan \theta = \frac{\sin 46^\circ 12'}{a} = \frac{.7218}{.0267} = - 87^\circ 53'$ .

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Feb. 17 A.M.	-76 44	165 48	S.	-122 02	s. by w.	-88 05	+ 9 18	-112 44	-113 41	
	-76 44	165 48	O.	-123 18	s. by w.		+ 9 18	-114 00		
	-76 44	165 48	Y.	-124 51	s. by w.		+ 9 18	-115 33		
17 P.M.	-76 27	164 18	R.	-113 59	s.	-88 05	0 00	-113 59	-113 41	
	-76 27	164 11	R.	-112 11	s.		0 00	-112 11		
	-76 26	164 02	R.	- 73 51	S.E. 1/2 E.		-38 49	-112 40		
	-76 26	164 02	T.	- 71 53	S.E. by E. 1/4 E.		-43 52	-115 45		
18 A.M.	-76 26	164 02	R.	- 73 51	S.E. 1/2 E.	-88 04*	-38 49	-112 40	-99 41	
	-76 16	165 53	T.	- 49 06	E. by s.		-51 20	-100 26		
	-76 16	165 53	T.	- 51 14	E. by s. 1/2 s.		-49 37	-100 51		
18 P.M.	-76 05	166 11	T.	- 71 05	N.E. by N.	-88 04	-25 56	- 97 01	-94 27	
	-76 06	166 11	T.	-152 46	w.		+52 20	-100 26		
	-76 03	166 23	S.	-142 55	w.N.w.		+46 47	- 96 08		
	-76 03	166 23	S.	-144 38	w. by N.		+51 20	- 93 18		
	-75 58	167 04	T.	- 71 05	N.E. by N.		-25 56	- 97 01		
	-75 58	167 04	T.	-149 32	w.		+52 20	- 97 12		
	-75 49	167 32	R.	-134 35	s.w. by w.		+42 07	- 92 28		
	-75 45	167 32	R.	-132 32	s.w. by w.		+42 07	- 90 25		
	-75 42	167 30	S.	-135 47	s.w. by w.		+42 07	- 93 40		
	-75 42	167 30	R.	-133 08	s.w. 1/2 w.		+37 47	- 95 21		
19 P.M.	-74 46	167 53	R.	-110 59	s.w.	-88 02	+34 12	- 76 47	-74 48	
	-74 46	167 53	T.	-107 01	s.w.		+34 12	- 72 49		
22 P.M.	-70 27	166 40	R.	- 18 35	E. by s. 1/4 s.	-85 50	-20 57	- 39 32	-39 45	
	-70 27	166 40	T.	- 16 21	E. by N. 1/2 N.		-20 13	- 36 34		
24 A.M.	-70 14	168 13	Y.	- 50 20	N.W. 1/2 N.	-85 50	+13 03	- 37 17	-39 45	
	-70 14	168 13	T.	- 49 18	N.W. 1/2 N.		+13 03	- 36 15		
24 P.M.	-70 24	167 20	S.	- 41 55	s. 1/2 E.	-85 50	- 2 08	- 44 03	-39 21	
	-70 26	167 19	R.	- 42 49	s.		0 00	- 42 49		
	-70 26	167 19	O.	- 41 44	s.		0 00	- 41 44		
25 P.M.	-70 07	167 27	R.	- 40 24	s. 1/2 w.	-85 50	+ 2 08	- 38 16	-39 21	
	-70 07	167 27	T.	- 40 16	s. 1/2 w.		+ 2 08	- 38 08		
	-70 06	167 29	R.	- 41 14	s.		0 00	- 41 14		
	-70 06	167 29	R.	- 44 06	N. by w. 3/4 w.		+ 6 52	- 37 14		
	-70 04	167 32	T.	- 49 16	N.N.W.		+ 7 50	- 41 26		
	-70 04	167 32	T.	- 56 14	N.W. by w. 1/2 w.		+18 27	- 37 47		
	-70 02	167 35	R.	- 52 55	N.W. by w.		+17 24	- 35 31		
	-70 02	167 11	S.	- 42 51	s. by w.		+ 4 17	- 38 34		
	-70 03	167 26	R.	- 46 21	s. by w.		+ 4 17	- 42 04		
	-70 03	167 26	S.	- 61 35	s.w. by w.		+18 16	- 43 19		
26 A.M.	-69 54	167 56	S.	- 61 35	s.w. by w.	-85 28	+18 16	- 43 19	-38 21	
	-69 17	168 00	R.	- 48 44	N.W.		+13 27	- 35 17		
	-69 17	168 00	O.	- 50 39	N.W. 1/2 w.		+15 12	- 35 27		
27 P.M.	-69 16	167 49	S.	- 45 13	s. by w.	-85 28	+ 3 58	- 41 15	-38 21	
	-69 25	167 39	R.	- 40 39	s. by w.		+ 3 58	- 36 41		
	-69 40	167 14	Sm.	- 34 21	s. by E.		- 4 12	- 38 33		
28 A.M.	-69 40	167 14	T.	- 35 28	s. by E. 1/2 E.	-85 45	- 6 18	- 41 46	-38 21	
	-69 40	167 25	T.	- 35 17	s. by E. 1/2 E.		- 6 18	- 41 35		
	-69 40	167 25	O.	- 36 51	s. by E.		- 4 12	- 41 03		
	-69 40	167 27	S.	- 37 06	s. 1/2 E.		- 2 05	- 39 11		
28 P.M.	-69 47	167 13	R.	- 56 47	w.N.w.	-85 45	+19 07	- 37 40	-38 21	
	-69 36	167 14	R.	- 50 21	N.W. by w.		+17 02	- 33 19		

\* The inclination is computed from the observed declination at West - 152° 46', and at E. by S. - 49° 06'; with the approximate inclination which these give we have  $\psi'$  at East - 48° 06';  $\psi = -\frac{152^\circ 46' + 48^\circ 06'}{2} = -100^\circ 26'$ ;  $\delta$  at East and West 52° 20'; and  $\theta = -\frac{\sin 52^\circ 20'}{.0267} = -88^\circ 04'$ .



Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.
	Lat.	Long.								
Mar. 1 A.M.	-69 22	167 40	S.	-47 21	N.W.	-85 10	+12 31	-34 50	-36 12	
1 P.M.	-68 51	167 47	R.	-48 53	N.W. by W. 1/2 W.		+15 45	-33 08		
	-68 56	167 49	O.	-33 25	S.		0 00	-33 25		
	-68 56	167 49	S.	-33 40	S. 1/2 E.		-1 52	-35 32		
	-68 56	167 49	W.	-35 23	S. 1/2 E.		-1 52	-37 15		
	-68 55	167 46	S.	-36 27	S. 1/2 E.		-1 52	-37 19		
	-68 55	167 46	T.	-31 54	S. by E.		-3 45	-35 39		
	-68 55	167 49	R.	-30 30	S.S.E.		-7 22	-37 52		
	-68 55	167 49	T.	-32 46	S. 1/2 E.		-1 52	-34 38		
	-68 57	167 46	R.	-30 24	S. by E. 1/2 E.		-5 33	-35 57		
	-69 02	167 42	R.	-30 30	S.E. by S.		-10 40	-41 10		
	-69 03	167 41	R.	-56 02	W. 1/2 S.		+18 19	-37 43		
2 P.M.	-68 13	167 56	R.	-49 58	W. by N.		+15 07	-34 51		
	-68 12	167 53	T.	-50 32	W. 1/4 S.		+15 38	-34 54		
	-68 12	167 53	W.	-48 26	W. 1/4 N.		+15 30	-32 56		
	-68 12	167 53	T.	-46 36	W. 1/4 N.	+15 30	-31 06			
	-68 09	167 45	R.	-45 44	W. 1/2 N.	+15 22	-30 22			
3 A.M.	-67 40	167 40	T.	-48 33	W. 1/2 S.	+15 20	-33 13			
3 P.M.	-67 24	166 34	R.	-47 00	W. by S. 1/2 S.	+14 52	-32 08			
	-67 23	166 33	S.	-46 12	W. by S.	+15 15	-30 57			
5 P.M.	-65 30	167 34	R.	-32 28	S.W. 1/2 S.	+9 23	-23 05			
6 A.M.	-65 40	165 06	T.	-36 36	S.S.W. 1/2 W.	+7 00	-29 36			
	-65 42	164 56	T.	-35 04	S.S.W.	+5 45	-29 19			
	-65 42	164 56	SM.	-32 27	S.S.W. 1/2 W.	+7 00	-25 27			
	-65 42	164 56	O.	-30 51	S. by W.	+2 57	-27 54			
	-65 42	164 56	T.	-33 09	S. by W. 1/2 W.	+4 21	-28 48			
	-65 44	165 05	Y.	-35 17	S. by W. 1/2 W.	+4 21	-30 56			
	-65 44	165 05	S.	-38 41	S.W. 1/2 S.	+9 23	-29 18			
	-65 44	165 05	W.	-33 03	S.S.W. 1/2 W.	+7 00	-26 03			
	-65 44	165 05	W.	-37 39	S.W. by S.	+8 17	-29 22			
	-65 44	165 05	S.	-37 02	S.W. by S.	+8 17	-28 45			
	-65 50	164 41	R.	-35 55	S.S.W.	+5 45	-30 10			
	-65 50	164 42	R.	-38 38	S.W. by S.	+8 17	-30 21			
7 A.M.	-65 25	162 06	Y.	-32 12	N.W. 1/2 N.	+8 38	-23 34			
	-65 25	162 06	T.	-27 09	N. 3/4 W.	+1 12	-25 57			
	-65 25	162 06	O.	-30 52	N. by W.	+2 32	-28 20			
	-65 25	162 06	W.	-30 37	N.N.W. 1/2 W.	+6 22	-24 15			
	-65 25	162 06	T.	-30 50	N.N.W.	+5 09	-25 41			
8 P.M.	-64 37	163 07	S.	-14 56	E. by N. 1/2 N.	-11 42	-26 38			
	-64 37	163 07	R.	-15 13	E. by N. 1/2 N.	-11 42	-26 55			
9 P.M.	-64 32	163 59	R.	-34 46	S.W. by S.	+7 39	-27 07			
10 P.M.	-64 02	163 31	S.	-26 40	S. 3/4 W.	+2 00	-24 40			
11 A.M.	-64 17	163 17	T.	-32 51	N.W.	+8 26	-24 25			
	-64 16	163 18	T.	-34 35	N.W. 1/2 W.	+9 12	-25 23			
	-64 16	163 18	Y.	-37 50	N.W. by W.	+9 59	-27 51			
	-64 16	163 18	W.	-35 16	N.W. by W.	+9 59	-25 17			
	-64 16	163 18	SM.	-36 46	W.N.W.	+11 17	-25 29			
	-64 16	163 19	T.	-36 10	W.N.W.	+11 17	-24 53			
11 P.M.	-64 02	163 06	S.	-32 38	S.W. by S.	+7 39	-24 59			
	-64 04	163 06	O.	-32 04	S.S.W. 1/2 W.	+6 25	-25 39			
	-64 04	163 02	T.	-33 33	S.W. by S.	+7 39	-25 54			
	-64 03	163 49	S.	-36 22	S.W. by W.	+10 53	-25 29			
	-64 03	162 45	W.	-34 23	S.W. by W. 1/2 W.	+11 25	-22 58			
12 A.M.	-63 57	161 11	T.	-28 07	S. by W.	+2 42	-25 25			
	-63 58	161 15	S.	-34 04	S.W. by S.	+7 39	-26 25			
12 P.M.	-64 07	161 16	T.	-35 27	W.N.W.	+11 17	-24 10			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.		
	Lat.	Long.										
Mar. 12 P.M.	-64 07	161 16	W.	-35 19	w.N.W.	-83 00	+11 17	-24 02	-24 06			
	-64 07	161 16	R.	-36 25	w. by N. 1/2 N.		+11 42	-24 43				
	-64 07	161 16	T.	-36 17	w. 1/2 N.		+12 20	-23 57				
	-64 07	161 16	T.	-35 30	w. 1/2 S.		+12 30	-23 00				
	-64 06	161 10	R.	-35 11	w. by S.		+12 30	-22 41				
14 P.M.	-64 06	161 05	R.	-35 02	w. by S.	+12 30	-22 32					
	-62 48	157 14	R.	-18 31	S.E. by S.	-82 33	-7 07	-25 38	-24 07			
	-62 48	157 14	O.	-21 04	S.S.E.		-4 53	-25 57				
	-62 48	157 14	S.	-21 31	S.S.E.		-4 53	-26 24				
	-62 50	157 14	R.	-19 00	S. by E. 1/2 E.		-3 43	-22 43				
-62 50	157 14	R.	-12 11	S.E. by E.	-10 14		-22 35					
17 A.M.	-62 50	157 14	Y.	-23 23	S.S.E.	-4 53	-28 16					
	-62 55	157 02	W.	-22 29	S. by E.	-2 32	-25 01					
	-64 19	153 40	T.	-28 35	S.W. by S.	-84 00	+8 39	-19 56	-18 59			
	-64 19	153 40	W.	-29 15	S.W. by S.		+8 39	-20 36				
	18 A.M.	-63 54	151 56	SM.	-6 11		E.N.E.	-13 28		-19 39		
-63 54		151 52	S.	-5 25	E.		-14 55	-20 20				
-63 54		151 52	O.	-7 29	S.E. by E.		-12 48	-20 17				
-63 50		151 48	T.	-7 33	S.E. by E.	-12 48	-20 21					
-63 50		151 48	SM.	-7 15	S.E. by E.	-12 48	-20 03					
18 P.M.	-63 50	151 48	S.	-8 05	S.E. by E.	-12 48	-20 53					
	-63 50	151 48	O.	-8 21	S.E. by E. 1/2 E.	-13 16	-21 37					
	-63 50	151 48	R.	-18 02	S. by E.	-3 00	-21 02					
	-63 50	151 48	T.	-19 05	S. by W.	+3 00	-16 05					
	-63 50	151 48	S.	-17 08	S.	0 00	-17 08					
19 A.M.	-63 50	151 48	R.	-14 09	S.S.E.	-6 00	-20 09					
	-63 51	151 48	R.	-13 20	S. by E. 1/2 E.	-4 30	-17 50					
	-64 14	149 10	T.	-27 16	S.W. by S.	-84 20	+9 08	-18 08	-16 41			
	-64 16	149 15	R.	-27 13	S.W. by S.		+9 08	-18 05				
	-64 16	149 15	W.	-26 08	S.W. by S.		+9 08	-17 00				
-64 18	149 09	R.	-25 43	S.W. 1/2 S.	+10 20		-15 23					
-64 24	148 27	R.	-26 04	S.W. by S.	+9 08		-16 56					
20 P.M.	-65 04	142 49	R.	-31 29	w.	+19 26	-12 03					
	-65 03	142 46	R.	-30 34	S.W. by W. 1/2 W.	+17 23	-13 11					
	-64 26	140 46	SM.	-24 11	W.N.W.	-84 55	+15 50	-8 21	-6 57			
	-64 26	140 46	Y.	-21 11	W.N.W.		+15 50	-5 21				
	-64 26	140 46	SM.	-22 47	W.N.W.		+15 50	-6 57				
-64 26	140 46	O.	-21 18	N.W. by W.	+14 00		-7 18					
-64 18	140 27	S.	-19 40	N.W. by W.	+14 00		-5 40					
21 P.M.	-64 01	140 31	W.	-23 56	W.N.W.	+15 50	-8 06					
	22 A.M.	-63 18	140 04	S.	-3 46	N.	0 00	-3 46				
		-63 18	140 04	O.	-1 55	N. 1/2 E.	-1 23	-3 18				
		-63 18	140 04	T.	-6 16	N. by W.	+2 44	-3 32				
		-63 18	140 04	T.	-19 52	w. by N. 1/2 N.	+3 57	-5 55				
-63 18		140 04	Y.	-18 31	W.N.W.	+13 27	-5 04					
22 P.M.	-63 20	139 52	S.	-20 19	W.N.W.	+13 27	-6 52					
	-63 14	139 43	R.	-19 39	N.W. by W. 1/2 W.	+12 37	-7 02					
	-63 14	139 43	R.	-22 28	w.	+14 54	-7 34					
	-63 09	139 28	R.	-21 01	W.N.W.	+13 27	-7 34					
	-63 03	139 38	R.	-20 52	N.W. by W. 1/2 W.	+12 37	-8 15					
22 P.M.	-63 03	139 38	R.	-14 41	N.W. 1/2 N.	+9 04	-5 37					
	-63 03	139 38	R.	-22 01	w.	+14 54	-7 07					
	-62 53	139 06	R.	-15 17	N.W. by W.	+11 39	-3 38					
	-62 52	139 05	R.	-14 43	N.W. 3/4 W.	+11 14	-3 29					
	-62 32	137 40	R.	-20 26	w.	+14 43	-5 43					

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.			
	Lat.	Long.											
Mar. 22 P.M.	-62 32	137 40	R.	-16 55	w. by N. $\frac{1}{2}$ N.	-84 00	+13 46	- 3 09	- 4 05				
	-62 28	137 26	R.	-18 35	w. by s. $\frac{1}{2}$ s.		+14 17	- 4 18					
23 A.M.	-62 28	137 26	R.	-18 29	w. by N.	-83 45	+14 15	- 4 14	- 1 12				
	-62 05	136 05	Sm.	-12 53	N.w. $\frac{1}{2}$ w.		+10 18	- 2 35					
	-62 18	136 25	T.	-14 00	N.w. by w.		+11 08	- 2 52					
	-62 18	136 25	W.	-13 48	N.w. by w.		+11 08	- 2 40					
	-62 20	136 27	R.	-11 53	N.w. by w.		+11 08	- 0 45					
	-62 17	136 29	R.	-11 41	N.w. by w.		+11 08	- 0 33					
	-62 16	136 26	R.	- 9 59	N.w. by w.		+11 08	+ 1 09					
	-62 13	136 20	R.	-11 19	N.w. by w.		+11 08	- 0 11					
23 P.M.	-62 07	136 08	R.	-11 05	N.w. by w. $\frac{1}{2}$ w.	-83 30	+11 27	+ 0 22	- 0 27				
	-62 07	136 08	R.	-14 02	w. $\frac{1}{4}$ s.		+13 32	- 0 30					
	-62 06	136 07	R.	-11 00	s.w. by w.		+11 39	+ 0 39					
	-62 06	136 07	O.	-14 49	w. by N.		+13 07	- 1 42					
25 A.M.	-62 06	136 07	S.	-10 59	N.w. by w.	-83 10	+10 42	- 0 17	+ 8 09				
	-62 06	136 06	T.	-12 41	N.w. by w. $\frac{1}{2}$ w.		+11 27	- 1 14					
	-60 30	131 47	S.	+ 0 15	N.W.		+ 8 40	+ 8 55					
	-60 30	131 47	O.	+ 1 13	N.W.		+ 8 40	+ 9 53					
	-60 30	131 47	Y.	+ 0 16	N.W.		+ 8 40	+ 8 56					
	-60 30	131 47	W.	+ 0 50	N.W.		+ 8 40	+ 9 31					
	-60 30	131 47	T.	- 0 35	N.W.		+ 8 40	+ 8 05					
	-60 23	131 28	R.	- 1 51	N.W. $\frac{1}{2}$ w.		+ 9 24	+ 7 33					
	-60 23	131 28	R.	- 5 51	w.		+12 53	+ 7 02					
	-60 23	131 28	T.	- 3 10	N.W.		+ 8 40	+ 5 30					
	-60 23	131 28	W.	- 1 51	N.W.		+ 8 40	+ 6 49					
	25 P.M.	-60 22	131 27	R.	+ 0 33		N.W.	-83 00		+ 8 40	+ 9 13	+ 7 38	
-60 20		131 22	R.	+ 1 00	N.W. by N.	+ 6 44	+ 7 44						
-60 20		131 22	T.	+18 20	E.N.E.	-11 17	+ 7 03						
-60 20		131 22	T.	+18 12	E. $\frac{1}{2}$ s.	-12 31	+ 5 41						
-60 20		131 22	R.	+14 06	N.E. by N.	- 6 44	+ 7 22						
-60 20		131 21	R.	+18 59	N.E. by E. $\frac{3}{4}$ E.	-10 57	+ 8 02						
-60 20		131 21	Sm.	+19 01	E.N.E.	-11 17	+ 7 44						
-60 20		131 21	R.	+22 22	E.	-12 33	+ 9 49						
-60 20		131 21	Sm.	+17 35	N.E. by E.	- 9 59	+ 7 36						
-60 20		131 21	T.	+18 36	E.N.E.	-11 17	+ 7 19						
-60 20		131 21	S.	+18 17	N.E. by E.	- 9 59	+ 8 18						
26 A.M.		-60 20	131 21	W.	+20 05	E. $\frac{1}{2}$ N.	-83 00		-12 20	+ 7 45	+ 8 18		
	-60 20	131 21	R.	+18 49	N.E. by E. $\frac{1}{2}$ E.	-10 37		+ 8 12					
	-60 20	131 21	R.	+16 36	N.E.	- 8 26		+ 8 10					
	-60 19	131 21	R.	+ 3 47	N.W. by N.	+ 6 44		+10 31					
	-60 19	131 21	R.	+ 8 33	N.	0 00		+ 8 33					
	-59 25	130 14	R.	+ 3 21	N.W. by N.	+ 6 12		+ 9 33					
	26 P.M.	-59 13	130 02	R.	+ 7 01	N.		-82 36	0 00	+ 7 01		+ 8 32	
		-59 13	130 02	S.	+ 4 42	N.N.W.			+ 4 10	+ 8 52			
		-59 11	130 00	R.	+ 1 49	N.N.W.			+ 4 10	+ 5 59			
		-59 10	129 56	R.	+ 2 32	N.N.W.			+ 4 10	+ 6 42			
		-59 10	129 56	O.	+ 1 48	N.N.W.			+ 4 10	+ 5 58			
		-59 10	129 56	W.	+ 2 48	N.N.W.			+ 4 10	+ 6 58			
-59 03		129 40	S.	+ 4 59	N.N.W.	+ 4 10	+ 9 09						
-58 08		128 46	R.	+ 8 55	N.N.W.	+ 3 54	+12 49						
27 A.M.	-58 08	128 46	S.	+ 5 44	N.N.W.	-82 00	+ 3 54	+ 9 38	+ 8 47				
	-58 06	128 43	S.	+ 6 53	N.N.W.		+ 3 54	+10 47					
	28 A.M.	-57 24	127 50	W.	- 2 21		w. $\frac{1}{2}$ s.	+10 41		+ 8 20			
		-57 24	127 50	O.	+ 0 05		w. $\frac{1}{2}$ s.	+10 41		+10 46			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.	
	Lat.	Long.									
Mar. 28 A.M.	-57 19	127 49	R.	- 1 35	w. by s.	+81 45	+10 40	+ 9 05	+ 8 47	Very much motion; observations uncertain to two or three degrees.	
	-57 19	127 49	T.	- 2 16	w. 1/2 s.		+10 41	+ 8 25			
	-57 20	127 47	R.	- 2 56	w.		+10 41	+ 7 45			
	-57 20	127 47	W.	- 1 20	w. 1/2 N.		+10 29	+ 9 09			
	-57 20	127 47	T.	- 3 05	w. by s. 1/4 s.		+10 48	+ 7 43			
	-57 21	127 42	R.	- 2 05	w. 1/2 N.		+10 29	+ 8 24			
	-57 21	127 42	S.	- 3 34	w. 1/2 N.		+10 29	+ 6 55			
	-57 22	127 37	R.	+ 0 39	w.		+10 41	+11 20			
	29 P.M.	-56 21	130 30	S.	+ 9 40		N.E.	- 6 27			+ 3 13
		-56 21	130 42	R.	+13 12		N.E.	- 6 27			+ 6 45
		-56 21	130 42	S.	+ 9 04		N.E.	- 6 27			+ 2 37
		-56 16	130 46	R.	+13 24		N.E.	- 6 27			+ 6 37
-56 14		130 50	R.	+11 27	N.E.	- 6 27	+ 5 00				
-56 05		130 42	T.	+14 07	N.E.	- 6 27	+ 7 40				
30 A.M.	-56 05	130 42	W.	+13 50	N.E. by N.	- 5 01	+ 8 49				
	-56 08	130 55	R.	+11 38	N.E.	- 6 27	+ 5 11				
	-55 20	131 39	SM.	+ 8 57	N.E. 1/2 E.	- 6 33	+ 2 24				
	-55 00	131 43	T.	+ 6 27	N.E. by N.	- 4 38	+ 1 49				
	-55 00	131 43	SM.	+ 5 43	N.E. by N.	- 4 38	+ 1 05				
	-55 00	131 43	S.	+ 6 27	N.E. by E.	- 7 06	- 0 39				
	-55 16	131 09	R.	+ 8 05	N.E. by E.	- 7 06	+ 0 59				
	-55 16	131 09	R.	+11 55	E.	- 8 59	+ 2 56				
	-55 14	131 12	R.	+ 8 55	N.E. 1/2 E.	- 6 33	+ 2 22				
	-55 14	131 12	T.	+ 6 27	N.E. 1/2 N.	- 5 17	+ 1 10				
	-55 14	131 12	S.	+ 4 16	N.E. by N.	- 4 38	- 0 22				
	-55 14	131 12	O.	+ 4 28	N.E. 1/2 N.	- 5 17	- 0 49				
30 P.M.	-55 14	131 18	Y.	+ 6 00	N.E. 1/2 E.	- 6 33	- 0 33				
	-55 14	131 18	W.	+ 5 28	N.E. by N.	- 4 38	+ 0 50				
	-55 11	131 15	R.	+ 6 33	N.E. by N.	- 4 38	+ 1 55				
	-55 11	131 15	T.	+ 6 04	N.E. by N.	- 4 38	+ 1 26				
	-55 05	132 48	W.	+ 3 18	N.E. 1/2 N.	- 5 05	- 1 47				
	-55 05	132 48	T.	+ 4 16	N.N.E.	- 3 00	+ 1 16				
	-55 05	132 48	S.	- 2 50	N.	0 00	- 2 50				
	-55 05	132 48	T.	+ 7 07	N.E. by N.	- 4 27	+ 2 40				
	-55 07	132 37	R.	+ 8 14	N.E. by N.	- 4 27	+ 3 47				
	-55 04	132 40	R.	+ 5 57	N.E. by N.	- 4 27	+ 1 30				
	-55 04	132 40	Y.	+ 8 43	N.E. by N.	- 4 27	+ 4 16				
	-55 02	132 42	R.	+ 4 56	N.E. by N.	- 4 27	+ 0 29				
31 A.M.	-55 02	132 42	T.	+ 4 55	N.E. by N.	- 4 27	+ 0 28				
	-54 07	134 31	S.	+ 4 23	N.E. by E.	- 6 29	- 2 06				
	-54 07	134 21	T.	+ 5 06	E.N.E.	- 7 26	- 2 14				
	-54 07	134 21	O.	+ 5 52	N.E. by E.	- 6 29	- 0 37				
	-54 01	134 35	T.	+ 5 57	E. by N.	- 7 57	- 2 00				
	-54 01	134 35	S.	+ 6 33	E. 1/2 S.	- 8 16	- 1 43				
	-54 01	134 35	S.	+ 5 15	E. by N. 1/2 N.	- 7 38	- 2 23				
	-54 04	134 35	O.	+ 3 27	E.N.E.	- 7 26	- 3 53				
	-54 04	134 40	W.	+ 6 32	E.N.E.	- 7 26	- 0 48				
	-54 05	134 40	W.	+ 5 26	E. by N.	- 7 57	- 2 31				
	-54 04	134 43	R.	+ 6 25	E. by N. 1/2 N.	- 7 38	- 1 13				
	-54 04	134 47	R.	+ 6 30	E. by N. 1/2 N.	- 7 38	- 1 08				
April 1 P.M.	-54 04	134 54	R.	+ 6 35	E. 1/2 N.	- 8 06	- 1 31				
	-54 04	134 54	R.	+ 7 04	E. 1/2 N.	- 8 06	- 1 02				
	-52 56	135 23	R.	+ 0 52	N.N.E.	- 2 42	- 1 50				
	-52 55	135 24	R.	+ 1 49	N.N.E.	- 2 42	- 0 53				

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Mean Declination.	Remarks.	
	Lat.	Long.									
April 1 P.M.	52	135	S.	+ 1 34	N.N.E.	-78 50	- 2 42	- 1 08	- 1 03		
	52	135	T.	+ 0 30	N.N.E.		- 2 42	- 2 12			
	52	135	T.	+ 3 13	N.N.E.		- 2 42	+ 0 31			
	52	135	R.	+ 2 24	N.N.E.		- 2 42	- 0 18			
	52	135	R.	+ 1 10	N.N.E.		- 2 42	- 1 32			
	2 A.M.	51	136	T.	- 1 37	N.E. by N.	-77 40	- 3 30		- 5 07	
		51	136	R.	- 1 00	N.N.E.		- 2 28		- 3 28	
		51	136	S.	- 5 26	N.		0 00		- 5 26	- 4 39
		51	136	T.	- 7 08	N. by W.		+ 1 12		- 5 56	
	2 P.M.	51	136	R.	- 0 49	N.N.E.	- 2 28	- 3 17			
5 P.M.	44	143	S.	- 0 06	N.E. by E.	-73 20	- 3 51	- 3 57			
	44	143	R.	- 1 11	N.E. by E.		- 3 51	- 5 02			
	44	143	R.	- 5 41	S.E. by S.		- 3 17	- 8 58			
6 A.M.	44	145	T.	- 6 33	E.	-71 40	- 4 38	-11 11			
	44	145	R.	- 5 35	N.E. by E. 1/2 E.		- 3 42	- 9 17	- 8 46		
	44	145	R.	- 7 01	N.E. by E.		- 3 26	-10 27			
	44	145	T.	- 7 19	N.E. by E.		- 3 26	-10 45			
	44	145	T.	- 6 50	N.E. by E.		- 3 26	-10 16			
6 P.M.	43	146	R.	- 5 58	N.E. 1/2 E.	- 3 08	- 9 06				

Observations of the INCLINATION in H.M.S. Erebus, from September 1840 to April 1841, made with Needle R. F. 4.

Observers Captain Ross and Lieutenant SMITH, R.N.

1840.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean In- clination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
			h m		° '		'	° '	° '	
Sept. 17.	Magnetic Observa- tory, Van Diemen Island.		2 P.M.	Direct.	-71 06.8	Observed } on shore. }	.....	-71 06	-70 38	
	-42 52	147 24		S. at 20°.	-71 13.4					
				N. at 20°.	-71 12.1					
				S.	-71 15.1					
19.			11 A.M.	Direct.	-71 02.8					
28.			2 P.M.	Direct.	-71 05.7					
			3 P.M.	Direct.	-70 58.4					
29.			1 P.M.	Direct.	-71 05.2					
			to	S. at 20°.	-71 09.9					
				S. at 20°.	-71 07.2					
				N. at 20°.	-70 58.5					
Oct. 17.	At anchor.		3 P.M.	Direct.	-71 02.6	S.E. by S.	-43	-71 24	-70 45	
			1 30 P.M.	Direct.	-70 39.1					
				S.	-70 42.8	W.	+24	-71 24		
				Direct.	-71 46.7					
			2 P.M.	Direct.	-70 29.9	S. by E.	-61	-71 33		
				S.	-70 33.4					
				Direct.	-70 35.6	S.S.E.	-53	-71 33		
				S.	-70 44.1					
21.			2 30 P.M.	Direct.	-71 00.5	S.E.	-32	-71 27		
				S.	-70 49.6					
			1 45 P.M.	Direct.	-72 06.7	W.N.W.	+46	-71 24		
				Direct.	-72 12.6					
29.			6 A.M.	Direct.	-72 20.9	N.	+74	-71 06		
				S.	-72 18.7					
				Direct.	-72 12.5	N.N.E.	+70	-71 00		
				S.	-72 07.8					
				Direct.	-72 10.3	N.E.	+64	-70 58		
				S.	-71 54.8					
				Direct.	-72 01.6	E.N.E.	+46	-71 15		
				S.	-71 59.6					
				Direct.	-71 22.5	E.	+24	-71 02		
				S.	-71 30.0					
				Direct.	-72 17.0	N.N.W.	+71	-71 12		
				S.	-72 29.4					
				Direct.	-72 37.8	N.W.	+64	-71 27		
				S.	-72 24.3					
				Direct.	-71 21.0	W.S.W.	- 3	-71 26		
				S.	-71 24.5					
				Direct.	-71 38.0	W.	+24	-71 17		
				S.	-71 44.7					
				Direct.	-71 57.7	W.N.W.	+46	-71 00		
				S.	-71 34.9					
				Direct.	-70 52.0	S.W.	-32	-71 20		
				S.	-70 43.7					
				Direct.	-70 38.5	S.S.W.	-52	-71 27		
				S.	-70 32.3					
				Direct.	-70 16.9	S.	-61	-71 18		
				S.	-70 17.0					
				Direct.	-70 16.7	S.S.E.	-53	-71 09		
				S.	-70 16.2					

Observations of Inclination. (Continued.)

1840.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean In- clination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
Oct. 29.	At anchor.		6 A.M.	Direct.	-70 46.5	S.E.	-31	-71 17	-70 45	
				S.	-70 44.6					
				Direct.	-71 12.8					
Nov. 13.	-44 16 149 29		1 15 P.M. to 2 15 P.M.	Direct.	-71 03.1	E.S.E.	-3	-71 09	-70 41	
				S.	-71 05.8					
				N.	-71 10.6					
14.	-45 13 151 57		10 40 A.M. to 11 25 A.M.	Direct.	-71 42.7	S.E.	-33	-72 17	-71 49	
				S.	-71 47.0					
				N.	-71 43.5					
15.	-45 33 152 45		11 20 A.M. to Noon.	Direct.	-72 26.0	E.	+23	-72 05	-71 37	
				S.	-72 18.3					
				N.	-72 39.0					
16.	-46 18 154 30		1 30 P.M. to 2 20 P.M.	Direct.	-72 22.5	E.S.E.	-5	-72 32	-72 04	
				S.	-72 21.2					
				N.	-72 37.1					
17.	-47 46 157 40		10 45 A.M. to 11 45 A.M.	Direct.	-73 20.2	S.E. by E. 1/2 E.	-14	-73 42	-73 14	
				S.	-73 24.7					
				N.	-73 37.7					
18.	-49 20 160 13		11 15 A.M. to Noon.	Direct.	-74 22.7	S.E. by E. 1/2 E.	-15	-74 43	-74 15	
				S.	-74 41.0					
				N.	-74 21.8					
19.	-50 28 164 9		11 20 A.M. to Noon.	Direct.	-75 16.8	E.	+22	-74 51	-74 23	
				S.	-75 12.5					
				N.	-75 11.0					
21.	Auckland Island. -50 33 166 19		1 15 P.M. to 4 P.M.	Direct.	-74 25.5	W.N.W.	+47	-73 49	-73 21	
				S.	-74 19.5					
				N.	-75 02.5					
24.			11 30 A.M. to 0 30 P.M.	Direct.	-75 05.1	(Record omitted.)				
				S.	-75 03.6					
				N.	-74 49.6					
At the Magne- tic Observa- tory.			2 00 P.M. to 5 30 P.M.	Direct.	-73 40.8	Observed } on shore.		-73 41.3	-73 13.3	Mean of needles whose poles were inverted -73 10.
				S.	-73 39.8					
				N.	-73 43.3					
26. Pig Island.	-50 32 166 12		9 00 A.M. to 10 00 A.M.	Direct.	-73 38.4	Observed } on shore.		-73 36.3	-73 08.3	
				S.	-73 33.3					
				N.	-73 34.4					
Shoe Island.			1 30 P.M. to 2 30 P.M.	Direct.	-77 27.5	Observed } on shore.		-77 31	-77 03	Excessive local at- traction.
				S.	-77 33.1					
				N.	-77 31.3					
200 yards west of the prece- ding station.				Direct.	-74 10.6	Observed } on shore.		-74 11	-73 43	

Observations of Inclination. (Continued.)

1840.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc-tion for ship's attrac-tion.	Mean In-clination. Face east.	True Inclination.	Remarks.																															
	Lat.	Long.																																							
Nov. 26.	At anchor.		h m 6 00 to	Direct.	-72 42.8	} s.s.w.	-58	-73 43	-73 15	} Excessive local attraction.																															
			6 40 P.M.	S.	-72 48.0																																				
			6 45 P.M.	Direct.	-73 40.4	} w.s.w.	-6	-73 43	-73 15																																
	S.	-73 34.7																																							
30.	Auckland Island, Ocean Point.		7 45 A.M.	Direct.	-73 29.1	} Observed on shore.	} .....	-73 28	-73 00																																
				S.	-73 26.0																																				
			2 00 P.M.	Direct.	-73 58.2																																				
	Sandy Bay.		2 30 P.M.	Direct.	-73 50.4									-73 26																											
				S.	-73 56.6																																				
				N.	-73 53.2																																				
Dec. 2.	Auckland Island.		1 20 P.M.	Direct.	-65 39.5								-65 02																												
			to	S.	-65 28.0																																				
			2 30 P.M.	N.	-65 13.0																																				
				Direct.	-65 38.0																																				
6.	At anchor.		7 15 A.M.	Direct.	-73 03.4	} s.w.	-37	-73 41	-73 13																																
				S.	-73 04.7																																				
			8 30 A.M.	Direct.	-72 46.5	} s.s.w.	-59	-73 44	-73 16.																																
				S.	-72 44.6																																				
7.			11 00 A.M.	Direct.	-74 12.2	} w. by s.	+ 8	-74 05	-73 37																																
				S.	-74 13.6																																				
8			9 00 A.M.	Direct.	-72 30.5	} s.	-67	-73 35	-73 07																																
					S.					-72 25.1																															
				Direct.	-72 33.0	} s.s.e.	-59	-73 32	-73 04																																
					S.					-72 32.5																															
				Direct.	-73 10.2	} s.e.	-37	-73 43	-73 15																																
					S.					-73 01.8																															
				Direct.	-73 27.5	} e.s.e.	-7	-73 37	-73 09																																
					S.					-73 33.0																															
				Direct.	-73 58.0	} e.	+22	-73 32	-73 04																																
					S.					-73 49.8																															
				Direct.	-74 10.6	} e.n.e.	+47	-73 25	-72 57																																
					S.					-74 12.8																															
				Direct.	-74 39.0	} n.e.	+66	-73 35	-73 07																																
					S.					-74 42.5																															
				Direct.	-74 33.2	} n.n.e.	+76	-73 21	-72 53																																
					S.					-74 41.1																															
				Direct.	-74 51.0	} n.	+79	-73 33	-73 05																																
					S.					-74 53.3																															
				Direct.	-75 01.5	} n.n.w.	+76	-73 46	-73 18																																
					S.					-75 02.3																															
				Direct.	-74 48.5	} n.w.	+66	-73 38	-73 10																																
					S.					-74 39.2																															
				Direct.	-73 10.7	} s.e.	-37	-73 48	-73 20																																
12.				Direct.	-73 55.8	} e. by n.	+36	-73 20	-72 52																																
				Direct.	-73 37.4					} e.	+22	-73 15	-72 47																												
				Direct.	-74 30.0									} n.e.	+66	-73 24	-72 56																								
				Direct.	-74 09.4													} n.e. by e.	+59	-73 10	-72 42																				
				Direct.	-74 04.9																	} e.n.e.	+47	-73 18	-72 50																
				Direct.	-73 24.3																					} e. by s.	+7	-73 17	-72 49												
				Direct.	-73 21.3																									} e.s.e.	-7	-73 28	-73 00								
				Direct.	-73 02.2																													} s.e. by e.	-22	-73 24	-72 56				



Observations of Inclination. (Continued.)

1840.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.		
	Lat.	Long.										
Dec. 14.	Campbell Island. -52 34 169 10 At anchor.		h m									
			10 00 A.M.	Direct.	-75 42.8	} N.W.	+67	-74 38	-74 10			
				S.	-75 48.3							
			11 00 A.M.	Direct.	-74 53.7	} W.	+22	-74 36	-74 08			
				S.	-75 02.4							
			1 00 P.M.	Direct.	-73 18.4	} S.S.W.	-60	-74 16	-73 48			
				S.	-73 13.1							
			2 00 P.M.	Direct.	-73 44.5	} Observed } on shore.	.....	-74 18	-73 50			
			to	S.	-74 29.7							
			4 15 P.M.	N.	-74 27.8							
15.	At the Magnetic Observatory.		6 15 A.M.	Direct.	-74 30.2	} Observed } on shore.	.....	-74 23	-73 55			
			to	S.	-74 24.5							
			8 30 A.M.	N.	-74 24.4							
			Direct.	-74 18.5								
			Direct.	-74 23.1								
16.	At Anchor.		1 00 P.M.	Direct.	-73 18.4	} S.S.W.	-60	-74 16	-73 48			
				S.	-73 13.1							
17.	Running out of Harbour.		9 30 A.M.	Direct.	-73 42.1	} E. by S.	+7	-73 35	-73 07			
				Direct.	-73 16.0					S.	-69	-74 25
18.	-53 47 169 02 -54 25 169 16		4 30 A.M.	Direct.	-74 21.0	} S.S.E.	-61	-75 28	-74 46			
				S.	-74 33.8							
			5 00 P.M.	Direct.	-73 39.9	} S.S.E. 1/2 E.	-57	-75 00				
	N.	-74 27.0										
19.	-55 50 170 6		10 15 A.M.	Direct.	-75 26.1	} S. by W.	-71	-76 44	-76 16			
			to	N.	-75 40.5							
			11 10 A.M.	S.	-75 32.5							
21.	-57 15 170 40 -57 54 170 25		4 20 A.M.	Direct.	-77 14.0	} S.S.E.	-67	-78 11	-77 43			
				N.	-77 01.2							
				N.S.	-76 58.0							
			5 10 P.M.	Direct.	-77 15.0	} S. by E.	-74	-78 19	-77 51			
to	N.	-77 00.5										
5 50 P.M.	N.S.	-77 00.1										
22.	-58 57 170 57		10 15 A.M.	Direct.	-77 24.2	} S.	-77	-78 32	-78 04			
			to	S.	-77 19.0							
			11 10 A.M.	N.	-77 10.8							
				N.S.	-77 05.2							
23.	-59 41 169 38 -59 48 169 42		10 15 A.M.	Direct.	-78 05.0	} S.S.W.	-69	-79 14	-78 34			
			to	S.	-78 08.5							
			11 20 A.M.	N.	-78 06.7							
				N.S.	-77 59.0							
			6 40 P.M.	Direct.	-78 57.8					} E.	+20	-78 38
				N.S.	-78 59.0							
24.	-60 14 170 15 -60 31 170 32		5 00 A.M.	Direct.	-78 27.3	} S.E. 1/2 S.	-52	-79 19	-78 53			
			to	N.	-78 13.4							
			6 00 A.M.	N.S.	-78 24.0							
			11 00 A.M.	Direct.	-78 05.5							
			to	S.	-78 47.2							
			Noon.	N.	-78 13.6					} S.S.E.	-70	-79 57
				N.S.	-78 01.0							

Mean on shore -73 52.5.  
Mean on board -73 50.

Uncertain.  
Very much motion.

Ship pitching.

Observations of Inclination. (Continued.)

1840.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean Incli- nation. Face east.	True Inclination.	Remarks.	
	Lat.	Long.									
Dec. 24.	-60 46	170 44	5 15 P.M.	Direct.	-78 40.4	s.e. by s.	-59	-79 34	-79 06		
			to	S.	-78 37.5						
6 10 P.M.	N.	-78 45.8									
	N.S.	-78 16.3									
25.	-61 34	170 40	2 15 A.M.	Direct.	-78 43.4	s.	-79	-79 58	-79 30		
			to	N.	-78 40.1						
			3 15 A.M.	N.S.	-78 32.9						
26.	-62 04	172 48	Noon.	Direct.	-81 29.2	N.	+88	-80 01	-79 41		
				?	-81 25.0						
	?	-81 27.2									
	-62 10	173 00	7 P.M.	Direct.	-79 28.3	s.s.w.	-71	-80 39			
27.	-62 40	173 40	10 30 A.M.	Direct.	-80 53.3	w. 1/2 N.	+27	-80 26	-79 58		
28.	-62 40	174 40	10 30 A.M.	Direct.	-79 26.4	s.	-80	-80 37	-80 09		
			to	S.	-79 21.4						
	11 45 A.M.	N.	-79 18.4								
		N.S.	-78 32.7								
	-62 52	174 28	3 00 P.M.	Direct.	-79 37.2						
				N.S.	-79 22.8						
29.	-64 00	172 44	8 40 A.M.	Direct.	-80 25.0	s.s.w. 1/2 w.	-67	-81 31	-81 03		
			to	S.	-80 24.1						
	10 20 A.M.	N.	-80 28.2								
		N.S.	-80 18.8								
	-64 06	172 38	10 30 A.M.	Direct.	-80 28.1	s.s.w.	-73	-81 41	-81 03		
			to	S.	-80 16.8						
			11 45 A.M.	N.	-80 20.5	s. by w.	-80	-81 08			
				N.S.	-79 47.8						
				Direct.	-80 17.3			-81 37			
30.	-64 30	172 51	6 45 A.M.	Direct.	-80 23.9	s.w. by s.	-61	-81 25	-81 11		
				N.S.	-80 16.2						
	-64 31	173 00	10 45 A.M.	Direct.	-80 16.3	s.	-82	-81 38	-81 11		
			to	S.	-80 14.4						
			11 45 A.M.	N.	-80 17.9						
				N.S.	-80 54.3						
31.	-65 58	171 47	10 45 A.M.	Direct.	-81 23.8	s.	-84	-82 48	-82 20		
			to	S.	-81 25.6						
	11 50 A.M.	N.	-81 29.3								
		N.S.	-81 18.2								
	-66 17	170 57	3 45 P.M.	Direct.	-81 25.0	s. by w. 1/2 w.	-77	-82 42	-82 25		
			to	S.	-81 23.9						
			4 40 P.M.	N.	-81 34.7						
				N.S.	-81 49.4						
1841.	Jan. 1.	-66 30	169 13	10 00 A.M.	Direct.	-81 36.4	s.	-85	-83 08	-82 40	
					S.	-81 39.0					
					N.	-81 49.6					
					N.S.	-81 49.2					

Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc-tion for ship's attrac-tion.	Mean Inclination. Face east.	True Inclination.	Remarks.			
	Lat.	Long.											
Jan. 1.	-66 32	169 45	h m	Direct.	-84 14.6	N.	+91	-82 59	-82 31*				
			11 25 A.M.		S.						-84 31.7		
			to		N.						-84 41.1		
			0 30 P.M.		N.S.						-84 32.9		
2.	-66 23	170 12	10 40 A.M.	Direct.	-84 16.3	N.N.W. 1/2 W.	+82	-83 21	-82 53				
			to	S.	-85 01.6								
			11 45 A.M.	N.	-85 05.6								
				N.S.	-84 29.6								
3.	-65 39	170 44	11 00 A.M.	Direct.	-83 28.7	N.N.W.	+86	-82 19	-81 51	Much motion.			
			to	S.	-83 46.0								
			Noon.	N.	-83 58.0								
				N.S.	-83 46.5								
4.	-65 22	172 40	10 15 A.M.	Direct.	-82 18.3	E. 1/2 S.	+9	-82 11	-81 43	Much motion.			
			to	S.	-82 06.0								
			11 40 A.M.	N.	-82 19.0								
				N.S.	-82 39.1								
5.	-66 55	174 31	10 30 A.M.	Direct.	-82 03.7	S.E. by E.	-34	-82 38	-82 13	Sailing amongst loose ice.			
				Direct.	-82 19.9						E.S.E.	-16	-82 36
				Direct.	-82 06.1						S.E. 1/2 E.	-42	-82 48
	-67 27	174 51	7 10 P.M.	Direct.	-83 03.6	E.S.E.	-16	-83 26	-82 58	Sailing in the pack.			
			to	S.	-83 11.3								
			7 50 P.M.	N.	-83 09.2								
				N.S.	-83 15.5								
6.	-68 17	175 0	11 00 A.M.	Direct.	-83 40.0	S.E. by S.	-63	-83 26	-83 12	Sailing in the pack.			
				S.	-83 35.0						E.S.E.	-17	-83 57
				Direct.	-82 23.1						E.S.E.	-17	-83 52
				Direct.	-82 35.4						S.E.	-50	-83 25
			Direct.	-82 26.1	S.S.E.	-75	-83 41						
7.	-68 32	175 49	9 30 A.M.	Direct.	-84 04.4	E.	+18	-83 53	-83 28	Standing off and on in a pool of water in the pack. Smooth water.			
			to	S.	-84 10.3								
			10 15 A.M.	N.	-84 19.6								
			to	Direct.	-84 10.8								
			S.	-84 18.1	w.	+18	-83 59						
			N.	-84 22.3									
8.	-68 28	176 31	11 00 A.M.	Direct.	-83 35.2	w. by S. 1/2 S.	-8	-83 43	-83 17	The ice was slightly in motion.			
			to	S.	-83 57.7								
			Noon.	N.	-84 03.5								
				N.S.	-84 03.2								
			Direct.	-83 43.2	w.	+18	-83 45						
			Direct.	-83 43.2									
	On ice.		1 20 P.M.	Direct.	-84 01.2	Observed on ice.	.....	-84 02.9	-83 34.9				
	-68 28	176 32	to	S.	-84 06.8								
			2 00 P.M.	N.	-84 09.3								
			3 00 P.M.	N.S.	-83 55.7								
				Direct.	-84 01.5								

\* The accordance of the results on the 1st of January with the ship's head on the north and south points, is extremely satisfactory with reference to the corrections, which on those points are very large and have opposite signs.

## Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean Inclination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
Jan. 9.	-68° 48'	176° 25'	2 45 A.M.	Direct.	-82° 41.8	s.s.e.	-76	-84 08	-83 40	
			to 4 00 A.M.	S. N. N.S.	-82 41.4 -82 48.6 -82 57.0					
10.	-69 15	176 14	11 40 A.M.	Direct.	-83 09.4	s.	-88	-85 28	-85 00	
			10 35 A.M. to 11 40 A.M.	Direct. S. N. N.S.	-84 01.8 -83 51.4 -84 16.2 -83 52.5					
11.	-71 15	171 15	9 30 A.M.	Direct.	-84 48.4	s.	-89	-86 18	-85 50	
			to 11 00 A.M.	S. N. N.S.	-84 48.5 -84 49.3 -84 49.3					
12.	-71 24	170 44	4 40 P.M.	Direct.	-84 55.4	s. by w.	-86	-86 21	-85 53	
			to 5 50 P.M.	S. N. N.S.	-84 56.9 -84 56.2 -84 51.4					
13.	-71 47	170 52	10 46 A.M.	Direct.	-86 17.8	w.s.w.	-14	-86 38	-86 10	Much motion; observations indifferent.
			to 11 40 A.M.	S. N.	-86 29.5 -86 25.2					
14.	-72 07	172 19	10 15 A.M.	Direct.	-87 14.7	E. by N. ½ N.	+46	-86 41	-86 13	
			to 11 40 A.M.	S. N. N.S.	-87 44.5 -87 32.6 -87 17.6					
15.	-71 51	172 40	9 00 A.M.	Direct.	-87 04.5	E. by N. ½ N. s.s.w.	+46 -79	-86 18 -86 23	-85 53	Much motion.
			-71 54	171 37	11 00 A.M. to Noon.					
16.	-72 12	172 13				9 15 A.M.	Direct.	-85 48.2	s. by w.	-87
			to 11 00 A.M.	S. N. N.S.	-85 40.3 -85 48.5 -85 32.2					
17.	-72 09	173 35	7 30 A.M.	Direct.	-86 53.3	E.	+24	-86 31	-86 03	Much motion.
			to 8 30 A.M.	N. N.S.	-86 50.2 -87 01.0					
18.	-72 57	176 06	11 00 A.M.	Direct.	-86 03.5	s.e. by e.	-33	-86 37 -87 05	-86 11	
			S. N. N.S.	-86 32.2 -86 32.3 -86 04.0	E.S.E.					
19.	-72 35	173 34		10 00 A.M.		Direct.	-86 12.4	E. by s. ½ s.	-4	-86 27
			to 11 00 A.M.	S. N. N.S.	-86 21.8 -86 22.2 -87 07.0	s.w. by w.	-33			

## Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean Inclination. Face east.	True Inclination.	Remarks.				
	Lat.	Long.												
Jan. 19.	-72 31	173 39	h m	Direct.	-85 58.4	s. by E. 1/2 E.	-83	-87 19	-86 51					
			4 30 P.M.		S.						-85 55.5			
			to		N.						-86 04.1			
			5 30 P.M.		N.S.						-85 45.8			
20.	-73 47	171 50	10 00 A.M.	Direct.	-86 56.7	s.E.	-51	-87 48	-87 04					
			to	S.	-86 59.8			-87 51						
			11 15 A.M.	N.	-86 58.4			-87 49						
				N.S.	-86 59.1			-87 50						
	-73 50	171 43	7 00 P.M.	Direct.	-86 49.0	s.w.	-51	-87 40						
			7 30 P.M.	Direct.	-86 04.7	s.w. by w.	-34	-86 39						
			7 50 P.M.	Direct.	-87 45.0	E. by N.	+39	-87 06						
21.	-74 10	170 28	0 30 A.M.	Direct.	-86 39.6	s. by E.	-87	-88 07	-87 12					
			to	S.	-86 37.4			-88 04						
			1 30 A.M.	N.	-86 38.5			-88 06						
				N.S.	-86 30.5			-87 57						
	-74 06	171 20	4 00 A.M.	Direct.	-87 48.1	E.	+24	-87 24						
			-74 00	170 43	10 40 A.M.	Direct.	-88 04.7	N.E. by E.			+66	-86 59		
					11 00 A.M.	Direct.	-88 46.3	N.E. by N.			+85	-87 21		
			11 40 A.M.	Direct.	-88 51.2	N.N.E.	+90	-87 21						
	-73 56	170 51	3 10 P.M.	Direct.	-88 40.4	N. by E.	+91	-87 22			-87 11			
			to	S.	-88 57.1									
4 20 P.M.			N.	-88 57.5										
			N.S.	-88 58.2										
22.	-73 56	172 20	11 25 A.M.	Direct.	-86 26.1	s. by E.	-87	-87 56	.....	Very unsteady.				
			to	S.	-86 32.3									
			0 15 P.M.	N.	-86 34.2									
				N.S.	-86 21.7									
23.	-74 23	175 35	Noon.	Direct.	-86 59.0	E. by s.	+6	-86 53	-87 29					
24.	-74 35	173 01	11 20 A.M.	Direct.	-86 36.8	s. by E.	-87	-87 59						
			to	N.	-86 23.0									
			11 50 A.M.	N.S.	-86 35.2									
	-74 36	173 01	11 20 P.M.	Direct.	-86 49.9	s. 1/2 w.	-88	-88 16						
			to	S.	-86 41.4									
			0 20 A.M.	N.	-86 54.3									
25.	-74 38	170 09		N.S.	-86 39.7	s. 1/2 w.	-88	-88 08	-87 25					
			-74 44	169 43	10 00 A.M.			Direct.			-88 12.4	E.	+24	-87 48
					to			S.			-88 21.0			-87 57
								11 15 A.M.			N.	-88 17.0		-87 53
					N.S.	-88 05.0		-87 41						
	-74 47	168 22	6 P.M.	Direct.	-87 24.7	s. by w. 1/2 w.	-85	-88 50			-88 18			
				Direct.	-87 35.7							s.w. by s.	-68	-88 44
			-74 44	168 23	7 20 P.M.							Direct.	-87 34.0	s.s.w. 1/2 w.
					Direct.				-87 49.2	s.w.		-52	-88 41	
26.	-74 54	169 00	5 45 A.M.	Direct.	-87 34.7	s. 1/2 E.	-89	-89 04	-88 21					
			7 45 A.M.	Direct.	-87 46.4			s.w. by s.			-68	-88 54		
			-74 58	169 02	8 20 A.M.			Direct.			-88 37.3	E. by s.	+7	-88 30
27.	-75 22	168 48	2 20 A.M.	Direct.	-87 45.2	s.s.E.	-84	-89 04	-88 36					
			to	S.	-87 45.2									
			4 10 A.M.	N.	-87 45.6									
				N.S.	-87 23.3									

Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc-tion for ship's attrac-tion.	Mean Inclination. Face east.	True Inclination.	Remarks.					
	Lat.	Long.													
Jan. 27.	-76 06	168 11	h m	Direct.	-88 05.4	}	/	o /	o / /						
			4 20 P.M.		S.						-88 06.1	S.E.	-52	-88 55	-88 27
			to		N.						-88 02.2				
			5 20 P.M.	N.S.	-87 59.0										
28.	-76 46	169 22	11 15 A.M.	Direct.	-88 39.6	}	-12	-88 52	-88 00						
			7 00 P.M.	Direct.	-89 32.4						E.S.E.	+85	-88 05		
29.	-77 29	170 30	6 00 A.M.	Direct.	-88 44.7	}	+91	-87 16	-86 48						
					S.						-88 54.6	N. by w.			
					N.						-88 50.2				
			N.S.	-88 36.7											
30.	-77 47	180 28	3 10 A.M.	Direct.	-87 51.4	}	+88	-86 23	-85 54						
			Noon.	Direct.	-87 43.9						N.N.W.	+83	-86 21		
31.	-77 35	181 20	9 30 A.M.	Direct.	-87 30.3	}	+83	-86 07	-85 56						
					to						S.	-87 36.4	N.E. by N.		
					11 30 A.M.						N.	-87 26.0			
											N.S.	-88 07.6			
	-77 06	189 06	7 00 P.M.	Direct.	-85 28.8	s. by E. 1/4 E.	-82	-86 45							
	-77 12	190 54						-86 51							
Feb. 1.	-77 04	188 30	10 30 A.M.	Direct.	-85 45.9	}	-51	-86 37	-86 12						
			to	S.	-85 56.7						S.E.				
			11 30 A.M.	N.	-85 52.5			-86 48							
			N.S.	-85 47.4				-86 43							
	-77 11	189 01	7 45 A.M.	Direct.	-86 02.5	s.w. by w.	-33	-86 38							
								-86 36							
2.	-77 9	188 15	5 10 P.M.	Direct.	-85 59.2	}	-66	-86 51	-86 23						
			to	N.	-85 52.4						S.E. by s.				
			8 15 P.M.	N.S.	-85 36.3										
				Direct.	-85 30.9										
3.	-77 45	187 00	11 35 A.M.	Direct.	-86 27.2	}	+23	-86 04	-86 10						
			to	Direct.	-85 46.9						S.E.				
			Noon.	Direct.	-85 37.5							S.E. by s.			
				Direct.	-85 43.0										
	-77 56	186 35	10 P.M.	Direct.	-85 34.4	s.w. by s.	-66	-86 49							
			10 30 P.M.	Direct.		s. by w. 1/2 w.	-83	-86 57							
3.	-77 17	185 26	10 00 A.M.	Direct.	-86 57.4	}	-14	-87 17	-86 49						
			to	S.	-87 02.3						W.S.W.				
			11 15 A.M.	N.	-87 04.4										
			N.S.	-87 07.0											
4.	-77 00	192 18	9 30 A.M.	Direct.	-86 52.8	}	+53	-86 00	-85 36						
					Direct.						-86 43.5	E.N.E.			
					S.						-86 30.3		E. by N.		
					N.						-86 35.3				
											?	-85 03.8	s. by E.	-86	-86 30
	-77 06	192 34	2 00 P.M.	Direct.	-86 29.5	}	+52	-85 54	-85 26						
			to	Direct.	-86 50.6										
	-77 08	192 19	4 00 P.M.	S.	-86 49.0										
			N.	-86 54.0											
5.	-77 24	192 56	3 00 A.M.	Direct.	-86 27.2	}	+23	-86 13	-85 45						
					to						S.	-86 36.0	E.		
					4 00 A.M.						N.	-86 34.7			
											N.S.	-86 46.5			

Much motion.

Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
Feb. 5.	-77 10	192 48	h m							
			11 45 A.M.	Direct.	-85 00.4	s.	-89	-86 34	-86 06	
			2 30 P.M.	Direct.	-84 57.2					
			to	S.	-84 53.1					
4 00 P.M.	N.	-85 26.3								
				N.S.	-85 09.9					
6.	-77 9	188 50	9 00 A.M.	Direct.	-86 52.2	E.N.E.	+53	-85 59	-85 54	
			to	S.	-87 03.0					
			10 45 A.M.	N.	-87 14.4					
				N.S.	-87 29.8					
			10 55 A.M.	Direct.	-85 03.5	s.	-89	-86 33		
				Direct.	-85 12.1	S.S.W.	-79	-86 31		
7.	-76 58	186 40	6 00 A.M.	Direct.	-85 27.6	s. by w.	-86	-86 54	-86 23	
			to	S.	-85 38.6					
			7 15 A.M.	N.	-85 35.8					
				N.S.	-85 29.3					
			11 30 A.M.	Direct.	-86 05.1	E.S.E.	-14	-86 19		
8.	-77 40	187 05	11 40 A.M.	Direct.	-87 02.5	E.N.E.	+53	-86 10	-85 51	
			1 30 P.M.	Direct.	-87 10.6					
			to	S.	-87 04.5					
			3 45 P.M.	N.	-87 29.6					
				N.S.	-87 35.1	N.E. by E. 1/2 E.	+59	-86 31		
								-86 36		
9.	-77 54	190 10	10 35 A.M.	Direct.	-87 16.3	N.E.	+75	-86 01	-85 49	
			0 20 P.M.	Direct.	-85 27.9	S.E. by S.	-66	-86 34		
10.	-77 39	187 06	5 45 A.M.	Direct.	-85 15.1	s. by E.	-86	-86 41	-86 19	
			to	S.	-85 26.8					
			8 00 A.M.	N.	-85 34.4					
				N.S.	-85 24.6					
			11 40 A.M.	Direct.	-86 33.7	w. by s.	+ 5	-86 29		
11.	-76 55	188 40	2 50 A.M.	Direct.	-87 16.6	N.W.	+75	-86 02	-86 07	
			11 40 A.M.	Direct.	-85 55.0					
			1 00 P.M.	Direct.	-85 29.3					
				S.	-85 39.4					
						S.S.W. 1/2 W.	-73	-86 42		
								-86 52		
12.	-76 50	183 26	10 15 A.M.	Direct.	-86 04.0	S.E. by E.	-33	-86 51	-86 23	
			to	N.	-86 39.8					
			11 40 A.M.	N.S.	-86 09.0					
14.	-76 16	174 14	3 A.M.	Direct.	-86 15.5	S.S.W.	-79	-87 43	-87 15	
			11 40 A.M.	Direct.	-86 20.8					
			2 00 P.M.	Direct.	-86 23.3					
				S.	-86 23.6					
				N.	-86 30.7					
				N.S.	-86 30.3					
			11 20 P.M.	Direct.	-86 34.0	s.	-90	-88 04	-87 36	
15.	-76 03	169 30	11 20 A.M.	Direct.	-87 05.3	s.	-91	-88 36	-88 21	
			to	N.	-87 13.5					
			Noon.	N.S.	-87 03.1					
			4 40 P.M.	Direct.	-87 30.1					
			7 10 P.M.	Direct.	-87 35.3					
			9 00 P.M.	Direct.	-87 36.4					
			11 00 P.M.	Direct.	-87 42.0	S.S.E.	-81	-88 57		
								-89 03		

Much motion.

Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.		
	Lat.	Long.										
Feb. 16.	-76 20	165 32	h m	Direct.	-87 42.8	S.S.E.	-81	-89 04	-88 35			
			6 00 A.M.		S.			-87 49.1			-89 10	
			8 00 A.M.		N.S.			-87 37.8			-88 59	
17.	-76 46	165 2	3 20 A.M.	Direct.	-88 33.2	E.S.E.	-13	-88 46	-88 19			
			4 15 A.M.	Direct.	-87 51.2	S.S.W.	-81	-89 12				
	-76 31	165 04	11 45 A.M.	Direct.	-87 05.3	S.	-91	-88 36				
			4 00 P.M.	Direct.	-87 13.3			-88 44				
	-76 26	164 02	5 00 P.M.	Direct.	-89 34.3	N.E. by E. 1/2 E.	+58	-88 36				
18.	-76 05	166 11	11 40 A.M.	Direct.	-89 26.5	W.	+26	-89 00	-87 53			
			8 15 P.M.	Direct.	-88 10.1			-87 44				
19.	-75 03	168 44	11 00 A.M.	Direct.	-87 21.0	S.W.	-52	-88 13	-88 08			
			to	S.	-87 35.0			-88 27				
			Noon.	N.	-87 44.2			-88 36				
				N.S.	-87 15.9		-88 08					
20.	-73 09	171 26	Noon.	Direct.	-87 02.5	S.W.	-51	-87 54	-86 23	Much motion.		
21.	-71 17	170 43	9 00 A.M.	Direct.	-86 01.8	S.W. by W. 1/2 W.	-27	-86 26				
			10 15 A.M.	S.	-86 03.6			-86 28				
				N.	-86 10.7		-86 35					
	-71 04	170 07	10 50 A.M.	Direct.	-86 31.9	W.	+24	-86 08	-85 53			
	-70 52	168 11	6 40 P.M.	Direct.	-86 15.4	W.S.W.	-14	-86 29				
	-70 48	167 52	8 15 P.M.	Direct.	-86 30.4	W. by S.	+5	-86 25				
22.	-70 41	167 20	6 40 A.M.	Direct.	-87 28.0	N.N.E.	+88	-86 19	-85 51	A great deal of motion.		
			to	S.	-87 57.8							
			7 30 A.M.	N.	-87 51.4							
				N.S.	-87 51.3							
23.	-70 27	166 40	5 00 P.M.	Direct.	-87 02.2	E. by N.	+39	-86 23	-86 19			
			11 40 A.M.	Direct.	-87 31.9	N.E. 1/2 E.	+70	-86 22				
24.	-70 14	167 34	10 00 A.M.	Direct.	-85 50.4	S.S.W. 1/2 W.	-73	-87 03	-86 19			
			to	S.	-85 45.8			-86 59				
			11 50 A.M.	N.	-85 42.7			-86 56				
				N.S.	-85 50.0		-87 03					
25.	-70 14	167 16	6 30 A.M.	Direct.	-85 20.7	S.	-89	-86 50	-86 06	Much motion.		
			to	S.	-85 04.7			-86 34				
			8 00 A.M.	N.	-84 49.2			-86 18				
26.	-70 02	167 35	5 00 P.M.	Direct.	-87 25.3	N.W.	+75	-86 10	-85 41			
			11 30 A.M.	Direct.	-85 54.7	W.S.W.	-14	-86 09				
27.	-69 24	167 55	10 30 A.M.	Direct.	-85 13.1	S.E.	-51	-86 04	-85 28			
			to	N.	-85 18.8			-86 10				
			Noon.	N.S.	-85 03.9			-85 55				
				Direct.	-85 34.1			E.S.E.			-14	-85 48
				Direct.	-86 56.0			N.W.			+75	-85 41
28.	-69 40	167 48	6 00 A.M.	Direct.	-85 03.2	S. by E.	-86	-86 29	-85 54			
			to	N.	-85 20.6			-86 47				
			8 00 A.M.	N.S.	-84 47.6			-86 14				
	-69 56	167 36	Noon.	Direct.	-85 14.4	S. by E.	-86	-86 40				
				Direct.	-86 45.6	N.W. by W.	+64	-85 42				



Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean Incli- nation. Face east.	True Inclination.	Remarks.							
	Lat.	Long.															
Mar. 1.	-69 04	167 41	h m 11 30 A.M.	Direct.	-86 51.5	} n.w. by w.  } n.w.	} +64  } +74	-85 48	} -85 26	} Much motion.							
	-69 06	167 42	2 00 P.M.	Direct.	-86 28.5			-85 25									
	-69 08	167 44	2 30 P.M.	N.	-87 40.5			-86 37									
			3 00 P.M.	N.S.	-87 07.0			-86 03									
			3 30 P.M.	Direct.	-86 49.5			-85 36									
2.	-68 28	168 10	9 30 A.M.	Direct.	-86 12.0	} w. by N.  } n.w. by w.	} +38  } +64	-85 34	} -85 07								
			S.	-86 12.1	-85 34												
			N.	-86 10.2	-85 32												
			N.S.	-86 32.4	-85 54												
			11 15 A.M.	Direct.	-86 24.0			-85 20									
3.	-67 52	167 28	6 15 A.M.	Direct.	-85 01.8	} w.	} +21	-84 41	} -84 28								
			S.	-85 19.2	-84 58												
			N.	-85 38.5	-85 17												
			7 45 A.M.	N.S.	-85 32.1			-85 11									
			11 45 A.M.	Direct.	-84 55.5			-84 35									
4.	-66 44	165 45	11 40 A.M.	Direct.	-85 00.5	} N.E.  } N.  } s.s.w. 1/2 w. } s.w. by s. } w.	} +72  } +91  } -69 } -63 } +18	-83 49	} -83 35	} A great deal of motion. Ship rolling deep.							
			10 30 A.M.	Direct.	-85 05.8			-83 35									
			11 10 A.M.	N.	-85 17.2			-83 46									
			11 40 A.M.	N.S.	-85 08.8			-83 38									
			7 00 A.M.	Direct.	-83 38.3			-84 47									
5.	-65 31	167 42	11 40 A.M.	Direct.	-83 28.3	} s.w. by s. } w.	} -63 } +18	-84 31	} -84 16								
			11 40 A.M.	Direct.	-83 28.3			-84 31									
			5 10 P.M.	Direct.	-84 34.0			-84 16									
			7.	-65 53	162 14			10 00 A.M.			Direct.	-85 17.3	} N.W.  } w.s.w.	} +72  } -17	-84 05	} -83 51	
								10 40 A.M.			S.	-85 39.2			-84 27		
11 20 A.M.	Direct.	-84 08.5				-84 25											
8.	-64 41	162 34	10 10 A.M.	Direct.	-84 33.7	} N.E. by N.	} +79	-83 15	} -82 55								
			S.	-84 47.7	-83 29												
			N.	-84 52.0	-83 33												
			N.S.	-84 32.6	-83 14												
			11 15 A.M.	Direct.	-84 26.5			-83 20									
9.	-64 22	164 32	7 30 A.M.	Direct.	-84 04.5	} N.E. 1/2 E. } N.N.E. } N.N.E. } N.W. by w.	} +67 } +86 } +86 } +62	-82 39	} -82 54	} Much motion on the 10th.							
			Direct.	-84 04.5	-82 39												
			Direct.	-85 01.7	-83 36												
			Direct.	-84 55.3	-83 53												
			9 30 A.M.	Direct.	-84 55.3			-83 53									
12.	-63 57	161 11	6 00 A.M.	Direct.	-83 06.5	} s.s.w. 1/2 w.  } s. by w.  } s.w. by w. 1/2 w.	} -69  } -82  } -25	-84 16	} -83 32								
			6 30 A.M.	Direct.	-82 44.3			-84 06									
			to	S.	-82 47.6			-84 10									
			7 45 A.M.	N.	-82 59.7			-84 22									
			N.S.	-82 10.5	-83 33												
13.	-63 28	159 35	11 40 A.M.	Direct.	-83 07.0	} s.w. by w. 1/2 w.	} -25	-83 32	} -83 32	} Much motion.							
			Direct.	-83 07.0	-83 32												
			14.	-62 41	156 59			10 30 A.M.			Direct.	-83 09.0	} w.	} +18	-82 51	} -82 33	
								to			S.	-83 17.0			-82 59		
								11 10 A.M.			N.	-83 28.7			-83 11		
11 20 A.M.	N.S.	-83 14.7	-82 57														
11 20 A.M.	Direct.	-81 52.5	-83 08														
15.	-63 50	156 06	6 45 A.M.	Direct.	-82 38.0	} s. 1/2 w.	} -85	-84 22	} -83 54								
			to	S.	-82 42.3			-84 22									
			7 40 A.M.	N.	-83 08.3			-83 54									
			?	-83 19.5	-83 54												
			?	-83 19.5	-83 54												

Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correction for ship's attraction.	Mean Inclination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
Mar. 16.	-64 11	154 40	h m 11 45 A.M.	Direct.	-83 28.2	s.w. 1/2 s.	-57	-84 25	-84 06	A heavy head swell.
			1 00 to	Direct.	-83 15.0	s.w. by s.	-64	-84 19		
			3 15 P.M.	S.	-83 52.8		-84 57			
	-64 13	154 03		N.	-83 37.0	s.w. by s.	-64	-84 41		
			N.S.	-83 28.3	-84 32					
			Direct.	-83 23.0	-84 27					
17.	-64 20	153 02	10 15 A.M.	Direct.	-83 27.6	s.w. by s.	-64	-84 32	-84 14	
			to	S.	-83 48.1		-84 52			
			11 15 A.M.	N.	-83 40.9		-84 45			
				N.S.	-83 47.2		-84 51			
			Direct.	-83 40.7	s.w.	-50	-84 31			
18.	-63 54	151 56	5 45 A.M.	Direct.	-84 44.0	w. by N.	+37	-84 34	-84 06	
			to	N.	-85 14.5					
			7 00 A.M.	N.S.	-85 35.2					
19.	-64 18	149 09	11 40 A.M.	Direct.	-84 00.5	s.w. by s.	-64	-85 05	-84 48	
			1 40 P.M.	Direct.	-84 09.7		-85 14			
				S.	-84 26.3		-85 30			
	-64 26	148 20	3 00 P.M.	N.	-84 26.1	s.w. by s.	-64	-85 30	-85 03	
			N.S.	-84 49.0	-85 53					
			Direct.	-84 05.0	-85 09					
	-64 56	147 14	6 15 P.M.	Direct.	-84 15.0	s.s.w.	-76	-85 31		
20.	-65 15	144 53	7 40 A.M.	Direct.	-84 55.7	s.w.	-51	-85 47	-85 05	
			8 50 A.M.	Direct.	-85 25.8	w.s.w.	-15	-85 41		
			10 00 A.M.	Direct.	-86 03.5	w.N.W.	+52	-85 12		
	-65 12	144 07	10 30 A.M.	Direct.	-84 54.3	s.w.	-51	-85 45	-85 10	
			11 20 A.M.	Direct.	-85 08.0	s.w. by w.	-33	-85 41		
			11 40 A.M.	Direct.	-85 12.8	w.s.w.	-15	-85 28		
	-65 10	143 21	11 50 A.M.	S.	-85 45.0	w.s.w.	-15	-86 00	-85 16	
			to	N.	-85 48.3		-86 03			
			1 00 P.M.	N.S.	-85 56.7		-86 12			
	-65 06	142 40	4 45 P.M.	Direct.	-85 55.0	w.	+21	-85 34		
			6 20 P.M.	Direct.	-85 46.5	w.	+21	-85 26		
				Direct.	-85 44.9	w. by N.	+38	-85 07		
21.	-64 20	140 40	5 40 A.M.	Direct.	-85 45.8	w.N.W.	+52	-84 54	-84 36	
			to	S.	-85 53.4		-85 01			
			7 00 A.M.	N.	-85 59.0		-85 07			
				N.S.	-86 11.0		-85 19			
			Direct.	-85 51.7			-85 00			
	-64 08	140 14	11 30 A.M.	Direct.	-84 24.5*	N. 1/2 W.				
22.	-63 09	139 28	9 30 A.M.	Direct.	-85 54.5	n.w. by w.	+62	-85 14	-84 46	
			to	S.	-86 33.1					
			11 10 A.M.	N.	-86 57.1					
				N.S.	-86 25.7					
			Direct.	-86 02.0						

\* There is an obvious error here in the degree recorded; it should be probably 86°. The observation is not employed.—E. S.

## Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean In- clination. Face east.	True Inclination.	Remarks.	
	Lat.	Long.									
Mar. 22.	° /	° /	h m	Direct. Direct.	-85 59.7 -86 02.0	N.W. by W.	+62	-85 14	-84 46		
22.	-62 46	138 22	4 00 P.M.	Direct.	-85 48.8	N.W. by W.	+62	-84 48	-84 20		
23.	-62 13	136 20	10 15 A.M. to Noon.	Direct. S. N. N.S. Direct.	-85 37.9 -85 58.0 -85 51.5 -86 10.9 -85 32.5						
24.	-61 20	134 05	6 10 A.M. to 7 00 A.M.	Direct. S. N. N.S. Direct.	-85 19.1 -85 17.7 -85 33.9 -85 46.2 -85 07.5						
25.	-60 22	131 27	11 45 A.M.	Direct.	-85 05.5	N.W.	+72	-83 54	-83 31		
	-60 19	131 20	3 15 P.M. to 4 15 P.M.	Direct. S. N. N.S.	-85 04.1 -85 20.6 -85 21.4 -85 32.5	N.W. by N.	+79	-83 45 -84 02 -84 02 -84 13			
26.	-59 25	130 14	10 15 A.M. to 11 40 A.M.	Direct. S. N. N.S. Direct.	-84 29.0 -84 49.0 -84 28.7 -84 56.2 -84 33.5	N.W. by N.	+79	-83 20			-82 52
27.	-58 06	128 43	11 40 A.M.	Direct.	-84 03.0	N.N.W.	+86	-82 37			-82 09
28.	-57 22	127 37	10 30 A.M. 11 45 A.M.	Direct. Direct.	-82 37.7 -82 51.0	W. E.N.E.	+18 +49	-82 20 -82 02	-81 43	Much motion.	
29.	-56 28	129 57	11 30 A.M.	Direct.	-82 21.5	N.E.	+71	-81 11	-80 43	Ship very unsteady.	
30.	-55 00	131 43	6 15 A.M. to 7 15 A.M.	Direct. S. N. N.S.	-81 28.5 -81 14.1 -82 29.2 -82 36.0	N.E. by E.	+62	-80 27 -80 12	-80 15	Ship very unsteady.	
	-55 11	132 10	11 45 A.M.	Direct.	-81 41.0	N.E. by N.	+77	-81 12 -81 19 -80 24			
	-54 55	132 50	5 00 P.M.	Direct. S. N. S. N. N.S.	-81 26.5 -81 48.5 -81 59.7 -81 54.7 -81 55.9 -82 05.5	N.E. by N.	+77	-80 10 -80 32 -80 43 -80 38	-80 07		
31.	-54 4	134 54	11 40 A.M. 0 15 P.M.	Direct. Direct.	-79 45.5 -80 25.0	E. ½ N. E.	+27 +19	-79 19 -80 06	-79 39		
	-54 00	135 02	1 00 P.M. 2 00 P.M. to 3 30 P.M.	Direct. S. N. N.S. Direct.	-80 00.0 -81 21.3 -81 50.2 -81 46.4 -81 26.6 -81 22.7	E. ½ N. N.W.	+27 +70	-79 33 -80 11 -80 40 -80 36 -80 17 -80 13			

## Observations of Inclination. (Continued.)

1841.	Position.		Time of day.	Method employed.	Observed Inclination. Face east.	Ship's head.	Correc- tion for ship's attrac- tion.	Mean In- clination. Face east.	True Inclination.	Remarks.
	Lat.	Long.								
April 1.	-53° 13'	135° 18'	h m							
			9 00 A.M.	Direct.	-80 48.5	} N.N.E.	+82	-79 37	-79 09	
			to	S.	-81 20.1					
11 45 A.M.	N.	-81 08.2								
				N.S.	-80 46.3					
				Direct.	-80 51.2					
2.	-51 16	136 50	6 00 A.M.	Direct.	-79 55.8	} N.N.E.	+82	-78 27	-77 59	
			to	S.	-79 49.5					
			7 15 A.M.	N.	-79 47.7					
				N.S.	-79 45.0					
3.	-48 56	138 34	11 45 A.M.	Direct.	-78 41.6	} N.N.E.	+81	-77 22	-76 54	Much sea.
			2 00 P.M.	Direct.	-78 50.3					
			to	N.	-79 09.4					
				N.S.	-78 13.0					
4.	-46 55	139 55	7 20 to	Direct.	-77 05.5	} N.E.	+69	-76 10	-75 42	Heavy sea, ship rolling deep.
			8 20 A.M.	N.	-77 29.8					
				N.S.	-77 20.7					
			10 30 A.M.	Direct.	-77 00.5	} N.E.				
			to	N.	-77 39.8					
			11 50 A.M.	N.S.	-77 37.9					
	-46 34	140 36	Noon.	S.	-77 37.5	} N.E.				Instrument in wrong azi- muth.
				N.	-77 33.2					
				N.S.	-77 49.1					
				Direct.	-78 11.5					
	-46 29	140 40	0 40 to	Direct.	-77 23.0	} N.E.	+69	-75 47	-75 12	Heavy sea.
			1 30 P.M.	S.	-76 33.5					
				N.	-76 29.0					
				N.S.	-77 18.0					
	-46 22	141 06	4 40 P.M.	Direct.	-76 48.5	} N.E. by E.	+62	-75 33		Much mo- tion.
			to	S.	-76 29.7					
			5 50 P.M.	N.	-76 10.2					
				N.S.	-76 50.6					
5.	-45 02	145 10	6 30 A.M.	Direct.	-76 04.0	} N.E. by E.	+60	-74 20	-73 54	
			to	S.	-75 02.2					
			8 30 A.M.	N.	-75 11.5					
				N.S.	-75 03.2					
	-44 52	143 27	11 40 A.M.	Direct.	-75 49.5	} N.E. by E.	+60	-74 24		
			4 30 P.M.	Direct.	-75 28.5					
			to	S.	-74 57.6					
			5 00 P.M.	N.	-75 20.9					
6.	-44 00	145 57	11 35 A.M.	Direct.	-73 49.8	} N.E. by E.	+58	-72 52	-72 15	Running along the land.
			1 20 P.M.	Direct.	-73 35.5					
			to	S.	-73 43.0					
	-43 41	146 03	4 30 P.M.	N.	-73 41.9	} N.E. ½ E.	+62	-72 40		
				N.S.	-73 47.6					

Observations of the INTENSITY of the Magnetic FORCE made in Her Majesty's Ship Erebus, from September 1840 to April 1841, with Needle R. F. 4.

Observers Captain Ross and Lieutenant SMITH, R.N.

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Sept. 17.	Magnetic Observatory, Hobarton. -42 52 147 24		Deflector S.	50 00.8	52	Observed on shore*.	1.820	.....	1.820	
18.			wt. ½ gr.	2 41.4	52					
			wt. 1 gr.	5 22.7	52					
			wt. 1½ gr.	8 14.6	52					
			wt. 2 grs.	10 49.6	52					
			wt. 3 grs.	16 15	52					
Oct. 17.	To obtain corrections for the ship's attraction.		S.	49 23	54	S.E. by s.	1.869	-035	1.834	} 1.823
			S.	49 51	54	w.	1.833	-003	1.830	
			S.	49 27.2	54	s. by E.	1.864	-043	1.821	
			S.	49 39	54	S.S.E.	1.849	-039	1.810	
21.			S.	49 50.9	51	W.N.W.	1.833	+008	1.841	
			S.	49 48.8	51	S.E.	1.835	-031	1.804	
29.			S.	50 19.8	48	N.	1.792	+028	1.820	
			S.	50 23.7	48	N.N.E.	1.787	+024	1.811	
			S.	50 21.8	48	N.E.	1.789	+020	1.809	
			S.	50 02.9	48	E.N.E.	1.816	+008	1.824	
			S.	49 53.5	48	E.	1.828	-003	1.825	
			S.	50 09.4	48	N.N.W.	1.807	+024	1.831	
			S.	50 12.6	48	N.W.	1.803	+020	1.823	
			S.	49 40	48	W.S.W.	1.848	-017	1.831	
			S.	49 52.2	48	w.	1.831	-003	1.828	
			S.	49 56.2	48	W.N.W.	1.826	+008	1.834	
			S.	49 28.8	48	S.W.	1.862	-031	1.831	
			S.	49 28.2	48	S.S.W.	1.863	-039	1.824	
			S.	49 27.0	48	s.	1.864	-046	1.818	
			S.	49 24.5	48	S.S.E.	1.867	-039	1.828	
	S.	49 39.5	48	S.E.	1.849	-031	1.818			
	S.	49 52.7	48	E.S.E.	1.830	-017	1.813			
Nov. 13.	-44 10 149 29	S.	49 23.8	54	E.S.E.	1.868	-017	1.851	} 1.844	
		N.	47 05.9	54		1.855	-017	1.838		
14.	-45 13 151 57	S.	49 34.5	45	S.E.	1.855	-031	1.824	} 1.833	
		N.	46 50.5	45		1.872	-031	1.841		
15.	-45 33 152 45	S.	49 56.9	51	E.	1.824	-003	1.821	} 1.843	
		N.	46 53.5	51		1.869	-003	1.866		
16.	-46 18 154 30	S.	49 50.7	57	E.S.E.	1.833	-017	1.816	} 1.820	
		N.	47 17	57		1.841	-017	1.824		
17.	-47 46 157 40	S.	49 52	51	S.E. by E. ½ E.	1.831	-020	1.811	} 1.817	
		N.	47 15	51		1.843	-020	1.823		
		S.	49 34	50		1.856	-020	1.836		
18.	-49 20 160 13	N.	46 47.2	50		1.876	-020	1.856	} 1.846	

\* The angles of deflection with 4, 5 and 6 grains, not having been observed at Hobarton, have been computed from the angles produced by the five weights which were employed at that station; they are as follows:—

gr.  
4 . . . . 22 06  
5 . . . . 28 03.5  
6 . . . . 34 21.

Much motion. Observations by no means good. Ship pitching greatly.

Much motion.

Observations of the Magnetic Force. (Continued.)

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Nov. 19.	-50° 28' 164 9		S.	49 11	49	E.	1.884	-0.03	1.881	1.858
			N.	47 20	49		1.838	-0.03	1.835	
21.	Auckland Island*. -50 33 166 19	At anchor.	S.	49 44.2	42	w.n.w.	1.842	+0.08	1.850	1.864
			N.	47 27.6	42		1.830	+0.08	1.838	
			wt. 1/2 gr.	2 33.9	42		1.830			
			wt. 1 gr.	5 13	50		1.876	+0.13	1.889	
			wt. 2 grs.	10 27.3	50		1.884	+0.13	1.897	
			wt. 3 grs.	15 28.6	50	n.w. by w.	1.909	+0.13	1.922	
26.			S.	49 29.2	41	s.s.w.	1.862	-0.37	1.825	
27.			S.	49 50.6	42	w.s.w.	1.833	-0.13	1.830	
			S.	49 29	53		1.862			
			N.	46 50.2	53		1.873			
24.	On shore.		wt. 1/2 gr.	2 33.5	52		1.844	.....	1.859	
			wt. 1 gr.	5 18.4	52		1.867			
			wt. 1 1/2 gr.	8 02.2	52		1.856			
			wt. 2 grs.	10 36.8	52		1.856			
			wt. 3 grs.	15 58.3	52		1.851			
26.	Pig Island.		S.	50 31	46	Observed on shore.	1.778			Excessive local attraction.
			N.	47 38	46		1.818			
	Shoe Island.		S.	47 50.7	44		1.981			
			N.	45 3.6	44		1.993			
30.	Ocean Point.		S.	49 49.8	51		1.834			
			S.	49 28	51		1.863			
	Sandy Bay.		S.	49 27	58		1.864	.....	1.847	
			N.	47 31.7	58		1.826			
			S.	59 56	55		.....			
Dec. 2.	Auckland Island.		N.	57 19.2	55		.....	.....	.....	Excessive local attraction.
6.			S.	49 35	50	s.w.	1.854	-0.30	1.824	1.836
			S.	49 05.9	50	s.s.w.	1.891	-0.36	1.855	
7.			S.	49 57.2	49	w. by s.	1.824	-0.08	1.816	
8.	At anchor.		S.	49 21.9	52	s.	1.871	-0.41	1.830	
			S.	49 19	52	s.s.e.	1.874	-0.36	1.838	
			S.	49 29.2	50	s.e.	1.862	-0.30	1.832	
			S.	49 29.5	50	e.s.e.	1.862	-0.15	1.847	
			S.	49 44.9	50	e.	1.841	-0.03	1.838	
			S.	49 46.7	51	e.n.e.	1.838	+0.08	1.846	
			S.	49 58	52	n.e.	1.823	+0.18	1.841	
			S.	50 06.9	52	n.n.e.	1.810	+0.21	1.831	
			S.	49 51.4	50	n.	1.832	+0.26	1.858	
			S.	50 01.8	50	n.n.w.	1.817	+0.21	1.838	
10.			S.	50 16.3	50	n.w.	1.797	+0.18	1.815	
			S.	49 27.2	52	s.e.	1.864	-0.30	1.834	

\* Mean of the results at Auckland Island, omitting those which appear to have been affected by excessive local attraction :

November 21 and 26, on board ..	1.864	} 1.851.
November 24, on shore ..	1.859	
November 30, on shore ..	1.847	
December 6, 7 and 8, on board ..	1.836	

## Observations of the Magnetic Force. (Continued.)

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 14.	Campbell Island*,	}	S.	50 01.4	50	N.W.	1.819	+018	1.837	}
			S.	49 39.2	50	W.	1.849	-003	1.846	
16.	at anchor.	}	S.	49 04.5	52	S.S.W.	1.893	-037	1.856	}
			S.	49 20.5	55		1.873			
15.	On shore.	-52 42 169 10	N.	46 10.8	55	Observed on shore.	1.917			}
			wt. 1/2 gr.	2 35.3	55		1.930			
			wt. 2 grs.	10 12.1	55		1.906			
			wt. 3 grs.	15 30.2	55					
			wt. 1/2 gr.	2 32.9	52					
			wt. 1 gr.	4 59.2	52					
			wt. 2 grs.	10 12.6	52					
			wt. 3 grs.	15 30.2	52					
			S.	49 17	52					
			N.	46 45.7	53					
18.	-53 47 169 02	}	S.	49 13.6	44	S.S.E.	1.881	-037	1.844	}
			N.	46 18.5	44	S.S.E. 1/2 E.	1.908	-034	1.874	
19.	-55 50 170 6	}	N.	45 48	48	s. by w.	1.943	-040	1.903	}
			N.S.	22 39.5	48					
21.	-57 15 170 40	}	N.	45 42.7	38	S.S.E.	1.949	-035	1.914	}
			N.S.	22 26						
22.	-57 54 170 25	}	N.	45 44.5	42	s. by E.	1.948	-037	1.911	}
			N.S.	22 25.6						
			S.	48 17.7	41					
			N.	45 25.2						
23.	-59 41 169 38	}	N.S.	22 31.7						}
			S.	48 11.5	39					
			N.	45 20.2		S.S.W.	1.959	-031	1.928	
			N.S.	22 29.5			1.975	-031	1.944	
24.	-59 48 169 42	}	N.S.	22 31.5	37	E.				}
			N.	45 16.9	36	S.E. 1/2 S.	1.978	-027	1.951	
			N.S.	22 27	36					
			S.	47 59.2	42					
25.	-60 14 170 15	}	N.	45 08.1	41	S.S.E.	1.972	-029	1.943	}
			N.S.	22 27	40		1.988	-029	1.959	
			S.	48 13.7	40					
			N.	45 15.1	40	S.E. by S.	1.956	-027	1.929	
26.	-60 31 170 32	}	N.S.	22 29.3	39		1.980	-027	1.953	}
			N.	45 08.4	35					
			N.S.	22 27.6	35	s.	1.988	-032	1.956	
			N.	45 00	46		1.997	+011	2.008	
27.	-60 46 170 44	}	N.S.	22 15.7	45	N.				}
			S.	47 33.2	34					
			N.	44 30.6	34		2.001	-032	1.969	
			N.S.	22 0.5	34	s.	2.029	-032	1.997	
28.	-62 40 174 40	}	N.S.	22 15.2	34					}
			S.	47 53.9	33		1.978	-026	1.952	
			N.	44 34.2	33	S.S.W. 1/2 W.	2.026	-026	2.000	
			N.S.	22 11.7	33					
29.	-62 52 174 28	}	S.	47 45	34	S.S.W.	1.988	-028	1.960	}
			N.	44 42.3	34		2.016	-030	1.986	
			N.S.	22 14.7		s. by w.				
			S.	47 45	34					

\* Mean of the results at Campbell Island :

December 14 and 15, on shore.. 1.909 } 1.877.  
December 14 and 16, on board.. 1.846 }

Observations of the Magnetic Force. (Continued.)

1840.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correc- tion for ship's attrac- tion.	Corrected Intensity.	Remarks.
Dec. 30.	-64 30	172 51	N.S.	22 17.6	33	s. by w.				
			S.	47 17	44	}	2.018	-0.30	1.988	} 1.988
	-64 31	173 00	N.	44 41.1			2.018	-0.30	1.988	
			N.S.	21 26.7		}				} 1.995
31.	-65 58	171 47	S.	46 58.5	34		s.	2.039	-0.28	
			N.	44 34		}	2.026	-0.28	1.998	} 1.995
			N.S.	21 36.2						
	-66 17	170 57	S.	47 29.5	35	}	2.005	-0.23	1.982	} 1.995
			N.	44 47.1			s. by w. 1/2 w.	2.012	-0.23	
			N.S.	21 52.3		}				} 2.008
1841. Jan. 1.	-66 30	169 13	S.	47 15.8	37		s.	2.020	-0.27	
			N.	44 30.1		}	2.030	-0.27	2.003	} 2.008
			N.S.	21 43.5						
	-66 32	169 45	S.	47 13	35	}				} 2.018
			N.S.	22 05.4			N.	2.023	+0.06	
	-66 23	170 12	S.	47 51.5	36	}	1.981	+0.04	1.985	} 2.018
2.			N.	44 13.9			N.N.W. 1/2 w.	2.047	+0.04	
			N.S.	21 56.1		}				} 2.046
3.	-65 39	170 44	S.	47 01.6	35		N.N.W.	2.035	+0.05	
			N.	44 14.5	34	}	2.047	+0.05	2.052	} 2.046
			N.S.	22 37.5	33					
	-65 22	170 40	S.	47 00.5	34	}	2.037	-0.13	2.024	} 2.025
4.			N.	44 20.5			E. 1/2 s.	2.040	-0.13	
			N.S.	21 54.1		}				} 2.009
5.	-66 55	174 31	S.	47 11.7	35		E.S.E.	2.024	-0.15	
			N.	44 35.9		}	2.023	-0.15	2.008	} 2.009
			N.S.	21 55						
6.	-68 17	175 0	S.	47 26.1	34	}	2.009	-0.15	1.994	} 2.011
7.	-68 32	175 49	S.	47 15.8			E.	2.020	-0.12	
			N.	44 27.9		}	2.032	-0.12	2.020	} 2.011
			S.	47 16.5	30		w.	2.019	-0.12	
			N.	44 21.1		}	2.040	-0.12	2.028	} 2.032
8.	-68 28	176 31	S.	47 09.1	39		E. by N. 1/2 N.	2.027	-0.02	
			N.	44 04.7		}	2.058	-0.02	2.056	} 2.032
			N.S.	21 55						
			S.	47 03.3	39	}	2.034	-0.13	2.021	} 2.025
			N.	44 22.6			w. by s. 1/2 s.	2.038	-0.11	
			N.S.	22 00.1		}				} 2.025
	-68 28	176 32	S.	47 15.7	42		Observed on ice.	2.021		
			N.	44 17.1		}	2.044		2.044	} 2.025
			N.S.	21 54.8						
			wt. 1/2 gr.	2 28	41	}	2.021		2.021	} 2.016
			wt. 3 grs.	14 34.3				2.015		
			wt. 6 grs.	30 38.7		}	2.030	-0.21	2.009	} 2.016
9.	-68 48	176 45	S.	47 06			s.s.e.	2.045	-0.21	
			N.	44 16		}				} 2.033
			N.S.	21 48.2						
10.	-70 23	174 50	S.	46 58.9	32	}	2.038	-0.22	2.016	} 2.033
			N.	43 49.2	31			2.073	-0.22	
			N.S.	22 10		}				} 2.030
11.	-71 15	171 15	S.	46 47.5	30		s.	2.050	-0.22	
			N.	44 07.3	30	}	2.054	-0.22	2.032	} 2.030
			N.S.	22 03.5						
	-71 24	170 44	S.	46 49.9	45	}	2.047	-0.21	2.026	} 2.029
			N.	44 08.6			s. by w.	2.053	-0.21	
			N.S.	21 53.6	43					



Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.		
Jan. 12.	-71 47	170 52	S.	46 41.5	34	W.S.W.	2.057	-.011	2.046	2.056	Much motion. Observations indifferent.	
			N.	43 44.1	33		2.078	-.011	2.067			
13.	-72 07	172 19	S.	47 24.5	33	E. by N. 1/2 N.	2.011	-.005	2.006	2.038		
			N.	43 47.4	33		2.075	-.005	2.070			
15.	-71 55	171 51	N.S.	21 47.9	33	E.	2.010	-.007	2.003	2.028		
			S.	47 25.2	33		2.060	-.007	2.053			
			N.	44 02			2.044	-.019	2.025			
16.	-72 12	172 13	S.	46 52.4	28	s. by w.	2.058	-.019	2.039	2.032		
			N.	44 04			2.033	-.007	2.026			
17.	-72 09	173 35	N.S.	21 47.5	30	E.	2.070	-.014	2.056	2.038		Much motion.
			N.	44 26.7	30		2.031	-.011	2.020			
18.	-72 57	176 06	N.S.	21 36.5	31	S.E. by E.	2.047	-.015	2.032	2.035		
			S.	46 30.1	31		2.054	-.015	2.039			
19.	-72 35	173 34	N.	44 07.9	41	s.w. by w.	2.044	-.018	2.026	2.039		
			N.S.	21 54.8	34		2.070	-.018	2.052			
	-72 31	173 39	S.	46 53	34	s. by E. 1/2 E.	2.067	-.014	2.053	2.052		
			N.	43 51.8	34		2.066	-.014	2.052			
			N.S.	21 50.1			2.046	-.019	2.027			
20.	-73 47	171 50	S.	46 31.9	34	S.E.	2.080	-.019	2.061	2.044		
			N.	43 56.3			2.056	-.004	2.052			
			N.S.	21 37.7		N. by E.	2.056	-.004	2.052	2.052		
			S.	46 50.7	30		2.041	-.017	2.024			
21.	-74 10	170 28	N.	43 41.8	30	s. by E.	2.062	-.017	2.045	2.035	Very unsteady.	
			N.S.	21 39			2.055	-.017	2.038			
			N.S.	22 08.6		s. by E.	2.045	-.018	2.027	2.037		
			S.	46 42	31		2.063	-.018	2.045			
	-74 06	171 20	N.	44 06		S. 1/2 W.	2.048	-.007	2.041	2.045		
			N.S.	21 52.2			2.056	-.007	2.049			
22.	-73 56	172 20	S.	46 57.7	32	E.	2.056	-.016	2.040	2.048		
			N.	44 00			2.073	-.016	2.057			
			N.S.	21 52.2		S.S.E.	2.036	-.015	2.026	2.031		
			S.	46 42	30		2.055	-.015	2.040			
24.	-74 35	173 01	N.	44 07	29	S.E.	2.037	-.008	2.029	2.040	Two points out of the meridian.	
			N.S.	21 27.8			2.058	-.008	2.050			
25.	-74 36	173 01	S.	46 51.7	29	E.	2.015	-.005	2.015	2.017		
			N.	43 59			2.028	-.005	2.023			
25.	-74 44	169 43	N.S.	21 47		N. by w.	2.048	-.007	2.041	2.045		
			S.	46 48.6	30		2.056	-.007	2.049			
			N.	44 05.7	30	E.	2.056	-.007	2.049	2.045		
			N.S.	21 50.3	29		2.056	-.016	2.040			
27.	-75 22	168 48	S.	46 42	30	S.S.E.	2.056	-.016	2.040	2.048		
			N.	43 48.6	28		2.073	-.016	2.057			
			N.S.	22 01	27	S.E.	2.036	-.015	2.026	2.031		
			S.	47 01.2	33		2.055	-.015	2.040			
	-76 06	168 11	N.	44 07.3		S.E.	2.037	-.008	2.029	2.040		
			N.S.	21 44.4			2.058	-.008	2.050			
28.	-76 46	169 22	S.	46 59.9	37	E.	2.015	-.005	2.015	2.017		
			N.	44 03.7	37		2.028	-.005	2.023			
			N.S.	22 0.0	37	N. by w.	2.015	-.005	2.015	2.017		
			S.	47 19.9	29		2.028	-.005	2.023			
29.	-77 47	175 43	N.	44 32.2	29	N. by w.	2.015	-.005	2.015	2.017		
			N.S.	21 51.9	28		2.028	-.005	2.023			

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 31.	-77 04	188 18	S.	47 43.6	25	N.E. by N.	1.989	-.001	1.988	} Ship's motion very considerable.
			N.	44 23.5			2.036	-.001	2.035	
			N.S.	22 26.6					2.017	
Feb. 1.	-77 04	188 30	S.	47 06.9		S.E.	2.029	-.016	2.013	
			N.	44 13.5			2.047	-.016	2.031	
			N.S.	22 14.8						
	-77 09	188 15	wt. 6 grs.	30 45	30	S.E.	2.014	.....	.....	
			wt. 1 gr.	4 42	31					
			wt. 1/2 gr.	2 27.6	31					
3.	-77 17	185 26	S.	46 59.9	33	w.s.w.	2.037	-.012	2.025	
			N.	44 02.6	34		2.034	-.012	2.022	
			N.S.	21 55.6	35					
4.	-77 00	192 18	S.	46 57.2		E. by N.	2.040	-.006	2.034	} 2.039
			N.	44 16.3	24		2.045	-.006	2.039	
			N.S.	22 00.1						
			S.	47 01.7	23	E.	2.035	-.006	2.029	} 2.036
			N.	44 00	21		2.062	-.006	2.056	
			N.S.	22 00.1			2.039	-.007	2.032	
5.	-77 10	192 48	S.	46 57.8	24	E.	2.047	-.007	2.040	} 2.020
			N.	44 14.2						
			N.S.	22 10	19					
	-77 14	192 02	S.	46 41.5	20	s.	2.056	-.021	2.035	} 2.020
			N.	44 33	19		2.027	-.021	2.006	
			N.S.	22 07.8	18					
6.	-77 09	188 50	S.	47 07.7	28	E.N.E.	2.028	-.005	2.023	} 2.036
			N.	44 06.6	24		2.055	-.005	2.050	
			N.S.	21 58.9						
7.	-76 58	180 40	S.	46 50.9	27	s. by w.	2.046	-.019	2.027	} 2.035
			N.	44 00.4	24		2.062	-.019	2.043	
			N.S.	22 02.3	23					
8.	-77 47	187 18	S.	47 03	34	N.E. by E. 1/2 E.	2.034	-.004	2.030	} 2.035
			N.	44 23.2	33		2.038	-.004	2.034	
			N.S.	22 03.4	32					
			wt. 6 grs.	30 30.9						
			wt. 3 grs.	14 14.6						
			wt. 2 grs.	9 15.6						
			wt. 1 gr.	6 15.1						
			wt. 1/2 gr.	2 27.8						
10.	-77 39	187 06	wt. 6 grs.	30 34.7	28	s. by E.	2.019	-.019	2.000	
			wt. 3 grs.	14 37			2.019	-.019	2.000	
			wt. 2 grs.	9 30.9			2.067	-.019	2.048	
			wt. 1 gr.	4 34.2						
			wt. 1/2 gr.	2 13.2						
			S.	46 55.5	33	N.W.	2.041	-.019	2.022	
			N.	44 13.9	29		2.047	-.019	2.028	
			N.S.	21 55.9	29		2.041	-.019	2.022	
11.	-76 55	188 40	S.	46 47	21	S.E. by E.	2.050	-.002	2.048	} Much motion.
12.	-76 50	183 26	N.	44 13.2	25		2.048	-.013	2.035	
			N.S.	21 47.5	24					
14.	-76 16	175 50	S.	46 55.1	34	s.s.w.	2.042	-.017	2.025	
			N.	44 33.7	33		2.026	-.017	2.009	
			N.S.	22 09.9	32					
15.	-76 03	169 30	N.	44 08.5	30	s.	2.053	-.020	2.033	
			N.S.	22 00.2	30					
			S.	46 45.9	30					
16.	-76 20	165 32	S.	44 08.4	30	S.S.E.	2.051	-.012	2.039	
			N.	44 08.4	30		2.054	-.012	2.042	
			N.S.	22 09.6	29					

## Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 19.	-75 03 168 44		S.	46 38.8	35	s.w.	2.059	-.011	2.048	2.040
			N.	44 16.9	32		2.044	-.011	2.033	
			N.S.	22 03.2	31					
21.	-71 17 170 43		S.	46 55.7	32	s.w. by w. 1/2 w.	2.041	-.011	2.030	2.037
			N.	44 07.7	30		2.055	-.011	2.044	
			N.S.	22 01.3	23					
	-71 34 178 07		S.	47 04	27	w.	2.033	-.007	2.026	2.026
			N.	44 28.2	26		2.032	-.007	2.025	
			N.S.	22 12	26					
22.	-70 41 167 26		S.	47 01.4	24	N.N.E.	2.036	-.001	2.035	Much motion.
			N.	43 48.5	24		2.073	-.001	2.072	
			N.S.	22 01.3	23					
24.	-70 14 167 34		S.	46 43.4	26	s.s.w. 1/2 w.	2.055	-.018	2.037	2.036
			N.	44 09.6	25		2.052	-.018	2.034	
			N.S.	22 12.1	24					
25.	-70 14 167 16		N.	44 35.3	22	s.	2.024	-.020	2.004	Much motion.
			N.S.	21 41.1	19					
			N.S.	21 41.1	19					
27.	-69 24 167 55		S.	46 46.5	30	s.e.	2.050	-.016	2.034	Unsteady.
			N.S.	21 59.9	29					
			N.S.	21 59.9	29					
28.	-69 40 167 48		N.	44 27.1	22	s. by e.	2.033	-.019	2.014	2.025
			N.S.	21 55.9	21					
			N.S.	21 55.9	21					
Mar. 1.	-69 08 167 44		N.	44 31	24	N.w. by w.	2.029	-.002	2.027	
			N.S.	21 56	22					
			N.S.	21 56	22					
2.	-68 28 168 10		S.	46 50.3	27	w. by N.	2.048	-.005	2.043	2.047
			N.	44 07.8	26		2.054	-.002	2.052	
			N.S.	22 20	28					
3.	-67 52 167 28		S.	46 43.4	16	w.	2.055	-.007	2.048	2.043
			N.	44 17.5	14		2.044	-.007	2.037	
			N.S.	22 27.9	14					
5.	-65 31 167 42		N.	44 25.1	28	N.	2.035	+.006	2.041	A good deal of motion.
			N.S.	22 23.2	27					
			N.S.	22 23.2	27					
7.	-65 33 162 14		S.	47 31.7	34	N.w.	2.002	+.003	2.005	2.024
			S.	47 17.9	35		2.017	+.004	2.021	
			N.	44 19.6	33		2.041	+.004	2.045	
8.	-64 41 162 34		N.S.	22 09.6	34	N.E. by N.				
			S.	47 29.3	31		2.005	+.002	2.007	
			N.	44 33	30		2.027	+.002	2.029	
11.	-64 13 163 18		N.S.	22 29.8	30	N.w. by w.				2.018
			S.	47 06.8	31		2.029	-.022	2.007	
			N.	44 25.4	30		2.035	-.022	2.013	
12.	-63 57 161 11		N.S.	21 59	30	s. by w.				2.010
			S.	47 13	28		2.023	-.012	2.011	
			N.	44 16.7	28		2.045	-.012	2.033	
14.	-62 41 156 59		N.S.	21 49.7	28	w.				2.022
			S.	47 02.7	33		2.034	-.024	2.010	
			N.	44 22.3	31		2.039	-.024	2.015	
15.	-63 50 156 06		N.S.	21 40.8	31	s. 1/2 w.				2.013
			S.	47 04.3	22		2.033	-.020	2.013	
			N.	44 31	22		2.029	-.020	2.009	
16.	-64 13 154 03		N.S.	22 10.1	22	s.w. by s.				2.011
			S.	46 50.1	26		2.047	-.020	2.027	
			N.	44 03.6	25		2.058	-.020	2.038	
17.	-64 20 153 02		N.S.	22 09.2	25	w. by N.				2.032
			S.	44 32	29		2.028	-.005	2.023	
			N.	44 32	29					
18.	-63 54 151 56		N.S.	22 42	27	w. by N.				A heavy head swell.
			S.	46 23.5	30		2.078	-.020	2.058	
			N.	43 29.9	29		2.092	-.020	2.072	
19.	-64 26 148 20		N.S.	22 01	29	s.w. by s.				2.065



## Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
April 4.	—46 22	141 06	S.	48 31.5	45	N.E. by E.	1.934	+0.11	1.945	1.954
			N.	45 40.2	45		1.952	+0.11	1.963	
5.	—45 02	143 10	N.S.	23 00.9	45	N.E. by E.	1.917	+0.12	1.929	1.923
			S.	48 46.2	46		1.913	+0.12	1.925	
6.	—43 41	146 03	N.S.	22 05.9	47	N.E. by E.	1.912	+0.13	1.925	1.923
			S.	48 49.8	50		1.901	+0.13	1.914	
			N.	46 25.1	48	N.E. by E.	1.820	+0.18	1.838	1.892
			S.	50 01.4	60		1.884	+0.18	1.902	
			N.S.	23 16.8	59	N.E. ½ E.	1.887	+0.18	1.905	1.892
			wt. 6 grs.	32 58.5	58		1.919	+0.18	1.937	
			wt. 5 grs.	26 29.7	58	N.E. ½ E.	1.881	+0.18	1.899	1.892
			wt. 4 grs.	21 21	59		1.850	+0.18	1.868	
			wt. 3 grs.	15 59.4	59	N.E. ½ E.	1.885	+0.18	1.903	1.892
			wt. 2 grs.	10 27.2	58		1.870	+0.18	1.888	
			wt. 1 gr.	5 14.2	58					Running along the land.

Observations of DECLINATION made on board Her Majesty's Ship Terror, between November 15, 1840, and April 5, 1841.

The Observers are distinguished by their Initials as follows:—C. Captain CROZIER; P. Lieut. PHILLIPS; CR. Mr. COTTER, Master.

1840.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.		
	Lat.	Long.											
Nov 15.	44° 24'	152° 58'	CR.	6° 57'	S.E. by E.	-71 40	-4 44	-11 41	+1 23	-11 38	Compass R. of Cummins, index error ascertained at Hobarton, June 1841.		
	44 24	152 58	CR.	9 36	S.E. by E.		-4 44	-14 20				-13 01	
	16.	46 05	154 18	C.	10 52	S.E.	-72 00	-4 09	-15 01	+1 23		-13 47	
		46 11	154 18	CR.	12 57	S.E.		-4 09	-17 06				-15 10
	18.	46 11	154 18	CR.	9 48	S.E.	-73 00	-4 09	-13 57	+1 23		-14 44	
		46 24	154 50	CR.	9 48	S.E. by E.		-4 49	-14 37				-16 07
		49 06	160 10	C.	11 12	S.E. by E. 1/2 E.		-5 20	-16 32				-16 07
		49 14	160 06	CR.	11 54	S.E. by E. 1/2 E.		-5 20	-17 14				-16 07
		49 14	160 06	CR.	9 39	S.E. by E. 1/2 E.		-5 20	-43 59				-16 43
	Dec. 6.	Auckland Island. At anchor.		CR.	21 10	S.W. by W.	-73 10	+5 09	-16 01	+1 23		-15 29	
8.		11.	CR.	21 12	S.W. by W.	+5 09		-16 03	-16 52				
			CR.	22 48	S.W.	+4 27		-18 21	-16 52				
12.			CR.	12 11	E.N.E.	-73 10	-5 07	-17 18	+1 23	-15 29			
			CR.	21 59	S.W. by W.		+5 09	-16 50			-16 52		
			CR.	21 47	N.W. by W.		+4 29	-17 18			-16 52		
			CR.	20 32	N.W. by W.		+4 29	-15 03			-16 52		
			C.	19 32	W.N.W.		+5 07	-14 25			-16 52		
			C.	19 47	W.N.W.		+5 07	-14 40			-16 52		
			C.	20 14	N.W. by W.		+4 29	-15 45			-16 52		
			C.	19 23	N.W.		+3 46	-15 37			-16 52		
			C.	22 09	W. by N.		+5 35	-16 34			-16 52		
			C.	21 28	N.W. by W.		+4 29	-16 59			-16 52		
			C.	20 29	N.W. by W. 1/2 W.		+4 48	-15 41			-16 52		
			C.	23 00	W.		+5 49	-17 11			-16 52		
			C.	22 07	W. by N. 1/2 N.		+5 21	-16 46			-16 52		
			C.	22 05	W. by N.		+5 35	-16 30			-16 52		
			C.	21 59	W. 1/2 N.		+5 42	-16 17			-16 52		
			C.	22 36	W. 1/4 S.		+5 50	-16 46			-16 52		
			C.	21 40	W.		+5 49	-15 51			-16 52		
			C.	20 54	N.W. by W.		+4 29	-16 25			-16 52		
			C.	21 50	W.N.W.		+5 07	-16 43			-16 52		
			C.	24 23	W. by N.		+3 35	-18 48			-16 52		
			CR.	20 20	N.W. by W.		+4 29	-15 51			-16 52		
			CR.	20 29	N.W. by W.		+4 29	-16 00			-16 52		
			CR.	19 39	N.W.		+3 46	-15 53			-16 52		
			CR.	21 02	W.N.W.		+5 07	-15 55			-16 52		
			CR.	21 19	W.N.W.		+5 07	-16 12			-16 52		
			CR.	22 12	W.N.W.		+5 07	-17 05			-16 52		
			CR.	21 49	W. by N.		+5 35	-16 14			-16 52		
			CR.	21 52	W. by N.		+5 35	-16 17			-16 52		
CR.	23 29	W.	+5 49	-17 40	-16 52								
C.	12 41	N.E.	-3 46	-16 27	-16 52								
C.	13 20	N.E. by N.	-2 57	-16 17	-16 52								
C.	13 49	N.N.E.	-1 58	-15 47	-16 52								
C.	13 18	E.S.E.	-5 36	-18 54	-16 52								
C.	13 18	S.E. by E.	-5 09	-18 27	-16 52								
CR.	13 21	N.E.	-3 46	-17 07	-16 52								
CR.	15 34	N.N.E.	-1 58	-17 32	-16 52								
CR.	15 17	N.E.	-3 46	-19 03	-16 52								
CR.	11 15	E. by S.	-5 51	-17 06	-16 52								
CR.	12 32	E.S.E.	-5 36	-18 08	-16 52								

## Observations of Declination. (Continued.)

1840.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's attraction.	Corrected Declination.	Correc- tion for index error.	True Declination.	Remarks.
	Lat.	Long.									
Dec. 12.	-50 32	167 45	C.	-14 02	s.e. by E.	-73 00	-5 06	-19 08			
13.	-52 30	169 50	C.	-13 23	s.e. by E.	-73 00	-5 22	-18 45			
	-52 30	169 50	C.	-12 57	s.e. by E.		-5 22	-18 19			
16.	-52 34	169 50	CR.	-22 21	w. by s.	-73 53	+6 08	-16 13			
	-52 34	169 50	CR.	-21 49	w.s.w.		+5 50	-15 59			
	-52 34	169 50	CR.	-22 50	w.s.w.		+5 50	-17 00	-18 31	+1 23	-17 08
	-52 34	169 50	CR.	-23 01	s.w. by w.		+5 21	-17 40			
	-52 34	169 50	CR.	-23 10	s.w. by w.		+5 21	-17 49			
	-52 34	169 50	CR.	-19 55	s.w.		+4 38	-15 15			
17.	-52 34	169 50	CR.	-12 59	E.S.E.	-76 30	-5 50	-18 49			
	-52 34	169 50	CR.	-12 53	E.S.E.		-5 50	-18 43			
20.	-56 39	168 54	CR.	-14 11	S.S.E.	-77 10	-2 58	-17 09			
21.	-57 33	170 30	C.	-21 54	S.S.E.		-3 06	-25 00			
	-57 33	170 30	C.	-21 06	S.S.E.	-77 10	-3 06	-24 12			
	-57 33	170 30	C.	-20 28	s. by E.		-1 36	-22 04			
	-57 33	170 30	C.	-23 45	s. by E.	-78 10	-1 36	-25 21			
22.	-58 54	171 02	CR.	-25 00	s. by E.		-1 44	-26 44	-23 21	+1 23	-21 58
	-58 54	171 02	C.	-20 41	s. by E. 1/2 E.	-78 10	-2 36	-23 17			
	-58 54	171 02	C.	-20 41	S.S.E.		-3 23	-24 04			
	-58 54	171 02	CR.	-20 21	S.S.E.	-78 10	-3 23	-23 44			
	-59 04	171 00	C.	-26 54	S.S.W.		+3 23	-23 31			
	-59 04	171 00	C.	-25 15	S.S.W.	-78 30	+3 23	-23 52			
	-59 04	171 00	C.	-26 34	S.S.W.		+3 23	-23 11			
23.	-59 32	170 05	C.	-24 05	S.S.W. 1/2 W.	-78 30	+4 17	-19 48			
	-59 32	170 05	CR.	-17 24	S.E.		-6 23	-23 47			
	-59 32	170 05	CR.	-16 38	S.E. by E.	-78 30	-7 23	-24 01			
	-59 32	170 05	CR.	-18 02	S.E. by S.		-5 03	-23 05			
	-59 32	170 05	CR.	-21 02	S.S.E.	-78 30	-3 31	-24 33			
	-59 32	170 05	CR.	-23 36	S.		0 0	-23 36			
	-59 32	170 05	CR.	-24 03	s. by w.	-78 30	+1 48	-22 15	-22 19	+1 23	-20 56
	-59 32	170 05	CR.	-26 39	S.S.W.		+3 31	-23 08			
	-59 32	170 05	CR.	-26 52	s.w. by s.	-78 30	+5 03	-21 49			
	-59 32	170 05	CR.	-28 17	S.W.		+6 23	-21 54			
	-59 32	170 05	CR.	-29 01	s.w. by w.	-78 30	+7 23	-21 38			
	-59 32	170 05	CR.	-28 11	w. by N.		+8 11	-20 00			
	-59 32	170 05	CR.	-28 10	w.N.W.	-78 30	+7 36	-20 34			
23.	-59 32	170 05	CR.	-27 50	N.W. by w.		+6 45	-21 05			
	-59 32	170 05	CR.	-26 47	N.W.	-78 30	+5 41	-21 06			
	-59 32	170 05	CR.	-25 49	N.W. by N.		+4 26	-21 23			
	-59 32	170 05	CR.	-23 55	N. by w.	-78 30	+1 33	-22 22	-21 43	+1 23	-20 20
	-59 32	170 05	CR.	-21 34	N.		0 0	-21 34			
	-59 32	170 05	CR.	-20 17	N. by E.	-78 30	-1 33	-21 50			
	-59 32	170 05	CR.	-18 32	N.N.E.		-3 02	-21 34			
	-59 32	170 05	CR.	-18 22	N.E. by N.	-79 00	-4 26	-22 48			
	-59 37	169 17	C.	-14 38	S.S.E. 3/4 E.		-4 53	-19 31			
	-59 37	169 17	C.	-15 17	S.S.E. 3/4 E.	-79 00	-4 53	-20 10			
24.	-60 17	170 12	C.	-25 59	S.		0 0	-25 59			
	-60 17	170 12	C.	-23 38	S.S.E.	-79 00	-3 41	-27 19			
	-60 17	170 12	C.	-22 25	S.E. by S.		-5 17	-27 42			
	-60 17	170 12	C.	-23 51	S.S.E.	-79 00	-3 41	-27 32	-25 11	+1 23	-23 48
	-60 17	170 12	C.	-22 00	S.E. 1/2 S.		-6 00	-28 00			
	-60 35	170 34	CR.	-18 19	S.E.	-79 00	-6 41	-25 00			
	-60 35	170 34	CR.	-17 57	S.E.		-6 41	-24 38			
	-60 35	170 34	CR.	-21 50	S.S.E.	-79 00	-3 41	-25 31			
	-60 35	170 34	CR.	-21 14	S.S.E.		-3 41	-24 55			
	-60 35	170 34	CR.	-20 40	S.E. by S.	-5 17	-25 57				

Observations of Declination. (Continued.)

1840.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's attraction.	Corrected Declination.	Correc- tion for index error.	True Declination.	Remarks.					
	Lat.	Long.														
Dec. 29.	-64 11	172 43	C.	-27 44	s. 1/2 E.	-81 15	-1 08	-28 52	+1 23	-25 52						
	-64 11	172 43	CR.	-24 39	s. by E.		-2 16	-26 55								
	-64 11	172 43	CR.	-25 09	s. by E.		-2 16	-27 25								
	30.	-64 26	173 15	C.	-34 58		s.w.	+ 8 23				-26 35				
		-64 26	173 15	C.	-34 22		s.w.	+ 8 23				-25 59				
		-64 26	173 15	C.	-35 07		s.w. 1/2 s.	+ 7 30				-27 37				
		-64 26	173 15	C.	-32 54		s.s.w.	+ 4 34				-28 20				
		-64 48	172 56	CR.	-25 15		s. by E.	-2 16				-27 31				
		-64 48	172 56	CR.	-34 20		s.w.	+ 8 23				-25 57				
	31.	-65 42	172 13	C.	-26 09		s. 1/2 E.	-82 00				-1 10	-27 19	+1 23	26 17	
		-65 42	172 13	C.	-26 13		s. by E.					-2 24	-28 37			
		-65 42	172 13	C.	-25 23		s. by E.					-2 24	-27 47			
-65 42		172 13	CR.	-26 26	s. by E.	-2 24	-28 40									
-65 42		172 13	CR.	-26 18	s. by E.	-2 24	-28 42									
-65 42		172 13	CR.	-23 34	s. by E.	-2 24	-25 58									
1841.																
Jan. 2.	-66 24	170 00	C.	-17 14	E. by s. 1/2 s.	-82 00	-11 57	-29 11	+1 23	-29 17						
	4.	-65 15	172 40	CR.	-19 54		S.E.	-9 09				-29 03				
		-65 15	172 40	CR.	-20 48		S.E.	-9 09				-29 57				
	-65 27	173 20	CR.	-21 14	E. by s. 1/2 s.		-11 57	-33 11								
	-65 27	173 20	C.	-21 00	E. by s. 1/2 s.		-11 57	-32 57								
	-65 27	173 20	C.	-17 49	E. 1/2 s.		-12 13	-30 02								
	-65 27	173 20	C.	-19 17	E. by s. 1/2 s.		-11 57	-31 14								
	-65 30	173 30	C.	-20 04	E. by s. 1/2 s.		-11 57	-32 01								
	-65 30	173 30	C.	-21 11	E.S.E.		-11 44	-32 55								
	-65 31	173 40	C.	-22 19	S.E. by E.		-10 38	-32 57								
	-65 32	173 50	C.	-21 48	S.E. 1/2 E.		-9 53	-31 41								
	-65 32	173 50	C.	-25 56	S.S.E. 1/2 E.		-6 07	-32 03								
	-65 32	173 50	C.	-22 38	S.E. by E. 1/2 E.		-10 34	-33 12								
	-65 35	173 52	C.	-26 59	S.S.E.		-4 41	-31 40								
	-65 35	173 52	C.	-26 54	s. by E.		-2 18	-29 12								
	-65 35	173 52	C.	-25 22	S.S.E. 1/2 E.		-5 45	-31 07								
	-65 35	173 52	C.	-25 54	S.S.E.		-4 40	-30 34								
	-65 27	173 20	P.	-23 56	E. by s. 1/2 s.		-11 16	-35 12								
	-65 35	173 52	P.	-22 34	S.E. by E.		-10 02	-32 36								
	-65 28	173 20	CR.	-18 25	E. by s.		-11 25	-29 50								
	-65 28	173 20	CR.	-17 29	E.S.E.		-11 04	-28 33								
	-65 28	173 20	CR.	-18 27	E.S.E.		-11 04	-29 31								
	-65 28	173 30	CR.	-20 09	E.S.E.		-11 04	-31 13								
	5.	-66 15	173 32	CR.	-25 37		S.S.E.	-4 41				-30 18				
	6.	-68 07	175 12	CR.	-30 21		S.S.E.	-5 57				-36 18				
		-68 07	175 12	CR.	-30 28		S.S.E.	-5 57				-36 25				
	7.	-68 30	175 30	CR.	-24 25		S.E. by E.	-12 58				-37 43				
		-68 30	175 30	CR.	-23 36		S.E. by E.	-12 58				-36 34				
	-68 30	175 30	CR.	-23 42	S.E.		-11 00	-34 42								
	-68 30	175 30	CR.	-23 12	E.S.E.		-14 09	-37 21								
	-68 30	175 30	CR.	-47 46	S.W. by W.		+12 58	-34 48								
	8.	-68 26	176 32	C.	-22 19		S.E. by E.	-12 58				-35 17				
-68 26		176 32	C.	-20 36	s. 73° E.	-14 30	-35 06									
-68 26		176 32	C.	-20 59	s. 85° E.	-14 56	-35 55									
11.	-70 53	173 00	C.	-45 31	s. 1/4 E.	-1 10	-46 41									
	-70 53	173 00	C.	-48 51	s. by W.	+ 4 43	-44 08									
	-70 53	173 00	C.	-43 10	s.	0 0	-43 10									
	-70 53	173 00	CR.	-43 22	s.	0 0	-43 22									
	-70 53	173 00	CR.	-44 57	s.	0 0	-44 57									

A light card of CUMMINS, marked P, was now used. Index error ascertained at Hobarton, June 1841.



Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Jan. 11.	-71° 21'	171° 14'	CR.	- 49 10	s. ½ w.	-85 50	+ 2 20	- 46 50	- 46 48	+ 1 03	- 45 45
	-71 21	171 14	C.	- 51 03	s.		0 0	- 51 03			
	-71 21	171 14	C.	- 53 04	s. by w.		+ 4 43	- 48 21			
	-71 21	171 14	C.	- 54 21	s. by w.		+ 4 43	- 49 38			
	-71 21	171 14	C.	- 54 32	s. by w.		+ 4 43	- 49 49			
	-71 21	171 14	C.	- 53 11	s. by w.		+ 4 56	- 48 15			
	-71 21	171 14	C.	- 51 22	s.		0 0	- 51 22			
	-71 21	171 14	C.	- 51 33	s. by w.		+ 4 56	- 46 37			
	-71 21	171 14	C.	- 50 08	s. by w.		+ 4 56	- 45 12			
	-71 21	171 14	CR.	- 52 01	s. by w.		+ 4 56	- 47 05			
	-71 21	171 14	CR.	- 53 19	s. by w.		+ 4 56	- 48 23			
	-71 21	171 14	CR.	- 53 18	s. by w.		+ 4 56	- 48 22			
	-71 21	171 14	CR.	- 53 00	s. by w.		+ 4 56	- 48 04			
	-71 48	171 21	C.	- 50 53	s. by w.		+ 4 56	- 45 57			
	-71 48	171 21	C.	- 57 58	s.w. by s.		+ 14 14	- 43 44			
	-71 48	171 21	C.	- 53 25	s. by w. ½ w.		+ 7 22	- 48 03			
	-71 48	171 21	C.	- 27 35	E. by s. ½ s.		- 24 22	- 51 57			
	-71 48	171 21	CR.	- 52 46	s.s.w.		+ 9 48	- 42 58			
	-71 48	171 21	CR.	- 54 17	s.s.w.		+ 9 48	- 44 29			
	-71 48	171 21	CR.	- 53 06	s. by w.		+ 4 56	- 48 10			
-71 48	171 21	CR.	- 53 11	s. by w.	+ 4 56	- 48 15					
-71 48	171 21	CR.	- 25 06	E. by s.	- 25 04	- 50 10					
-71 48	171 21	CR.	- 26 50	E. by s.	- 25 04	- 51 54					
-72 06	171 07	CR.	- 58 11	s.s.w.	+ 9 48	- 48 23					
-72 06	171 07	CR.	- 58 27	s.s.w.	+ 9 48	- 48 39					
17.	-72 24	174 45	C.	- 35 06	s.E. by E.	-86 00	- 21 21	- 56 27	- 53 38	+ 1 03	- 52 35
	-72 25	174 50	C.	- 35 46	s.E. ½ E.		- 19 44	- 55 30			
	-72 13	173 59	CR.	- 35 00	s.E. by E.		- 21 21	- 56 21			
	-72 13	173 59	CR.	- 35 00	s.E. by E.		- 21 21	- 56 21			
-72 25	174 26	CR.	- 34 37	s.E. by E.	- 21 21	- 55 58					
-72 25	174 26	CR.	- 34 19	s.E. by E.	- 21 21	- 55 40					
18.	-73 03	176 20	C.	- 64 55	s.w. by s.	-86 00	+ 14 14	- 50 41	- 50 03	- 51 32	- 50 42
	-73 03	176 20	CR.	- 64 17	s.w. by s.		+ 14 14	- 50 03			
	-73 03	176 20	CR.	- 65 46	s.w. by s.		+ 14 14	- 51 32			
	-73 03	176 20	CR.	- 62 42	s.s.w. ½ w.		+ 12 00	- 50 42			
-73 03	176 20	CR.	- 64 56	s.w. by s.	+ 14 14	- 50 42					
19.	-72 34	173 21	C.	- 68 00	s.w. ¼ s.	-86 10	+ 16 53	- 51 07	- 49 52	+ 1 03	- 48 49
	-72 34	173 21	C.	- 68 37	s.w.		+ 18 55	- 49 42			
	-72 33	173 10	C.	- 66 01	s.w.		- 18 55	- 47 06			
	-72 33	173 10	C.	- 67 00	s.w. ¼ s.		+ 16 50	- 50 10			
	-72 32	172 27	CR.	- 69 35	s.w.		+ 18 55	- 50 40			
	-72 32	172 27	CR.	- 67 12	s.w. ½ s.		+ 16 53	- 50 19			
	-72 32	172 27	CR.	- 67 40	s.w.		+ 18 55	- 48 45			
	-72 32	172 27	CR.	- 67 57	s.w. ½ s.		+ 16 53	- 51 04			
	-72 31	172 47	C.	- 44 51	s.s.E. ½ E.		- 12 30	- 57 21			
	-72 31	172 47	C.	- 44 23	s.s.E. ½ E.		- 12 30	- 56 53			
-72 31	172 47	CR.	- 43 53	s.s.E.	- 10 12	- 54 05					
-72 31	172 47	CR.	- 45 36	s.s.E.	- 10 12	- 55 48					
-72 31	172 47	CR.	- 49 19	s. by E.	- 5 08	- 54 27					
-72 31	172 47	CR.	- 54 17	s.	0 0	- 54 17					
-72 31	172 47	CR.	- 53 18	s.	0 0	- 53 18					
-72 52	172 20	P.	- 48 34	s.s.E.	- 10 12	- 58 46					
22.	-73 51	171 50	C.	- 34 19	E. by s.	-86 10	- 32 26	- 66 45	- 55 37	+ 1 03	- 54 34
	-73 51	171 50	C.	- 35 58	E. by s. ¼ s.		- 31 56	- 67 44			
	-73 52	170 40	P.	44 12	N.E. ½ E.		- 24 30	- 68 42			
-73 44	171 03	CR.	- 40 41	N.E. by N.	- 17 23	- 58 04					

A light card of CURRIER'S, marked P, was now used. Index error ascertained at Hobarton, June 1841.

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Jan. 22.	-73 46	171 25	CR.	- 42 16	N.E. 1/2 N.	-86 50	-24 30	- 66 46	- 66 44	+ 1 03	- 65 41
	-73 46	171 25	CR.	- 43 41	N.E. 1/2 N.		-24 30	- 68 11			
	-73 46	171 25	CR.	- 36 51	E.N.E.	-29 58	- 66 49				
	-73 46	171 25	CR.	- 36 16	E.N.E.	-29 58	- 66 14				
	-73 46	171 25	CR.	- 36 32	E. by N.	-32 03	- 68 35				
	-73 46	171 25	CR.	- 36 26	E. by N.	-32 03	- 68 29				
	-73 46	171 35	CR.	- 36 14	E.	-31 04	- 67 18				
	-73 46	171 35	CR.	- 36 12	E.	-31 04	- 67 16				
	-73 46	171 35	CR.	- 36 50	E.	-31 04	- 67 54				
	-73 46	171 35	CR.	- 35 47	E. by S.	-30 36	- 66 23				
	-73 59	171 40	C.	- 62 48	S.	0 0	- 62 48				
	-73 59	171 40	C.	- 63 52	S.	0 0	- 63 52				
	-74 03	171 40	C.	- 62 41	S.	0 0	- 62 41				
	-74 03	171 40	C.	- 63 47	S.	0 0	- 63 47				
-74 04	173 09	C.	- 40 33	E. by S.	-27 31	- 68 04					
-74 04	172 43	C.	- 40 47	E. by S.	-27 31	- 68 18					
-74 04	172 43	CR.	- 38 47	E. by S.	-27 31	- 66 18					
23.	-73 55	172 46	CR.	- 62 02	S.	0 0	- 62 02	- 65 15	+ 1 03	- 64 12	
	-73 59	171 32	CR.	- 38 22	E. by S.	-27 31	- 65 33				
25.	-74 24	168 28	C.	- 77 13	S.S.W.	+13 46	- 63 27	- 69 43	+ 1 03	- 68 40	
	-74 24	168 28	C.	- 81 13	S.S.W.	+13 46	- 67 27				
	-74 24	168 28	CR.	- 80 24	S.S.W.	+13 46	- 66 38				
	-74 28	168 46	CR.	- 39 28	E.S.E.	-34 13	- 73 41				
	-74 28	168 46	CR.	- 38 39	E.S.E.	-34 13	- 72 52				
	-74 28	168 46	CR.	- 39 57	E.S.E.	-34 13	- 74 10				
-74 50	168 45	C.	- 43 23	E. by S.	-46 49	- 90 12					
-75 37	168 28	C.	-102 27	S. by W.	- 8 23	- 94 04					
26.	-74 45	168 48	CR.	- 33 53	E. 1/2 S.	-47 08	- 81 01	- 91 47	+ 1 03	- 90 44	
27.	-75 40	168 28	C.	- 53 33	E.S.E.	-36 33	- 90 06				
-75 40	168 28	C.	- 56 14	E.S.E.	-36 33	- 92 47					
-75 40	168 28	C.	- 60 19	E.S.E.	-36 33	- 96 52					
-75 40	168 28	CR.	- 55 50	E.S.E.	-36 33	- 92 23					
-75 40	168 28	CR.	- 56 52	E.S.E.	-36 33	- 93 25					
-75 40	168 28	CR.	- 58 39	E.S.E.	-36 33	- 95 12					
-75 58	168 50	C.	- 72 06	S.E. 1/2 E.	-28 16	-100 22					
-75 58	168 50	C.	- 73 11	S.E. 1/2 E.	-28 16	-101 27					
28.	-76 47	169 26	C.	- 72 17	E. 3/4 S.	-36 36	-108 53				-108 08
-76 47	169 26	C.	- 70 45	E. by S.	-36 38	-107 23					
-77 17	171 38	C.	- 81 31	E. 1/2 S.	-34 42	-116 13					
-77 22	172 00	C.	- 80 29	E. 1/2 S.	-34 42	-115 01					
-77 30	172 20	C.	-119 58	N. 3/4 W.	+ 4 46	-115 12					
-77 17	172 20	C.	-116 46	N. 1/4 W.	+ 1 35	-115 11					
29.	-77 47	176 23	P.	- 98 39	N. by E.	- 6 21	-105 00	-103 12	+ 1 03	-102 09	
-77 47	176 23	P.	- 94 04	N. by E.	- 6 21	-100 25					
-77 47	176 14	CR.	-100 48	N.	0 0	-100 48					
-77 46	176 38	C.	-123 50	N.W. by N.	+18 23	-105 27					
-77 46	176 00	C.	-110 43	N. by W.	+ 6 21	-104 22					
31.	-77 06	187 30	CR.	- 65 19	N.E.	-17 26	- 82 45	- 86 12	+ 1 03	- 85 09	
-77 06	187 42	C.	- 64 40	N.E.	-17 26	- 82 06					
Feb. 1.	-77 03	189 03	C.	- 76 06	S.E. by S.	-14 14	- 90 20				
-77 03	189 03	C.	- 74 36	S.E. by S.	-14 14	- 88 50					
-77 03	189 03	C.	- 77 11	S.S.E.	-19 48	- 86 59					
2.	-77 45	187 08	C.	- 74 47	S. 62° E.	-21 00	- 95 47	- 96 24	+ 1 03	- 95 21	
-77 45	187 08	C.	- 75 23	S.E. by E.	-20 29	- 95 52					
-77 45	187 08	C.	- 76 56	S.E. by E.	-20 29	- 97 25					
-77 45	187 08	C.	- 77 48	S. 50° E.	-18 56	- 96 44					

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Feb. 2.	-77 41	187 02	P.	- 75 39	E. by S. $\frac{1}{2}$ S.	-85 50	-23 22	- 99 01	+1 03	- 95 21	
	-77 41	187 02	P.	- 73 43	E. by S. $\frac{1}{2}$ S.		-23 22	- 97 05			
	-77 41	187 02	P.	- 74 56	S.E. $\frac{1}{2}$ E.		-18 56	- 93 52			
	-77 43	187 01	C.	- 74 57	S.E. by E.		-20 29	- 95 26			
	-77 45	189 00	C.	-115 08	N. 74° W.		+23 07	- 92 01			
	-77 45	189 00	C.	-118 10	N. 80° W.		+24 00	- 94 10			
	-77 45	189 00	C.	- 77 37	N. 56° E.		-19 50	- 97 27			
	-77 45	189 00	C.	- 76 48	S. 56° E.		-20 29	- 97 17			
	-77 45	189 00	C.	- 75 16	E.S.E.		-22 41	- 97 57			
	-77 45	189 00	C.	- 74 39	E.S.E.		-22 41	- 97 20			
	-77 58	186 50	C.	- 77 31	S. 83° E.	-85 50	-25 15	-102 46	+1 03	- 94 59	
	-77 58	186 50	C.	- 76 06	S. 75° E.		-21 30	- 97 36			
	-77 58	186 50	CR.	- 73 42	E. by S.		-25 04	- 98 46			
	-77 22	185 00	C.	-119 49	S. 74° W.		+21 49	- 98 00			
3.	-77 22	185 00	C.	-117 43	S. 67° W.	-86 00	+23 39	- 94 04	+1 03	- 97 11	
	-77 22	185 00	C.	-117 32	S. 10° E.		+ 4 31	- 82 03			
4.	-76 56	192 19	C.	- 59 49	N.E. by E. $\frac{1}{2}$ E.	-85 40	-20 10	- 79 59	+1 03	- 83 03	
	-76 56	192 19	CR.	- 62 37	E.N.E.		-21 18	- 83 55			
	-77 04	192 02	C.	- 62 30	E. by N.	-85 40	-22 48	- 85 18	+1 03	- 83 03	
	-77 04	192 02	C.	- 63 34	E. by N. $\frac{3}{4}$ N.		-21 40	- 85 14			
	-77 04	192 02	CR.	- 61 20	E.N.E.		-21 18	- 82 38			
	-77 09	192 30	C.	- 96 17	S.S.W. $\frac{1}{2}$ W.		+11 12	- 85 05			
	-77 09	192 30	C.	- 88 25	S. by W.		+ 4 31	- 83 54			
	-77 09	192 30	C.	- 83 24	S. $\frac{1}{4}$ E.		- 1 05	- 84 29			
	-77 09	192 30	C.	- 65 46	N.E. by E. $\frac{1}{2}$ E.		-20 10	- 85 56			
	-77 12	192 30	P.	- 62 30	E. $\frac{1}{2}$ N.		-23 06	- 85 36			
	-77 15	192 40	P.	- 64 04	E. $\frac{3}{4}$ N.		-22 57	- 87 01			
	-77 20	192 30	CR.	- 93 11	S.S.W.		+ 9 03	- 82 08			
6.	-76 57	188 24	C.	- 88 27	S. $\frac{3}{4}$ W.	-86 00	+ 3 42	- 84 45	+1 03	- 83 24	
	-76 57	188 24	C.	- 86 19	S. $\frac{1}{2}$ W.		+ 2 28	- 83 51			
	-76 57	188 24	C.	- 61 44	E.N.E.		-23 10	- 84 54			
	-76 57	188 24	C.	- 62 49	E. by N. $\frac{1}{2}$ N.		-24 00	- 86 49			
	-76 57	188 24	C.	- 82 24	S. $\frac{3}{4}$ E.		- 3 42	- 86 06			
	-76 57	188 24	C.	- 93 19	S. by W. $\frac{3}{4}$ W.		+ 8 35	- 84 44			
	-76 57	188 24	P.	- 87 16	S. $\frac{1}{2}$ W.		+ 2 28	- 84 48			
	-76 57	189 00	CR.	- 84 11	S.		0 0	- 84 11			
	-76 59	188 45	CR.	- 87 13	S. by W. $\frac{1}{2}$ W.		+ 7 22	- 79 51			
	-76 56	186 21	C.	- 95 43	S. by W. $\frac{1}{2}$ W.		+ 7 22	- 88 21			
7.	-76 56	186 21	C.	- 61 53	E.	-86 00	-25 25	- 87 18	+1 03	- 89 37	
	-76 56	186 21	C.	- 63 01	E.		-25 25	- 88 26			
	-76 56	186 21	C.	- 63 08	E. $\frac{1}{4}$ N.		-25 06	- 88 14			
	-77 10	187 10	CR.	- 92 37	S. by W. $\frac{3}{4}$ W.		+ 8 35	- 84 02			
	-77 07	186 50	C.	- 72 58	S.E. by E. $\frac{1}{2}$ E.		-22 30	- 95 28			
	-77 07	186 50	C.	- 70 33	E.S.E.		-23 39	- 94 12			
	-77 07	186 50	C.	- 77 19	S.E. $\frac{3}{4}$ S.		-15 12	- 92 31			
	-77 07	186 50	C.	- 75 44	S.E.		-18 07	- 93 51			
	-77 07	186 50	CR.	- 76 11	S.E.		-18 07	- 94 18			
	-77 30	186 20	C.	- 65 18	E. $\frac{1}{2}$ S.		-25 15	- 90 33			
8.	-77 32	186 30	C.	- 69 25	E. $\frac{1}{4}$ N.	-86 00	-25 16	- 94 41	+1 03	- 93 24	
	-77 32	186 30	C.	- 69 20	E. $\frac{1}{2}$ N.		-25 07	- 94 27			
	-77 32	186 30	C.	- 69 39	E. $\frac{1}{2}$ N.		-25 07	- 94 46			
	-77 32	186 30	C.	- 70 52	E. by N. $\frac{3}{4}$ N.		-23 35	- 94 27			
	-77 31	186 17	CR.	- 72 06	S.E. by E. $\frac{3}{4}$ E.		-23 04	- 95 10			
	-77 37	186 30	CR.	- 68 35	E.		-25 25	- 94 00			
	-77 46	187 22	P.	- 72 52	E.N.E.		-23 10	- 96 02			
	-77 52	187 40	CR.	- 74 04	N.E. by E. $\frac{1}{2}$ E.		-21 56	- 96 00			

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Feb. 9.	-77 54	190 50	C.	-108 41	s.w. by s.	-86 00	+14 14	-94 27	+1 03	-94 42	
	-77 54	190 50	C.	-106 37	s.w. by s.		+14 14	-92 23			
	-77 54	190 50	CR.	-107 42	s.s.w. $\frac{1}{2}$ w.		+12 01	-95 41			
	-77 54	190 50	CR.	-110 45	s.w. by s.		+14 14	-96 31			
	-77 53	189 25	P.	-110 56	s.s.w. $\frac{1}{2}$ w.		+12 01	-98 55			
10.	-77 42	188 00	CR.	-114 10	s.w. $\frac{3}{4}$ w.	-87 00	+15 12	-98 58	+1 03	-88 55	
	-77 43	187 07	P.	-111 30	s.w.		+18 07	-93 23			
14.	-76 26	177 19	C.	-101 52	s.s.w.	-87 00	+13 01	-88 51	+1 03	-88 55	
	-76 25	177 50	CR.	-104 06	s.s.w.		+13 01	-91 05			
15.	-76 31	168 30	C.	-82 26	s.s.e. $\frac{3}{4}$ E.	-87 40	-22 47	-105 13	+1 03	-111 44	
16.	-76 30	166 15	C.	-67 30	s.e.		-32 02	-99 32			
	-76 30	166 15	C.	-65 14	e. by s.	-46 49	-112 03	-112 47	+1 03	-111 44	
-76 30	166 15	C.	-70 38	e. by s.	-46 49	-117 27					
	-76 30	166 15	C.	-74 30	e. $\frac{1}{2}$ N.	-87 40	-46 47	-111 17	+1 03	-111 44	
	-76 30	166 15	C.	-82 25	N.E. by E.		-37 36	-120 01			
	-76 30	166 15	P.	-73 22	e. $\frac{1}{2}$ N.	-87 40	-46 47	-120 09	+1 03	-111 44	
	-76 30	166 15	CR.	-66 43	E. by s. $\frac{3}{4}$ S.		-44 28	-111 11			
	-76 39	166 20	C.	-72 58	E. by s. $\frac{1}{2}$ S.	-87 40	-45 14	-118 12	+1 03	-100 14	
	-76 05	166 30	C.	-144 55	w. by N. $\frac{1}{2}$ N.		+45 20	-99 35			
	-76 05	166 30	C.	-131 51	N.W.	-87 40	+31 21	-100 30	+1 03	-100 14	
	-76 00	167 00	C.	-140 50	N.W. by w.		+37 36	-103 14			
	-76 05	165 49	CR.	-51 37	E.	-87 40	-47 27	-99 04	+1 03	-89 32	
	-76 05	165 49	C.	-56 46	E. $\frac{1}{4}$ S.		-47 17	-104 03			
	-76 00	167 00	C.	-129 44	W.N.W.	-87 40	+42 44	-87 00	+1 03	-89 32	
	-75 12	168 30	C.	-100 16	S. $\frac{3}{4}$ W.		+6 05	-94 11			
	-74 51	168 10	C.	-110 40	s.w.	-88 00	+38 02	-72 38	+1 03	-70 52	
	-74 51	168 10	C.	-109 33	s.w.		+38 02	-71 31			
	-74 51	168 10	C.	-110 11	s.w.	-88 00	+38 02	-72 09	+1 03	-70 52	
	-74 51	168 10	CR.	-109 24	s.w.		+38 02	-71 22			
20.	-72 22	171 11	CR.	-72 08	w. by N.	-86 20	+27 13	-44 55	+1 03	-37 41	
22.	-70 22	170 00	C.	-19 00	E.N.E.		-21 18	-40 18			
	-70 20	166 50	CR.	-21 22	E. by N.	-85 40	-22 48	-44 10	+1 03	-37 41	
	-70 22	167 12	C.	-45 30	S. $\frac{1}{4}$ E.		-1 07	-46 37			
	-70 32	167 34	CR.	-59 52	w. by N. $\frac{3}{4}$ N.	-85 40	+21 40	-38 12	+1 03	-37 41	
	-70 32	167 34	CR.	-57 07	N.W. $\frac{1}{2}$ W.		+16 48	-40 19			
	-70 09	167 20	C.	-48 07	N.W. $\frac{3}{4}$ N.	-85 40	+13 34	-34 33	+1 03	-36 06	
	-70 09	167 20	C.	-46 51	N.W.		+16 03	-30 48			
	-70 03	167 30	C.	-51 55	N.W. $\frac{1}{2}$ W.	-85 30	+17 32	-34 23	+1 03	-36 06	
	-70 03	167 30	C.	-50 19	N.W. by w.		+19 01	-31 18			
	-70 03	167 30	C.	-46 14	s. by w. $\frac{1}{2}$ W.	-85 30	+5 38	-40 36	+1 03	-36 06	
	-69 51	167 50	C.	-53 54	w. by s.		+22 06	-31 48			
	-69 51	167 50	C.	-53 23	w. by s. $\frac{1}{2}$ S.	-85 30	+21 30	-31 53	+1 03	-36 06	
	-68 48	167 42	CR.	-55 05	w. by s.		+22 06	-32 59			
	-68 48	167 42	CR.	-51 31	w. by s. $\frac{1}{2}$ S.	-85 30	+21 48	-29 43	+1 03	-36 06	
	-69 26	167 40	CR.	-47 25	s. by w.		+4 20	-43 05			
28.	-69 55	167 30	CR.	-39 10	s. by E. $\frac{1}{2}$ E.	-84 00	-6 31	-45 41	+1 03	-27 06	
Mar. 1.	-69 01	168 00	CR.	-36 08	s.s.e.		-8 43	-44 51			
	2.	-68 10	167 37	C.	-45 52	w. by N. $\frac{1}{2}$ N.	-84 00	+15 28	-30 24	+1 03	-27 06
-68 10		167 37	C.	-45 17	N.W. by w. $\frac{1}{2}$ W.	+14 15		-31 02			
	-68 10	167 37	C.	-46 45	W.N.W.	-84 00	+14 56	-31 49	+1 03	-27 06	
	-68 19	167 50	CR.	-46 49	w. by N.		+16 01	-30 48			
5.	-65 32	167 20	C.	-28 22	s. by w. $\frac{1}{2}$ W.	-84 00	+4 53	-23 29	+1 03	-27 06	
	-65 32	167 20	C.	-26 58	s. by w.		+3 17	-23 41			
	-65 32	167 40	C.	-32 43	s. by w. $\frac{1}{2}$ W.	-84 00	+4 53	-27 50	+1 03	-27 06	
	-65 32	167 40	C.	-32 48	s.s.w.		+6 29	-26 19			

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's attraction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Mar. 6.	-65 50	164 40	C.	-37 12	s.s.w. $\frac{1}{2}$ w.	-83 45	+ 7 36	-29 36	+1 03	-26 56	
	-65 50	164 40	C.	-35 02	s.s.w.		+ 6 12	-28 50			
	-65 50	164 40	C.	-34 22	s.s.w.		+ 6 12	-28 10			
	-65 50	164 40	C.	-33 23	s. by w. $\frac{1}{2}$ w.		+ 4 40	-28 43			
	-65 50	164 40	C.	-38 53	s.w. by s.		+ 8 59	-29 54			
	-65 50	164 40	C.	-39 02	s.w. $\frac{1}{2}$ s.		+10 13	-29 08			
	-65 50	164 40	CR.	-38 29	s.w.		+11 27	-27 02			
	-65 47	164 30	C.	-40 08	w. $\frac{3}{4}$ N.		+15 23	-24 35			
	-65 50	164 37	CR.	-42 20	w. $\frac{1}{2}$ s.		+15 35	-26 45			
	7.	-65 34	162 08	C.	-29 08		N. by w. $\frac{1}{2}$ w.	-83 30			
-65 34		162 08	C.	-27 42	N. by w. $\frac{1}{2}$ w.	+ 4 08	-23 34				
-65 34		162 08	C.	-29 19	N.N.W.	+ 5 31	-23 48				
-65 34		162 08	C.	-36 28	N.W.	+10 19	-26 09				
-65 34		162 08	C.	-16 26	s.E. by E.	-12 58	-29 26				
8.	-65 34	162 08	CR.	-25 28	N. by w. $\frac{1}{2}$ w.	-83 00	+ 4 08	-26 08	+1 03	-26 58	
	-64 44	162 20	C.	-25 24	N. by E. $\frac{1}{2}$ E.		- 3 49	-29 13			
	-64 44	162 20	C.	-23 05	N.N.E.		- 5 07	-28 12			
	-64 44	162 20	C.	-20 49	N.N.E. $\frac{1}{2}$ E.		- 6 18	-27 07			
	-64 44	162 20	C.	-19 40	N.E. $\frac{1}{2}$ N.		- 8 31	-28 11			
9.	-64 44	162 20	CR.	-18 01	N.E. $\frac{1}{2}$ E.	-83 00	-10 32	-28 33	+1 03	-22 48	
	-64 20	164 34	C.	-30 53	s. by w.		+ 2 43	-28 10			
	-64 20	164 34	C.	-31 16	s. by w. $\frac{1}{4}$ w.		+ 3 25	-27 51			
	-64 23	164 15	C.	-33 23	s.s.w. $\frac{1}{2}$ w.		+ 6 48	-26 35			
	-64 23	164 15	C.	-32 17	s.s.w. $\frac{1}{4}$ w.		+ 6 10	-26 07			
11.	-64 22	164 30	CR.	-31 51	s. by w.	-83 00	+ 2 43	-29 08	+1 23	-22 19	
	-64 10	163 00	C.	-34 24	N.W. $\frac{1}{2}$ w.		+10 32	-23 52			
	-64 10	163 00	C.	-32 34	N.W. $\frac{1}{2}$ w.		+10 32	-22 02			
	-64 18	163 15	CR.	-33 14	N.W. by w.		+11 30	-21 44			
	-64 18	163 15	CR.	-32 42	N.W.		+ 9 34	-23 08			
	-64 00	163 00	C.	-33 44	N.N.W. $\frac{1}{2}$ w.		+ 6 17	-27 27			
	-64 00	163 00	C.	-35 55	s.w. $\frac{3}{4}$ s.		+ 9 06	-26 49			
	-64 00	163 00	C.	-35 23	s.w. $\frac{3}{4}$ s.		+ 9 06	-24 17			
	-64 04	162 40	C.	-36 53	s.w. by w.		+12 00	-24 53			
	-64 04	162 40	C.	-37 54	s.w. by w. $\frac{1}{2}$ w.		+12 34	-25 20			
12.	-64 04	162 40	C.	-38 41	w.s.w.	-83 00	+13 09	-25 32	+1 23	-26 49	
	-64 04	160 53	C.	-34 41	w. $\frac{1}{2}$ s.		+13 51	-20 50			
	-64 04	160 53	C.	-34 28	w. by s.		+13 48	-20 40			
	-64 07	161 20	C.	-29 30	s.s.w. $\frac{1}{2}$ w.		+ 6 48	-22 42			
	-64 07	161 20	C.	-37 55	s.w. by w.		+12 00	-25 55			
14.	-62 49	157 00	C.	-22 39	s.s.e.	-82 45	- 5 24	-28 03	+1 23	-18 31	
	-62 49	157 00	C.	-22 32	s.s.e.		- 5 24	-27 56			
	-62 49	157 00	C.	-21 53	s. by E. $\frac{1}{2}$ E.		- 4 00	-25 53			
	-62 49	157 00	C.	-22 42	s. by E. $\frac{3}{4}$ E.		- 4 42	-27 24			
	-62 49	157 00	CR.	-24 05	s.s.e.		- 5 24	-29 29			
18.	-62 55	157 07	CR.	-25 07	s.s.e.	-83 45	- 5 24	-30 31	+1 23	-18 09	
	-62 55	157 07	CR.	-22 42	s.s.e.		- 5 24	-28 06			
	-63 50	151 35	C.	-21 06	s. by w.		+ 3 06	-18 00			
	-63 50	151 35	C.	-17 35	s. $\frac{1}{2}$ E.		- 1 30	-18 05			
	-63 50	151 35	C.	-14 57	s. by E. $\frac{1}{2}$ E.		- 4 30	-19 27			
	-63 50	151 35	C.	-14 47	s.s.e.		- 6 12	-20 59			
	-63 50	151 35	C.	-17 05	s. by E. $\frac{1}{4}$ E.		- 3 50	-20 55			
	-63 50	151 35	C.	-21 27	s. $\frac{1}{2}$ w.		+ 1 30	-19 57			
	-63 50	151 35	C.	-29 36	s.w.		+11 27	-18 09			
	-63 50	151 35	C.	-22 16	s. $\frac{1}{2}$ w.		+ 1 30	-20 46			
-63 50	151 35	CR.	-19 32	s. $\frac{1}{2}$ E.	- 1 30	-21 02					
-63 50	151 35	CR.	-15 30	s.s.e.	- 6 12	-21 42					

Card R substituted.

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Mar. 19.	64 15	149 00	C.	24 28	s.w. $\frac{1}{2}$ s.	-84 15	+11 11	-13 17	+1 23	-13 59	
	64 15	149 00	C.	24 03	s.s.w. $\frac{3}{4}$ w.		+9 05	-14 58			
	64 15	149 00	C.	17 37	s.s.w.		+6 45	-10 52			
	64 15	149 00	C.	23 31	s.s.w. $\frac{1}{2}$ w.		+8 19	-15 12			
	64 15	149 00	CR.	28 00	s.w. by s.		+9 50	-18 10			
	64 15	149 00	CR.	25 51	s.w. by s.		+9 50	-16 01			
21.	64 27	148 12	C.	28 51	s.w. by s.	-84 00	+9 50	-19 01	+1 23	-3 29	
	64 05	140 00	C.	21 49	w. $\frac{1}{2}$ N.		+16 13	-5 36			
22.	64 05	140 00	C.	21 13	w. by N.	-84 00	+16 01	-5 12	+1 23	-3 29	
	63 10	139 30	C.	17 14	N.w. $\frac{1}{2}$ w.		+12 25	-4 49			
23.	63 10	139 30	C.	15 50	N.w. $\frac{1}{2}$ N.	-83 45	+10 02	-5 48	+1 23	+1 35	
	63 10	139 30	C.	18 22	N.w. $\frac{1}{4}$ w.		+11 51	-6 31			
	63 06	139 40	C.	16 01	N.w. by w.		+13 34	-2 27			
	63 06	139 40	C.	17 47	N.w. $\frac{1}{2}$ w.		+12 25	-5 22			
	63 06	139 40	C.	15 36	N.w. $\frac{1}{2}$ w.		+12 25	-3 11			
	62 25	136 30	C.	11 46	N.w. by N.		+18 24	-3 22			
25.	62 25	136 30	C.	12 04	N.w. $\frac{1}{4}$ w.	-83 10	+11 20	-0 44	+1 23	+8 15	
	62 05	136 00	C.	13 15	w. by N. $\frac{1}{4}$ N.		+15 02	+1 47			
	62 05	136 00	C.	14 54	w. by N.		+15 17	+0 23			
	62 05	136 00	C.	11 20	w.N.w.		+14 16	+2 56			
	60 23	131 38	C.	2 53	N.w. $\frac{1}{2}$ N.		+8 43	+5 50			
	60 23	131 38	C.	0 35	N.w. $\frac{1}{2}$ N.		+8 43	+8 08			
	60 23	131 38	C.	3 15	N.w. $\frac{1}{2}$ N.		+8 43	+5 28			
	60 23	131 38	C.	4 53	N.w. $\frac{1}{2}$ w.		+10 48	+5 55			
	60 23	131 38	C.	4 12	N.w.		+9 48	+5 36			
	60 23	131 38	C.	2 17	N.w. $\frac{1}{2}$ N.		+8 43	+6 26			
	60 23	131 38	C.	2 24	N.w. $\frac{1}{2}$ N.		+8 43	+6 19			
	60 23	131 38	C.	2 34	N.w. $\frac{1}{2}$ N.		+9 15	+6 41			
26.	60 33	131 37	CR.	0 41	N.w.	-83 00	+9 48	+9 07	+1 23	+10 23	
	60 33	131 37	CR.	1 58	N.w.		+9 48	+7 50			
	60 23	131 38	CR.	1 34	N.w.		+9 48	+8 14			
	60 20	131 30	C.	5 54	w. by N. $\frac{1}{2}$ N.		+13 06	+7 12			
	60 20	131 30	C.	8 02	N. $\frac{1}{2}$ w.		+1 15	+9 17			
	60 20	131 30	C.	3 25	N.w. by w. $\frac{1}{2}$ w.		+12 05	+8 40			
	60 20	131 30	C.	8 30	N. $\frac{3}{4}$ w.		+1 53	+10 23			
	60 20	131 30	C.	8 05	N. $\frac{3}{4}$ w.		+1 53	+9 58			
	60 20	131 30	C.	1 55	N.w. by w. $\frac{1}{4}$ w.		+11 48	+9 53			
	60 20	131 30	C.	12 22	N.N.E.		-5 07	+7 15			
	60 20	131 30	C.	19 22	N.E. by N.		-7 28	+11 54			
	60 20	131 30	C.	13 35	N.N.E.		-5 07	+8 28			
27.	60 20	131 30	C.	4 58	N.w. by w. $\frac{1}{2}$ w.	-82 45	+12 05	+7 07	+1 23	+10 07	
	59 24	129 46	C.	0 17	N.w. $\frac{1}{2}$ N.		+8 15	+7 58			
	59 12	129 40	C.	7 47	N. $\frac{3}{4}$ w.		+1 49	+9 36			
	59 12	129 40	C.	4 29	N. by w. $\frac{1}{4}$ w.		+3 03	+7 32			
	59 12	129 40	C.	2 34	N.N.W. $\frac{1}{4}$ w.		+5 32	+8 06			
	59 12	129 40	C.	1 08	N.N.W. $\frac{1}{4}$ w.		+6 41	+7 49			
28.	59 12	129 40	C.	5 05	N.N.W.	-81 45	+4 58	+10 03	+1 23	+8 37	
	58 00	129 45	C.	10 02	N.		0 0	+10 02			
	57 22	127 40	C.	4 55	w. by s. $\frac{3}{4}$ s.		+11 30	+6 35			
	57 22	127 40	C.	3 41	w. by s.		+11 48	+8 07			
	57 22	127 40	C.	2 00	w. $\frac{1}{2}$ s.		+11 49	+9 49			
	57 22	127 40	C.	14 24	E. by N. $\frac{3}{4}$ N.		-11 04	+3 20			
29.	57 22	127 40	CR.	2 19	w. $\frac{1}{2}$ N.	-81 45	+11 47	+9 28	+1 23	+8 37	
	57 22	127 40	CR.	0 44	w. $\frac{1}{2}$ N.		+11 47	+11 03			
	57 22	127 40	C.	12 27	N.E. $\frac{1}{2}$ E.		-8 58	+3 29			
	57 22	127 40	C.	14 56	N.E. $\frac{1}{2}$ E.		-8 58	+5 58			

Observations of Declination. (Continued.)

1841.	Position.		Observers.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.				
	Lat.	Long.													
Mar. 29.	-56 35	129 50	C.	+15 58	N.E. by E. $\frac{1}{2}$ E.	-81 15	-9 41	+6 17	+1 23	+5 21					
	-56 35	129 50	C.	+10 23	N.E. $\frac{1}{2}$ E.		-8 25	+1 58							
	-56 35	129 50	C.	+14 24	N.E.		-7 41	+6 43							
	-56 44	129 37	Cr.	+11 40	E. by N.		-11 01	+0 39							
	-56 47	129 30	Cr.	+11 35	N.E. by N.		-6 00	+5 35							
	-56 47	129 30	Cr.	+9 11	N.E. by N.		-6 00	+3 11							
	-56 30	130 10	C.	+8 56	N.E. E. $\frac{3}{4}$ E.		-5 31	+3 25							
	30.	-55 12	132 00	C.	+7 38		N.E. by E. $\frac{1}{2}$ E.	-80 20			-8 38	-1 00	+1 23	+0 45	
		-55 12	132 00	C.	+1 47		N.E.				-6 50	-5 03			
		-55 12	132 00	C.	+4 15		N.E. $\frac{1}{2}$ N.				-6 05	-1 50			
		-55 12	132 00	C.	+5 18		N.E. $\frac{1}{2}$ N.				-6 05	-0 47			
		-55 12	132 00	C.	+8 28		N.E.				-6 50	+1 38			
-55 12		132 00	C.	+2 52	N.E. by N.	-5 20	-2 28								
-55 12		132 00	Cr.	+7 20	N. by E. $\frac{3}{4}$ E.	-3 13	+4 07								
-55 04		132 10	C.	+2 37	N. $\frac{1}{2}$ E.	-0 50	+1 47								
-55 04		132 10	C.	+8 00	N.E. by E.	-8 24	-0 24								
-55 04		132 10	C.	+2 37	N.N.E. $\frac{1}{2}$ E.	-80 20	-4 40		-2 03	+1 23	+0 16				
-55 04		132 10	C.	-00 04	N. $\frac{3}{4}$ E.		-1 26		-1 22						
-55 04		132 10	C.	+3 45	N.E. $\frac{1}{4}$ E.		-7 18		-3 33						
-54 56	132 15	C.	+4 43	N.E. by N.	-5 32		-0 49								
-54 56	132 15	C.	+3 24	N.N.E. $\frac{3}{4}$ E.	-5 01		-1 37								
-54 56	132 15	C.	+0 32	N. by E. $\frac{5}{4}$ E.	-3 13		-2 41								
-54 56	132 15	C.	+2 57	N. $\frac{3}{4}$ E.	-1 26		+1 31								
-55 06	132 07	Cr.	+1 47	N.N.E.	-3 48		-2 01								
-55 01	132 15	Cr.	+2 46	N.E. $\frac{1}{2}$ N.	-6 05		-3 19								
-54 05	134 50	C.	+4 03	E. by N. $\frac{1}{2}$ N.	-8 33		-4 30								
-54 05	134 50	C.	+6 12	E.N.E.	-8 15		-2 03								
-54 05	134 50	C.	+2 07	E. by N. $\frac{1}{2}$ N.	-8 24		-6 17								
-54 05	134 50	C.	+2 25	E. $\frac{1}{2}$ N.	-9 01	-6 36									
-54 05	134 50	C.	+2 07	E. $\frac{3}{4}$ N.	-8 56	-6 49									
-54 05	134 50	C.	+6 00	E. $\frac{1}{2}$ N.	-79 15	-9 01	-3 01	+1 23	-3 44						
-54 06	134 31	Cr.	+5 19	E. by N.		-8 52	-3 33								
-54 06	134 31	Cr.	+2 53	E. by N.		-8 52	-5 59								
-54 06	134 31	Cr.	+4 27	E. by N.		-8 52	-4 25								
-54 06	134 39	Cr.	+1 34	E.		-9 10	-7 36								
-54 06	134 48	Cr.	+3 38	E.		-9 10	-5 32								
April 1.	-53 01	134 50	C.	-0 30		N.N.E. $\frac{3}{4}$ E.	-79 00			-4 18	-4 48	+1 23	-3 55		
	-53 01	134 50	C.	-0 46		N.E. $\frac{1}{2}$ E.				-6 33	-7 19				
	-52 54	135 10	C.	-0 44		N.N.E. $\frac{3}{4}$ E.				-4 18	-5 02				
	-52 54	135 10	C.	-1 52		N. by E. $\frac{1}{4}$ E.				-2 01	-3 53				
	-52 54	135 10	C.	-1 18		N. by E. $\frac{1}{2}$ E.				-2 25	-3 43				
	-52 54	135 10	C.	-2 56		N. by E. $\frac{1}{2}$ E.				-2 25	-5 21				
	-52 54	135 10	C.	-1 47	N.N.E.	-3 12		-4 59							
	-52 54	135 10	C.	-4 08	N.N.E.	-3 12		-7 20							
	2.	-51 16	136 49	Cr.	-5 35	N. by E. $\frac{5}{4}$ E.		-77 30	-2 23	-7 58	+1 23			-5 38	
		-51 16	136 49	C.	-4 12	N. by E. $\frac{1}{4}$ E.			-1 44	-5 56					
		-51 14	136 50	C.	-2 00	N.E.			-5 09	-7 09					
		5.	-44 53	143 00	Cr.	-7 44			N.E.	-73 00					-3 43
-44 53			143 00	C.	-7 22	N.E.	-3 43		-11 05						
-44 56			143 16	C.	-7 12	N.E. by E.	-4 26		-11 38						
-44 40			143 50	C.	-8 16	N.E.	-3 43		-11 59						
-44 40			143 50	C.	-7 21	N.E. $\frac{3}{4}$ E.	-4 00		-11 21						
-44 56			143 16	Cr.	-1 23	E.N.E.	-5 04		-6 27						
-44 50			143 20	Cr.	-2 22	S.E.	-4 24		-6 46						
-44 50			143 20	Cr.	-6 19	S.S.E. $\frac{1}{2}$ E.	-3 00		-9 19						
-44 05			145 30	C.	-7 16	N.E. $\frac{1}{2}$ E.	-4 04		-11 20						
-44 05	145 30		C.	-5 01	N.E. $\frac{1}{2}$ E.	-4 04	-9 09								
-44 05	145 30		C.	-5 57	N.E. $\frac{1}{4}$ E.	-3 53	-9 50								

General Table of the Declinations observed on board Her Majesty's Ships Erebus and Terror, between November 1840 and April 1841.

Lat.	Long.	Ship.	No. of observations.	Declination.	Lat.	Long.	Ship.	No. of observations.	Declination.
+ 15° to + 5°.					-50 32	166 12	Erebus.	6	-17 44
-60 20	131 30	Terror.	10	+10 23	-52 33	169 09	Erebus.	2	-17 52
-59 03	129 33	Terror.	7	+10 07	-63 50	151 35	Terror.	10	-18 31
-57 21	127 45	Erebus.	10	+ 8 47	-54 14	169 06	Erebus.	5	-18 44
-57 22	127 40	Terror.	8	+ 8 37	-63 50	151 48	Erebus.	6	-18 59
-58 54	129 38	Erebus.	11	+ 8 32	-63 52	151 51	Erebus.	6	-20 15
-60 20	131 21	Erebus.	8	+ 8 18	-59 32	170 05	Terror.	8	-20 20
-60 25	131 38	Terror.	11	+ 8 15	-59 32	170 05	Terror.	13	-20 56
-60 25	131 37	Erebus.	10	+ 8 09	-59 32	169 59	Erebus.	8	-21 28
-60 20	131 22	Erebus.	7	+ 7 38	-57 10	170 06	Erebus.	7	-21 58
-56 14	130 44	Erebus.	8	+ 5 46	-58 19	170 39	Terror.	12	-21 58
-56 39	129 45	Terror.	7	+ 5 21	-57 40	170 26	Erebus.	7	-21 59
+ 5° to - 5°.					-64 05	161 47	Terror.	7	-22 19
-62 13	136 12	Terror.	5	+ 1 35	-60 47	170 55	Erebus.	11	-22 32
-55 11	131 31	Erebus.	7	+ 1 34	-64 08	163 04	Terror.	7	-22 48
-55 04	132 44	Erebus.	9	+ 1 09	-60 13	170 25	Erebus.	10	-22 49
-55 12	132 00	Terror.	7	+ 0 45	-65 34	162 08	Terror.	6	-23 47
-55 13	131 15	Erebus.	7	+ 0 31	-60 18	170 12	Terror.	12	-23 48
-55 04	132 10	Terror.	5	+ 0 16	-64 05	161 13	Erebus.	9	-24 06
-54 59	132 13	Terror.	6	- 0 06	-63 10	156 25	Erebus.	9	-24 07
-62 06	136 07	Erebus.	6	- 0 27	- 25° to - 35°.				
-52 52	135 26	Erebus.	7	- 1 03	-65 06	172 20	Erebus.	8	-25 06
-62 15	136 23	Erebus.	7	- 1 13	-64 10	163 14	Erebus.	11	-25 18
-54 04	134 45	Erebus.	7	- 1 44	-64 18	172 31	Erebus.	9	-25 33
-54 04	134 30	Erebus.	6	- 1 50	-64 26	173 00	Terror.	9	-25 52
-63 22	139 41	Terror.	8	- 3 29	-64 52	162 42	Erebus.	9	-25 54
-54 05	134 44	Terror.	11	- 3 44	-64 40	172 44	Erebus.	8	-25 57
-52 56	135 05	Terror.	8	- 3 55	-65 42	172 13	Terror.	7	-26 17
-62 37	138 24	Erebus.	6	- 4 05	-62 50	157 01	Terror.	7	-26 49
-51 11	136 54	Erebus.	5	- 4 39	-65 50	164 39	Terror.	9	-26 56
- 5° to - 15°.					-64 33	163 23	Terror.	10	-26 58
-51 15	136 49	Terror.	3	- 5 38	-66 52	167 35	Terror.	8	-27 06
-63 13	140 00	Erebus.	12	- 5 58	-65 57	171 45	Erebus.	7	-27 11
-64 20	140 40	Erebus.	6	- 6 57	-66 27	169 44	Erebus.	8	-27 21
-44 37	143 56	Terror.	11	- 8 39	-65 27	172 29	Erebus.	11	-27 34
-44 18	145 04	Erebus.	9	- 8 46	-65 30	172 34	Erebus.	10	-28 08
-42 52	147 24	Erebus.	6	-10 24	-66 20	169 51	Erebus.	9	-28 21
-44 24	152 58	Terror.	2	-11 38	-65 43	165 10	Erebus.	13	-28 23
-65 04	142 47	Erebus.	2	-12 37	-65 31	173 05	Terror.	12	-29 17
-45 36	152 53	Erebus.	8	-13 09	-65 35	173 38	Terror.	12	-29 42
-46 08	154 15	Erebus.	8	-13 38	-67 16	174 41	Erebus.	16	-31 29
-46 13	154 26	Terror.	4	-13 47	-67 56	167 31	Erebus.	8	-32 35
-46 30	154 55	Erebus.	7	-13 58	-68 31	176 05	Erebus.	12	-33 52
-64 17	148 52	Terror.	7	-13 59	-68 00	175 05	Erebus.	13	-34 04
-49 18	160 18	Terror.	4	-14 44	-68 24	175 45	Terror.	10	-34 38
- 15° to - 25°.					-68 28	176 32	Erebus.	1	-34 39
-50 33	166 15	Terror.	42	-15 29	-68 55	176 20	Erebus.	5	-34 58
-50 54	166 35	Erebus.	7	-16 03	- 35° to - 45°.				
-52 22	169 38	Terror.	11	-17 08	-69 23	167 45	Terror.	7	-36 06
-49 47	161 00	Erebus.	8	-17 16	-68 59	167 46	Erebus.	12	-36 12
-64 17	149 03	Erebus.	5	-17 19	-70 27	167 57	Terror.	11	-37 41
					-69 33	167 31	Erebus.	11	-38 21
					-70 03	167 30	Erebus.	10	-39 21



## General Table of Declination. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Declination.	Lat.	Long.	Ship.	No. of observations.	Declination.
- 35° to - 45°.					- 85° to - 95°.				
-70 33	172 57	Erebus.	6	-39 35	-77 04	188 28	Terror.	5	- 85 09
-70 23	167 23	Erebus.	7	-39 45	-76 23	177 25	Erebus.	2	- 85 10
-71 00	172 25	Erebus.	9	-43 56	-77 12	187 02	Erebus.	10	- 87 29
-71 22	170 56	Erebus.	10	-44 01	-76 25	177 35	Terror.	2	- 88 55
-71 51	171 53	Erebus.	9	-44 24	-77 22	186 21	Erebus.	6	- 89 19
- 45° to - 55°.					- 85° to - 95°.				
-71 08	172 07	Terror.	10	-45 45	-75 36	167 45	Terror.	2	- 89 32
-71 52	171 19	Terror.	12	-46 40	-77 03	186 40	Terror.	10	- 89 37
-71 21	171 14	Terror.	8	-46 52	-77 28	186 33	Erebus.	6	- 90 21
-71 55	172 00	Erebus.	9	-48 12	-75 28	168 12	Terror.	9	- 90 44
-72 33	172 51	Terror.	8	-48 49	-77 09	188 22	Erebus.	9	- 91 07
-72 36	173 40	Erebus.	5	-50 31	-77 35	186 40	Erebus.	9	- 93 22
-72 16	174 09	Erebus.	6	-51 41	-77 36	186 41	Terror.	9	- 93 24
-72 36	173 46	Erebus.	8	-51 54	-77 44	188 00	Erebus.	8	- 93 41
-72 40	175 17	Terror.	11	-52 35	-77 54	188 27	Erebus.	8	- 93 41
-73 01	175 55	Erebus.	12	-52 41	-77 51	191 01	Erebus.	5	- 93 43
-72 34	172 43	Terror.	8	-54 34	-77 46	186 53	Erebus.	8	- 94 14
- 55° to - 65°.					- 85° to - 95°.				
-73 57	171 23	Erebus.	12	-63 38	-75 52	167 00	Erebus.	8	- 94 27
-73 53	171 37	Terror.	8	-64 12	-77 51	189 42	Terror.	7	- 94 42
-74 01	171 42	Erebus.	10	-64 25	-77 45	189 00	Terror.	6	- 94 59
- 65° to - 75°.					- 95° to - 105°.				
-74 01	172 35	Terror.	5	-65 04	-77 43	187 04	Terror.	8	- 95 21
-73 47	171 23	Terror.	10	-65 41	-77 49	187 26	Erebus.	6	- 95 52
-74 26	168 37	Terror.	6	-68 40	-77 51	187 38	Erebus.	6	- 96 00
-74 39	169 00	Erebus.	7	-69 47	-77 51	186 38	Erebus.	10	- 96 14
-74 51	168 10	Terror.	4	-70 52	-77 47	180 34	Erebus.	1	- 96 17
-74 46	168 42	Erebus.	10	-71 08	-77 44	186 06	Terror.	5	- 97 11
-74 46	167 53	Erebus.	2	-74 48	-76 07	168 45	Erebus.	4	- 98 45
- 75° to - 85°.					- 95° to - 105°.				
-76 40	188 40	Erebus.	5	-77 53	-75 58	168 50	Terror.	2	- 99 41
-76 57	186 38	Erebus.	9	-81 33	-76 10	166 02	Erebus.	4	- 99 41
-77 18	192 38	Erebus.	13	-81 50	-76 04	166 19	Terror.	5	-100 14
-77 08	189 02	Erebus.	6	-82 09	-77 47	176 19	Terror.	5	-102 09
-77 11	192 58	Erebus.	6	-82 26	-77 41	175 57	Erebus.	7	-104 25
-77 22	188 43	Erebus.	12	-82 29	- 105° to - 115°.				
-77 07	192 22	Terror.	13	-83 03	-77 50	178 00	Erebus.	4	-105 21
-76 57	188 30	Terror.	9	-83 24	-76 22	165 44	Erebus.	6	-106 13
-77 17	191 35	Erebus.	6	-83 56	-76 47	169 26	Terror.	2	-107 05
-75 39	168 33	Erebus.	9	-84 58	-76 32	166 30	Terror.	9	-111 44
					-76 36	166 18	Erebus.	13	-113 23
					-76 33	164 45	Erebus.	8	-113 41
					-77 22	172 04	Terror.	4	-114 21

Total number of observations 1368. No observation has been omitted or its result rejected. The scale of the declination chart has not permitted the insertion of all the results comprised in this table, and a few of those of the Terror have consequently been omitted in the very high latitudes where the figures are most crowded. The next number of these contributions, embracing the observations of the succeeding voyage, will contain a declination chart of the high latitudes on a more extended scale, in which all the results of both voyages will be inserted.

General Table of the Inclinations observed in Her Majesty's Ship Erebus, from  
June 1840 to April 1841.

Lat.	Long.	No. of observations.	Inclination.	Lat.	Long.	No. of observations.	Inclination.
-48 41	68 54	9	-70 00 <i>a</i>	-68 17	175 00	5	-83 12
-48 29	76 55	2	-70 55	-68 32	175 49	6	-83 28
-48 17	80 15	2	-71 50	-68 28	176 31	5	-83 17
-47 55	83 00	2	-72 34	-68 28	176 32	5	-83 35 <i>e</i>
-47 46	86 18	2	-73 33	-68 53	176 23	5	-83 40
-47 12	89 45	2	-73 35	-70 23	174 50	4	-85 00
-47 03	93 00	2	-74 37	-71 15	171 15	4	-85 50
-47 39	102 42	2	-74 28	-71 24	170 44	4	-85 53
-47 35	106 26	2	-74 31	-71 47	170 52	3	-86 10
-47 45	110 39	2	-75 08	-72 07	172 19	4	-86 13
-47 34	114 15	2	-75 26	-71 52	172 08	2	-85 53
-47 41	121 30	2	-76 04	-71 55	171 51	4	-85 55
-47 34	124 43	2	-76 40	-72 12	172 13	4	-86 41
-46 44	128 26	2	-75 41	-72 09	173 35	3	-86 03
-46 13	132 00	2	-75 17	-72 57	176 06	5	-86 11
-45 59	135 38	2	-73 48	-72 35	173 34	4	-86 36
-45 17	139 19	2	-73 23	-72 31	173 39	4	-86 51
-44 24	141 39	2	-72 37	-73 48	171 47	7	-87 04
-44 16	142 38	2	-73 03	-74 06	170 40	8	-87 12
-42 52	147 24		-70 38 <i>b</i>	-73 56	171 35	8	-87 11
-44 16	149 29	3	-70 41	-74 33	173 23	7	-87 29
-45 13	151 57	3	-71 49	-74 43	169 48	5	-87 25
-45 33	152 45	3	-71 37	-74 45	168 23	4	-88 18
-46 18	154 30	3	-72 04	-74 55	169 01	3	-88 21
-47 46	157 40	3	-73 14	-75 22	168 48	4	-88 36
-49 20	160 13	3	-74 15	-76 06	168 11	4	-88 27
-50 28	164 09	3	-74 23	-77 07	169 56	2	-88 01
-50 33	166 19		-73 10 <i>c</i>	-77 47	175 43	4	-86 48
-52 34	169 10	7	-73 52 <i>d</i>	-77 41	180 54	2	-85 54
-54 06	169 09	4	-74 46	-77 06	189 08	5	-85 56
-55 50	170 06	3	-76 16	-77 05	188 36	5	-86 12
-57 15	170 40	3	-77 43	-77 09	188 15	4	-86 23
-57 54	170 25	3	-77 51	-77 49	186 30	5	-86 10
-58 57	170 57	4	-78 04	-77 17	185 26	4	-86 49
-59 43	169 39	6	-78 34	-77 00	192 18	5	-85 36
-60 19	170 20	7	-78 53	-77 07	192 26	4	-85 26
-60 46	170 44	4	-79 06	-77 24	192 56	4	-85 45
-61 34	170 40	3	-79 30	-77 10	192 48	5	-86 06
-62 06	172 51	4	-79 41	-77 09	188 43	6	-85 54
-62 40	173 40	1	-79 58	-76 59	186 39	5	-86 23
-62 44	174 36	5	-80 09	-77 43	187 10	5	-85 51
-64 00	172 44	4	-81 03	-77 55	189 04	2	-85 49
-64 06	172 38	5	-81 03	-77 38	187 00	5	-86 19
-64 31	172 57	6	-81 11	-76 22	188 05	4	-86 07
-65 58	172 47	4	-82 20	-76 50	183 26	3	-86 23
-66 17	170 57	4	-82 25	-76 17	175 37	6	-87 15
-66 30	169 13	4	-82 40	-76 14	172 35	1	-87 36
-66 32	169 45	4	-82 31	-76 06	168 07	7	-88 21
-66 23	170 12	4	-82 53	-76 20	165 32	4	-88 35
-65 39	170 44	4	-81 51	-76 36	164 38	5	-88 19
-65 22	172 40	4	-81 43	-75 21	168 06	6	-87 52
-66 55	174 31	3	-82 13	-72 13	171 04	4	-86 23
-67 27	174 51	4	-82 58	-70 55	168 43	3	-85 53

*a* On shore at Kerguelen Island. *b* On shore at Van Diemen Island. *c* On shore at Auckland Island.*d*. On shore at Campbell Island. *e* On Ice.

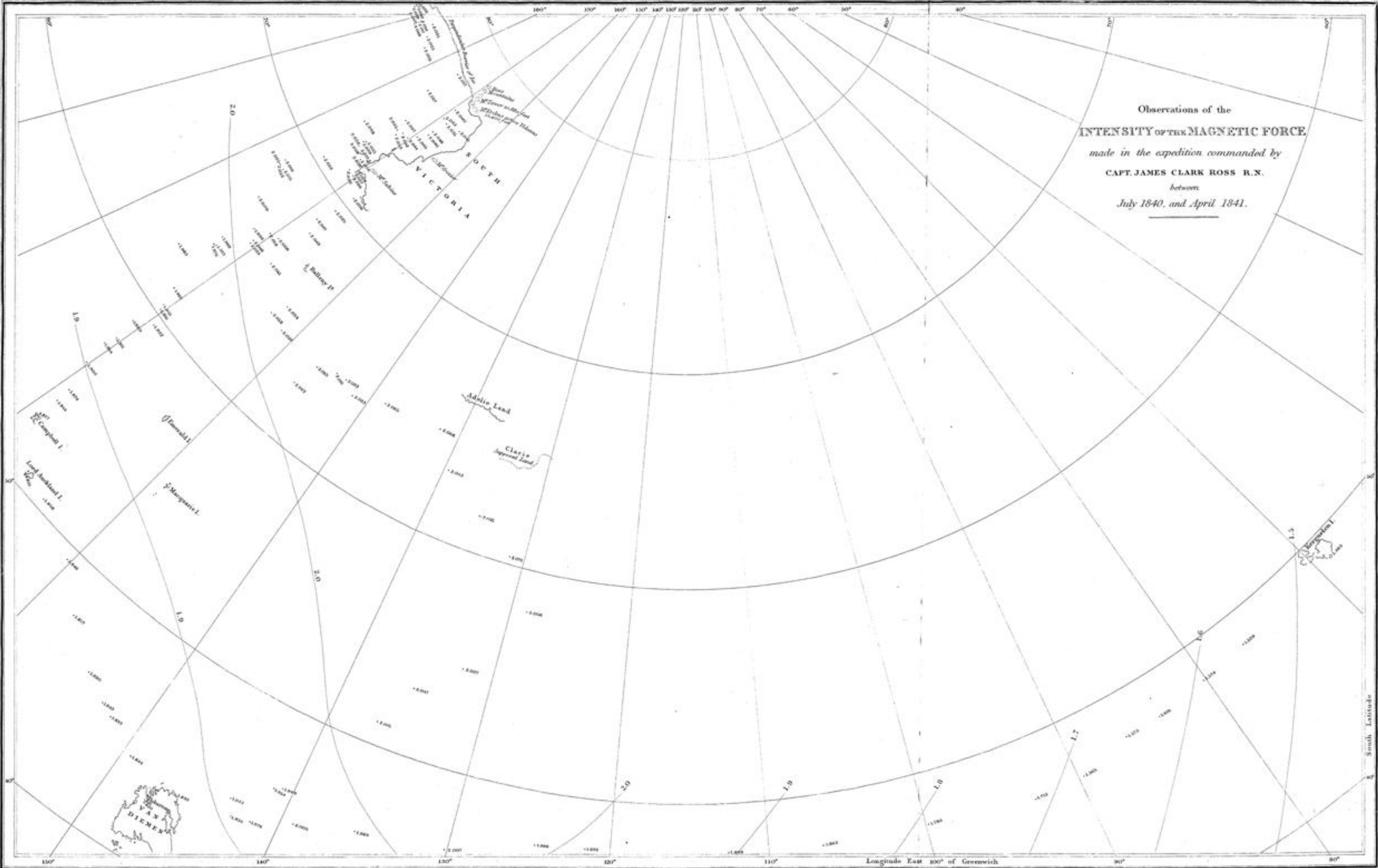
General Table of Inclination. (Continued.)

Lat.	Long.	No. of observations.	Inclination.	Lat.	Long.	No. of observations.	Inclination.
-70 41	167 20	4	-85 51	-65 14	144 37	3	-85 05
-70 17	167 24	6	-86 19	-65 11	143 52	3	-85 10
-70 14	167 16	3	-86 06	-65 09	143 07	6	-85 16
-69 57	167 52	2	-85 41	-64 20	140 40	5	-84 36
-69 24	167 55	5	-85 28	-63 09	139 28	7	-84 46
-69 46	167 43	5	-85 54	-62 18	136 40	6	-84 20
-69 06	167 43	5	-85 26	-61 18	134 02	5	-83 55
-68 28	168 10	5	-85 07	-60 20	131 21	5	-83 31
-67 47	167 22	5	-84 28	-59 25	130 14	5	-82 52
-65 49	166 12	7	-83 35	-58 06	128 43	1	-82 09
-65 53	162 14	3	-83 51	-57 22	127 37	2	-81 43
-64 41	162 34	4	-82 55	-56 28	129 57	1	-80 43
-64 20	163 29	4	-82 54	-55 02	131 48	5	-80 15
-63 52	160 55	5	-83 32	-54 55	132 50	6	-80 07
-62 41	156 59	5	-82 33	-54 02	134 59	8	-79 39
-63 50	156 06	4	-83 54	-53 13	135 18	5	-79 09
-64 12	154 47	3	-84 06	-51 16	136 50	4	-77 59
-64 13	154 03	3	-84 06	-48 48	138 34	4	-76 54
-64 20	153 02	5	-84 14	-46 55	139 55	3	-75 42
-63 54	151 56	3	-84 06	-46 25	140 55	7	-75 12
-64 18	149 09	3	-84 48	-44 57	144 18	8	-73 54
-64 33	148 03	4	-85 03	-43 50	146 00	5	-72 15

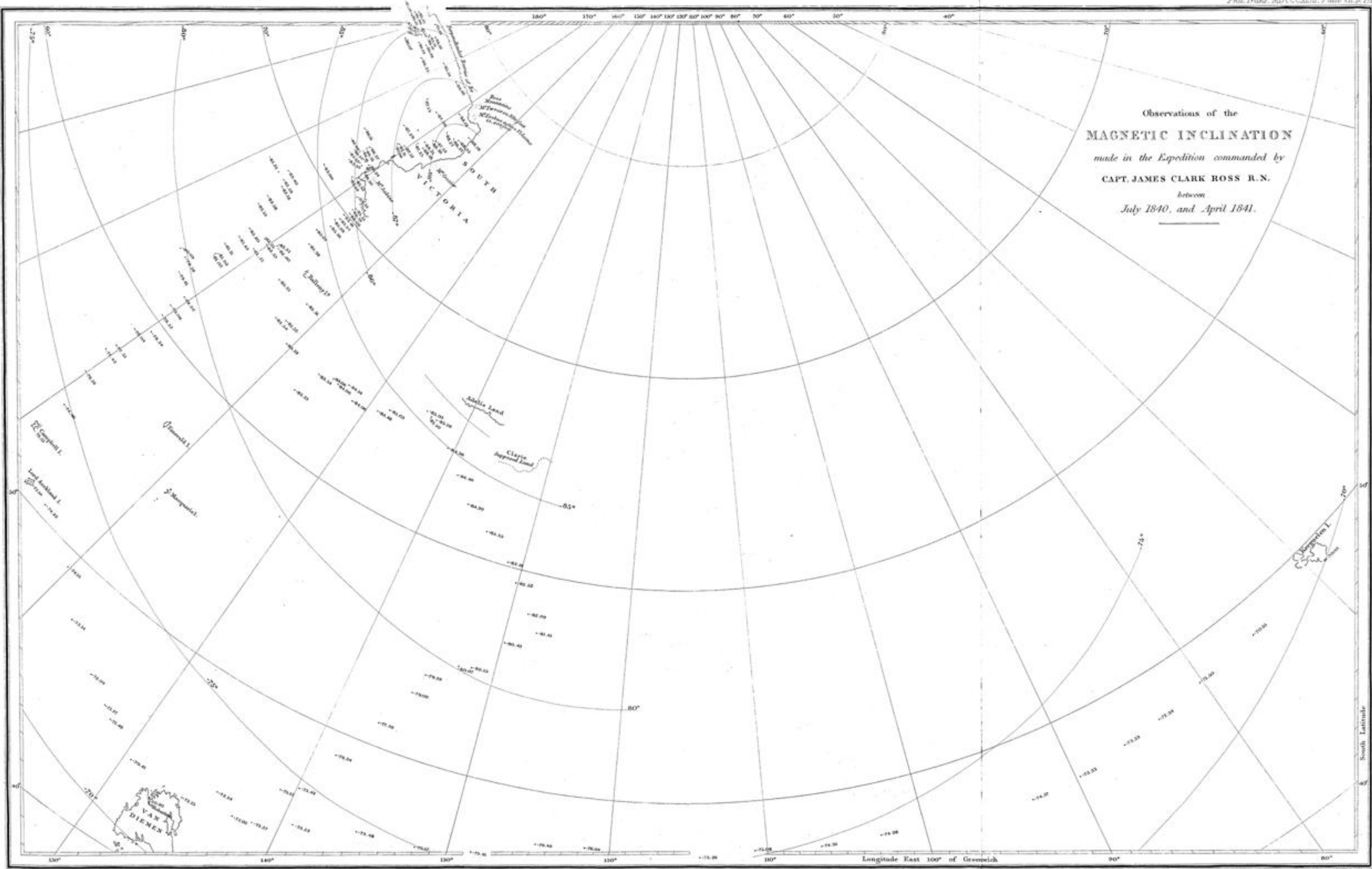
General Table of the Intensity of the Magnetic Force from the observations made on board Her Majesty's Ship Erebus, between July 1840 and April 1841.

Latitude.	Longitude.	Intensity.	Latitude.	Longitude.	Intensity.	Latitude.	Longitude.	Intensity.
		London = 1·372.			London = 1·372.			London = 1·372.
-48 41	68 54	1·465	-60 31	170 32	1·951	-77 00	192 18	2·039
-48 29	76 55	1·539	-61 17	171 14	1·960	-77 10	192 48	2·036
-48 17	80 15	1·574	-62 40	174 40	1·983	-77 14	192 02	2·020
-47 55	83 51	1·601	-64 00	172 44	1·976	-77 09	188 50	2·036
-47 46	86 18	1·575	-64 06	172 38	1·973	-76 58	188 40	2·035
-47 12	89 45	1·565	-64 31	172 55	1·988	-77 43	187 11	2·035
-47 03	93 00	1·712	-65 46	171 40	1·996	-76 55	188 49	2·048
-47 26	99 54	1·783	-66 31	169 20	2·008	-76 50	183 26	2·035
-47 35	106 26	1·863	-66 23	170 12	2·018	-76 16	175 50	2·017
-47 40	112 27	1·898	-65 39	170 44	2·046	-76 03	169 30	2·033
-47 41	121 30	1·992	-65 22	170 40	2·025	-76 20	165 32	2·041
-47 34	124 43	1·996	-66 55	174 31	2·009	-75 03	168 44	2·040
-46 28	130 13	2·007	-68 30	175 40	2·011	-71 17	170 43	2·037
-45 59	135 38	1·989	-68 28	176 31	2·032	-71 04	170 07	2·026
-45 17	139 19	2·005	-68 28	176 32	2·025	-70 25	167 27	2·036
-44 24	141 39	1·976	-68 48	176 45	2·016	-69 24	167 49	2·025
-44 16	142 38	1·934	-70 23	174 50	2·033	-68 28	168 10	2·047
-45 02	143 10	1·923	-71 15	171 15	2·030	-67 52	167 28	2·043
-46 22	141 06	1·954	-71 24	170 44	2·029	-65 31	167 42	2·041
-46 29	140 40	1·949	-71 47	170 52	2·056	-64 58	162 27	2·024
-43 41	146 03	1·892	-72 07	172 19	2·038	-64 13	163 18	2·018
-42 52	147 24	1·820	-71 55	171 51	2·028	-63 57	161 11	2·010
-44 10	149 29	1·844	-72 12	172 13	2·032	-62 41	156 59	2·022
-45 13	151 57	1·833	-72 09	173 35	2·026	-63 50	156 06	2·013
-45 33	152 45	1·843	-72 57	176 06	2·038	-64 13	154 03	2·011
-46 18	154 30	1·820	-72 35	173 34	2·035	-64 20	153 02	2·032
-47 46	157 40	1·817	-72 31	173 39	2·039	-63 54	151 56	2·023
-49 20	160 13	1·846	-73 47	171 50	2·052	-64 26	148 20	2·065
-50 28	164 09	1·858	-74 10	170 28	2·044	-64 45	142 00	2·068
-50 33	166 19	1·851	-74 06	171 20	2·052	-63 09	139 28	2·043
-52 42	169 10	1·877	-73 56	172 20	2·035	-61 46	135 12	2·051
-53 47	169 02	1·844	-74 36	173 01	2·037	-60 19	131 20	2·071
-54 25	169 16	1·874	-74 44	169 43	2·045	-58 00	128 40	2·056
-55 50	170 06	1·903	-75 22	168 48	2·048	-54 44	132 21	2·027
-57 15	170 40	1·914	-76 06	168 11	2·031	-53 13	135 18	2·047
-57 54	170 25	1·911	-76 46	169 22	2·040	-51 16	136 50	2·041
-58 57	170 57	1·920	-77 47	175 43	2·017			
-59 41	169 38	1·932	-77 04	188 24	2·017			
-60 14	170 15	1·951	-77 17	185 26	2·023			

Observations of the  
**INTENSITY OF THE MAGNETIC FORCE**  
*made in the expedition commanded by*  
**CAPT. JAMES CLARK ROSS R.N.**  
*between*  
**July 1840, and April 1841.**



Observations of the  
**MAGNETIC INCLINATION**  
*made in the Expedition commanded by*  
**CAPT. JAMES CLARK ROSS R.N.**  
*between*  
*July 1840, and April 1841.*



South Latitude

Longitude East 100° of Greenwich